

**Leon County Research and Development Authority
Development Review Committee**

Collins Building
2051 East Paul Dirac Drive
Tallahassee, FL 32310

September 12, 2023
9:00am to 10:00am

Wi-Fi: INVP – Guest
Innovate2051

Agenda

Anyone wishing to submit written comments may do so by 9:00am the day before the scheduled meeting date so that the comments can be distributed to the Committee. Comments submitted after this time (up to the time of the meeting) will be accepted and included in the official record of the meeting. Email comments to: publicinput@inn-park.com and reference the meeting title and date in the subject line. Include your name and contact information. All times are approximate.

1. Call to Order

2. Introductions

3. Approval of Participation by Electronic Means

In accordance with the Bylaws, there being a quorum of members present in person, the members of the Committee present in person are required to approve participation by those participating via Electronic Means acknowledging that the absence is due to extraordinary circumstances.

4. Modifications to the Agenda

5. Public Comment

Any public comment received prior to the meeting will be provided to the Committee members in addition to any in-person public comment.

6. Approval of Draft Meeting Minutes, July 11, 2023 (Attachment A)

7. Florida Department of Transportation Structures Research Center Proposed Vehicle Shelter

DOT requests approval of a vehicle structure to be located at 2007 East Paul Dirac Drive, behind the Phipps Building. (Attachments B-F)

9. New Business

10. Adjourn

**Leon County Research and Development Authority
Development Review Committee**

Collins Building
2051 East Paul Dirac Drive
Tallahassee, FL 32310

July 11, 2023
9:00am to 10:00am

DRAFT Minutes

Members in Attendance: Chair Michael Kramer, Dylan Haase, Ben Hood, Brad Richardson, Kimberly Strobel-Ball.

Members Not in Attendance: None.

Guests: Doug McLeod, Signs by Design of North Florida; Chris Neal, Danfoss; Bryce Hill, Sperry & Associates Construction; Peggy Bielby, LCRDA staff.

1. Call to Order

Michael Kramer called the meeting to order at 9:01am.

2. Introductions

All present introduced themselves.

3. Approval of Participation by Electronic Means

As all committee members were present in person no approval was needed.

4. Modifications to the Agenda

None.

5. Public Comment

None.

6. Approval of Draft Meeting Minutes, June 13, 2023

Dylan Haase offered a motion to approve the draft minutes. Brad Richardson seconded the motion which passed unanimously.

7. Innovation Park Building Sign Specifications, Declarations of Covenants and Restrictions

The committee reviewed requirements of the sign specifications and covenants and restrictions.

8. Danfoss Proposed Monument Sign

Danfoss representatives reviewed the request for a variance for two new signs to be located at the Roberts Road entrance and the West Paul Dirac Drive entrance of the new Danfoss building currently under construction at 1737 West Paul Dirac Drive. They explained that the Danfoss detailed branding requirements dictate the sign design, and acknowledged the signs do not meet any of the current sign specifications and that denial of the variance would not cause any undue financial hardship to Danfoss.

After discussion it was unanimously agreed by the committee that it would recommend for the Board of Governors to deny that variance request as proposed.

Ben Hood offered a motion to recommend denial. Brad Richardson seconded the motion which passed unanimously.

9. New Business

None.

10. Adjourn

The meeting was adjourned at 9:44am.

LCRDA Board of Governors Meeting

Collins Building Seminar Room

Thursday, August 3, 2023

11:00am – 1:00pm



Florida Department of Transportation

RON DESANTIS
GOVERNOR

605 Suwannee Street
Tallahassee, FL 32399-0450

JARED W. PERDUE, P.E.
SECRETARY

August 24, 2023

Mr. Michael Kramer
Executive Director
Leon County R & D Authority
Innovation Park
1736 Paul Dirac Drive
Tallahassee, FL 32310

RE: Truck Shelter
Phipps Building
1736 West Paul
Tallahassee, FL 32310

Dear Mr. Kramer,

We are herein submitting our site plan for an application for approval of the installation of the truck shelter for FDOT. This is a 50'W x 60'L x 23'H fabric structure manufactured by Big Top Manufacturing Inc. needed to protect and shield trucks that carry materials for testing purposes integral for the structural bridge research lab. The structure is largely screened by the gate and surrounding trees, faces a rear parking lot and is partially visible over the fence line. The translucent fabric has a UPF rating of 2,000 and blocks 99.95% of harmful UV-A and UV-B radiation deflecting heat gain and allowing longevity of the vehicles. The structure uses heavy duty PVC-vinyl fabric that is flame retardant and rip resistant anchored to the ground using 40" spiral anchors and galvanized steel that meets Florida Building Code requirements. Permission is needed to trim existing vegetation to maintain the rear egress into the adjacent parking lot.

The building will be 26' off the rear set-back as shown in *figure A* on the site plan. A similar example that was 50'W x 72'L x 23'H that was installed in the same Jurisdiction of Authority (JOA) for the Department of Emergency Management which was approved for use in Tallahassee in 2021 is attached.

Pending manufacture and receipt of the structure, it will take two weeks to install. Please let us know if we need to meet to review plans or if we can answer any questions.

Sincerely,

Scott Cannard, AIA, NCARB
Senior Architect
Florida Department of Transportation

Project Description

A 50W x 60L x23H fabric structure manufactured by Big Top needed to protect and shield trucks that carry materials for testing purposes integral for the structural bridge research. The structure is largely screened by the gate and surrounding trees, faces a rear parking lot and is partially visible over the fence line. The translucent fabric has a UPF rating of 2,000 and blocks 99.95% of harmful UV-A and UV-B radiation deflecting heat gain and allowing longevity of the vehicles. The structure uses heavy duty PVC-vinyl fabric that is flame retardant and rip resistant anchored to the ground using 40" spiral anchors and galvanized steel that meets Florida Building Code requirements. Permission is needed to trim existing vegetation to maintain the rear egress into the adjacent parking lot.

Vegetation

Permission is needed to trim existing vegetation to maintain the rear egress into the adjacent parking lot.



Current (Google Earth 2023) below:



Before (Google Earth 2009) below:



Picture of Mag Lab Rods



RESOLUTION

WHEREAS, the Leon County Research and Development Authority (Authority) is a local governmental body created and existing pursuant to Florida Statutes, which has acquired by long term lease from the State of Florida certain lands for development as Innovation Park, a research and development park; and

WHEREAS, the Authority has adopted a Declaration of Protective Covenants and Restrictions which creates a development review committee to review and approve all plans for construction or alteration of any building or other improvements in Innovation Park; and

WHEREAS, the City of Tallahassee's Land Use Administrator has historically been a member of the Authority's Development Review Committee and the Authority wishes to memorialize this position; and

WHEREAS, the City of Tallahassee has approved Innovation Park's planned unit development with conditions acceptable to the Authority regarding the scope of review by the LCRDA Development Review Committee;

BE IT RESOLVED:

1. The LCRDA Development Review Committee shall have, as one of its voting members, the Tallahassee-Leon County Planning Department's land use administrator or other person designated by the Planning Department Director.


2. The LCRDA Development Review Committee's review of a proposed project shall incorporate the elements of Site Plan A Review listed in the attached City of Tallahassee/Innovation Park

Site Plan Review Completeness Determination Checklist, incorporated by reference into this Resolution.

3. If the Planning Department's designee is not satisfied that the LCRDA Development Review Committee has adequately reviewed an aspect of a project application which is part of the Site Plan A requirements incorporated by reference, the Planning Department designee may request and the LCRDA shall require the application for an Innovation Park development project to be submitted to the City of Tallahassee, Growth Management Department for Site Plan A Review.

Resolved this 16th day of June, 1993, by the Leon County Research and Development Authority.

By:


DR. ROBERT M. JOHNSON, Chairman
LEON COUNTY RESEARCH AND DEVELOPMENT
AUTHORITY

CITY OF TALLAHASSEE/INNOVATION PARK
 SITE PLAN REVIEW
 COMPLETENESS DETERMINATION CHECKLIST

In order for an application to be eligible for review, the following materials must be submitted to the Innovation Park/Tallahassee Development Review Committee. Five copies are required for this review.

APPLICANT VERIFICATION	STAFF VERIFICATION	
X	_____	1. The applicant shall submit to the Innovation Park/Tallahassee Development Review Committee a detailed statement of objectives indicating: <ul style="list-style-type: none"> a. The general purpose of the development b. The type and square footage of non-residential development including floor area ratios, pervious and impervious surface areas, and other standards as may be required.
X	_____	
X	_____	2. A site conditions map drawn to an appropriate engineer's scale sufficient to show and to depict the location of existing property lines for both private and public property (boundary survey), existing contours shown at a contour interval of two (2) feet, streets, buildings, watercourses, transmission lines, sewers, culverts, and drain pipes, water mains, public utility easements, wooded area, streams, lakes, marshes, and any other physical conditions on the site.
NA	_____	3. A site plan shall be drawn to an appropriate engineer's scale showing: <ul style="list-style-type: none"> a. The proposed grading plan. b. All rights-of-way and easements showing points of reference. c. All proposed buildings and other structures.
X	_____	
X	_____	

<u>NA</u>	<u> </u>
<u>NA</u>	<u> </u>
<u>NA</u>	<u> </u>
<u>NA</u>	<u> </u>
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- d. The location of phase lines indicating all applicable construction phases if applicable.
 - e. The off-street parking and loading plan.
 - f. A circulation diagram showing vehicular and pedestrian movements including any special engineering features and traffic regulation devices.
 - g. Provisions for the control of signs including size, shape and appearance.
4. A utility service plan showing:
- a. Existing drainage and sewer lines.
 - b. The disposition and/or retention of sanitary waste and storm water.
5. A landscaping plan showing:
- a. Landscaped areas.
 - b. All specimen trees or groups of trees thirty-six (36) inches in diameter or larger, indicating those to be retained, removed, or relocated.
 - c. The location, height, and material for walks, fences, walkways, and other man-made landscape features.
 - d. Any special landscape features including but not limited to, man-made lakes, land sculptures and waterfalls.
6. Statistical information including:
- a. Total acreage of the site.
 - b. Maximum building coverage expressed as a percentage of the total site area.
 - c. The area of land devoted to rights-of-way, transportation easements, parking and other transportation facilities expressed as a percentage of the total site area.
 - d. The area of land devoted to undisturbed open space expressed as a percentage of the total site area.
 - e. The calculated density/intensity for the project and impervious percentage.

TBD < 2 weeks on site

X

X

7. Development schedule showing order of construction, proposed date for the beginning of construction and completion of the project as a whole and any phases thereof.

8. This completed checklist.

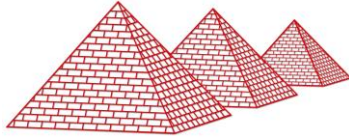
9. Other relevant information which is deemed to be appropriate by the Innovation Park/Tallahassee Development Review Committee to ensure consideration of all relevant issues.

If the Innovation Park/Tallahassee Development Review Committee refers the project to the City of Tallahassee the following will be required:

10. Completed application for Site Plan Review - Type A.

11. Application fee.

Note: All of the items listed above must be submitted at time of application, unless the Development Review Committee Chairman waives a specific item.



PSE CONSULTING ENGINEERS INC.

STRUCTURAL ENGINEERING CALCULATIONS

PROJECT: 50 x 72 x 23 Department Emergency
Management

PROJECT LOCATION: 3266 Capital Cir SW,
Tallahassee, FL 32310

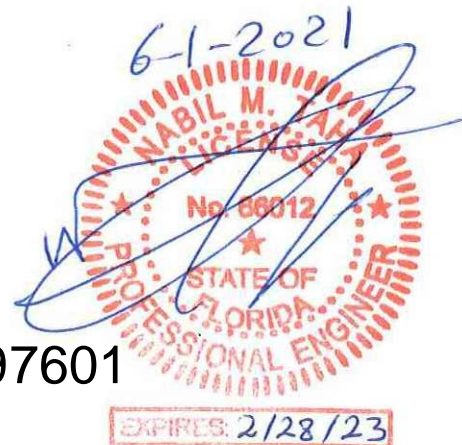
PSE PROJECT NUMBER: Big Top 221-80

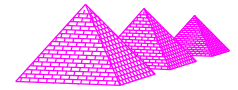
DATE: 05/27/21

BY: Nabil Taha, Ph.D., P.E.
Address: 250 Main Street
Klamath Falls, OR 97601

Florida License No: #66012

Company License No: #33311





**PSE
Consulting
Engineers,
Inc.**

www.structure1.com
Klamath Falls Office
250 Main
Klamath Falls, Oregon
97603
Phone: (541) 850-6300
Fax: (541) 850-6233
info@structure1.com

A. GENERAL REQUIREMENT:

1. Furnish all labor, materials, and equipment necessary to complete the work shown or inferred by these drawings.
2. Where construction details are not shown or noted for any part of the work, such details shall be the same as for similar work shown on the drawings.
3. Notes and details on the drawings take precedence over the general notes and typical details in case of conflict.
4. Locate and protect underground or concealed conduit, plumbing or other utilities where new work is being performed.
5. The contract drawings and specifications represent the finished structure and do not indicate methods, procedures or sequence of construction. The contractor shall take necessary precautions to maintain and insure the integrity of the new and any existing structures during construction. The design stresses shall not be exceeded during construction based on the age of each element. Neither the owner nor Architect/Engineer will enforce safety measure regulations. Installation Contractor shall design, construct and maintain all safety devices, including shoring and bracing for the new and any existing structures and shall be solely responsible for conforming to all local, state and federal safety and health standards, laws and regulations.
6. Obtain prior written approval for any changes to the drawings.
7. The contractor shall review and compare the structural drawings with all other Construction Documents, such as Architectural, Mechanical and Electrical drawings, specifications, etc. Do not scale drawings. The contractor shall verify dimensions, elevations and all information. Report, in writing, any inconsistencies, errors, or omissions to the Architect/Engineer of record before proceeding with the work.
8. All existing constructions are shown schematic only. Installation Contractor is responsible to verify actual conditions and allow for them in his bid. Notify the Architect/Engineer, in writing, in case of any discrepancy between actual conditions and what is shown on the structural drawings before proceeding with the work.
9. See Architectural, Mechanical, Electrical and other drawings for embedded items.
10. All communication shall be in writing. No verbal communications, decisions, instructions or approvals shall be valid.
11. Adequate drainage path must be provided to drain water away from the perimeter of the building.

B. CODE AND LOADS:

1. All material and construction work for this project shall conform to 2020 Florida Building Code per 2018 International Building Code (IBC 2018) along with local amendments by the Authority Having Jurisdiction. The International Building Code Parameters are:
 - a. Roof Dead Load = 1 PSF
 - b. Ground Snow Load = 0 PSF
 - c. Roof Snow Load = 0 PSF (FLAT)
 - d. Roof Live Load = 5 PSF (Governs)
 - e. Seismic Occupancy Category = II
 - f. R, Response Modification Coefficient = 3.0
 - g. Ultimate Wind Speed, V3g = 110 mph, Exposure = C, Category II

Seismic Parameters:
 a. Ss = 0.072
 b. S1 = 0.05
 c. Sds = 0.102
 d. Sd1 = 0.085
 e. SDC = B

C. HOT-ROLLED STEEL:

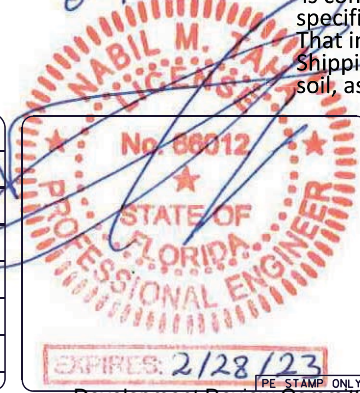
1. Tube Frames shall be manufactured from steel with the following properties:
 - a. Yield strength: 50,000 psi (rectangular); 55,000 psi (round)
 - b. Tensile Strength: 55,000 psi (rectangular); 60,000 psi (round)

D. FOUNDATION DESIGN:

1. Foundation design/check to support the new truss reactions/loads was not included in the scope of service.
2. Any foundation shown on this drawings, if any, are approximate and need to be checked/adjusted to the local site conditions and local soil properties by a licensed Engineer hired by the Contractor/Builder or Owner of this shelter.
3. For soil anchors applications, see page S-0A for additional requirements.

All engineering to support the structure is considered "by others", unless specifically noted on our drawings. That includes, but is not limited to, shipping containers, concrete, soil, asphalt, custom support steel, etc.

6-1-2021




BIG TOP MANUFACTURING INC.
 3255 NORTH US 19
 PERRY, FL 32347
 PH: (850) 584 - 7786

CUSTOMER: DEM	
SIZE 50 x 72 x 23	
LOCATION Tallahassee, FL	
CUSTOMER CONTACT:	SALES: DH
DRAWN BY: Mo	DATE DRAWN: 5/27/21
APPROVED BY:	

NOTES:	
FOUNDATION TYPE:	
TITLE:	
TITLE:	
TITLE:	
TITLE:	
TITLE:	
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DRAWING TYPE: ENGINEERING	
PAGE: S-0	
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D. FOUNDATION DESIGN CONTINUED:

4. For soil anchor applications, as an alternative to item 2 on sheet S-0, the following approximate method could be used.
 - a. Number of soil anchors shown on the plans assumed that the soil anchor's ultimate capacity is 2500 lbs minimum, which shall be verified by site test results.
 - b. Pull out strength varies based on the local soil type and shall be verified by local soil tests at the site.
 - c. The tables below should be used as a guide only and subject to results of anchor pull test at the site.
 - d. Perform soil anchor tests to verify the above value for the soil type. A minimum of four tests shall be conducted to verify the assumed capacity above.
 - e. Use an approved method to obtain the values for the site:
 - (i) Dynamometer to obtain uplift by pulling out the anchors with a forklift
 - (ii) Hydraulic Pump
 - f. Pull out strength shall be measured at a maximum deflection/letup of 1/2 inch.
 - g. The tests shall be performed by a third party approved testing agency. In absence of a third party approved testing agency, the tests shall be performed in the presence of at least two of the following representatives and the results thereafter shall be signed by them upon completion of the tests.
 - (i) Big Top Manufacturing representative
 - (ii) Customer representative
 - (iii) Installation representative
 - h. If the test results are less than the above value, do not install the anchors and contact the Engineer of Record immediately, both by telephone and in writing.
 - i. If the test results are equal to or more than the above value, install the soil anchors as shown on the plans.
 - j. Results of the tests shall be submitted to both the Engineer of Record and to the General Manager of Big Top Manufacturing Inc.
 - k. The Owner and/or the Installation Contractor shall assume all responsibilities for the accuracy of the test results when using this method.

Soil Anchor Installation Guideline

Soil Type	Anchor Capacity (lbs)
Soft/Medium Sandy	600
Medium/Sandy Grass Top	1000
Medium/Sandy Soil Gray	1200
Medium/Sandy with Asphalt Top	1800
Medium Soil with Limerock and Asphalt	2000
Caliche	2500
Medium Dense Soil - Dry	3000
Medium Dense Soil with Asphalt Top	3500
Hard Clay	5500
Hard Clay with Asphalt Top	6000

Time to Set Anchor (min)	Pull Out Strength (lbs)
<1	0
1-3	0
4-6	600-1100
7-9	1100-1800
10-15	1800-2500
>15	2500-3500

Time to Set Anchor (min)	Pull Out Strength (lbs)
<1	0
1-3	600-1100
4-6	1100-1800
7-9	1800-2500
10-15	2500-3500
>15	>3500

Soil Anchor Capacity Based on Time to Set Anchor w/ 60lb Breaker

②

Scale: N.T.S.

Soil Anchor Capacity Based on Time to Set Anchor w/ 90lb Breaker

③

Scale: N.T.S.

Soil Anchor Capacity Based on Soil Type

①

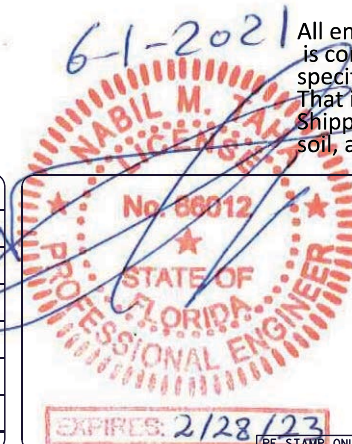
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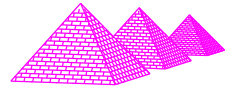
CUSTOMER: DEM	
SIZE 50 x 72 x 23	
LOCATION Tallahassee, FL	
CUSTOMER CONTACT:	SALES: DH
DRAWN BY: Mo	DATE DRAWN: 5/27/21
APPROVED BY:	

NOTES:	
FOUNDATION TYPE:	
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All engineering to support the structure is considered "by others", unless specifically noted on our drawings. That includes, but is not limited to, shipping containers, concrete, soil, asphalt, custom support steel, etc.

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PAGE: S-0A	
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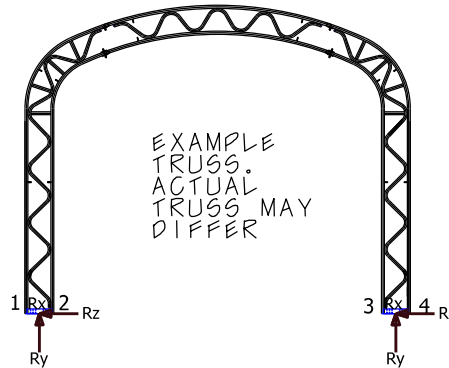
D. FOUNDATION DESIGN CONTINUED:

5. Foundation must meet the building reaction data shown below.

*See notes below		UNFACTORED BASE REACTIONS TO CONSIDER AT TYPICAL BASES											
		Side A, Joint 1 (1 as per RISA Model)			Side A, Joint 2 (2 as per RISA Model)			Side B, Joint 3 (3 as per RISA Model)			Side B, Joint 4 (4 as per RISA Model)		
		Rx (kip)	Ry (kip)	Rz (kip)	Rx (kip)	Ry (kip)	Rz (kip)	Rx (kip)	Ry (kip)	Rz (kip)	Rx (kip)	Ry (kip)	Rz (kip)
Dead Load, Self Weight	DL	0	0.5	-0.07	0	0.06	-.07	0	0.06	.07	0	0.49	0.07
Snow Load/ Live Load	SL/RLL	0	1.2	-0.21	0	0.09	-.22	0	-.08	.22	0	1.19	.21
Wind Load, Normal to Ridge, Case A	WLZ(+GCp)	0	-5.6	1.25	0	1.29	1.28	0	-1.07	-.17	0	-2.51	-.16
Wind Load, Normal to Ridge, Case B	WLZ(-GCp)	0	-3.48	1.07	0	.88	1.1	0	-1.14	-.23	0	-1.81	-0.23
*Wind Load, Along the Ridge, Case A	WLX(+GCp)												
*Wind Load, Along the Ridge, Case B	WLX(-GCp)												

* Note on reactions:

- a. All reactions are un-factored loads as per IBC 2018. Reactions should be combined as required by the load combinations from IBC or other applicable code.



Typical Reaction at Base for Intermediate Frame

① Scale: N.T.S.

6-1-2021

All engineering to support the structure is considered "by others", unless specifically noted on our drawings. That includes, but is not limited to, Shipping containers, concrete, soil, asphalt, custom support steel, etc.

BIG TOP
MANUFACTURING

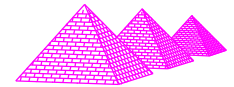
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TITLE:	
TITLE:	

NABIL M. Taha
No. 86012
STATE OF FLORIDA
PROFESSIONAL ENGINEER
EXPIRES: 2/28/23

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E. WIND LOAD SAFETY RESTRICTIONS:

1. The Fabric cover for this structure must conform to the following 2020 Florida Building Code Section:

CH 31-(Special Construction) Section - 3105.4 Design:

3105.4.2.1 states that:

The wind design loads for any fabric or membrane-covered structure designed with a quick removal or breakaway membrane or fabric at wind velocities of 75 mph, shall be based on the following criteria:

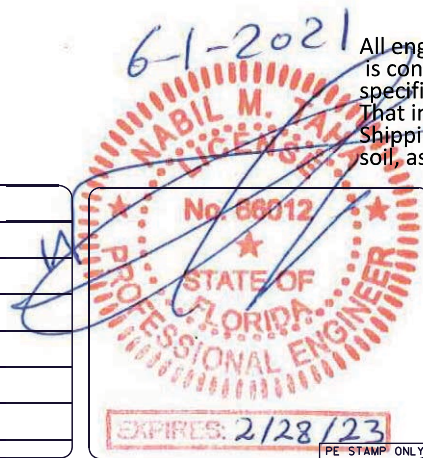
- 1.) Minimum wind speed of 105 mph.
- 2.) Exposure category B, C, or D as defined in Ch 16.


2. For this building, the fabric shall be removed from the steel trusses before the 3-second gust wind speed exceeds 110 mph.

3. Naked trusses without the fabric shall be safe for wind speed of 170 mph.

All engineering to support the structure is considered "by others", unless specifically noted on our drawings. That includes, but is not limited to, Shipping containers, concrete, soil, asphalt, custom support steel, etc.

6-1-2021

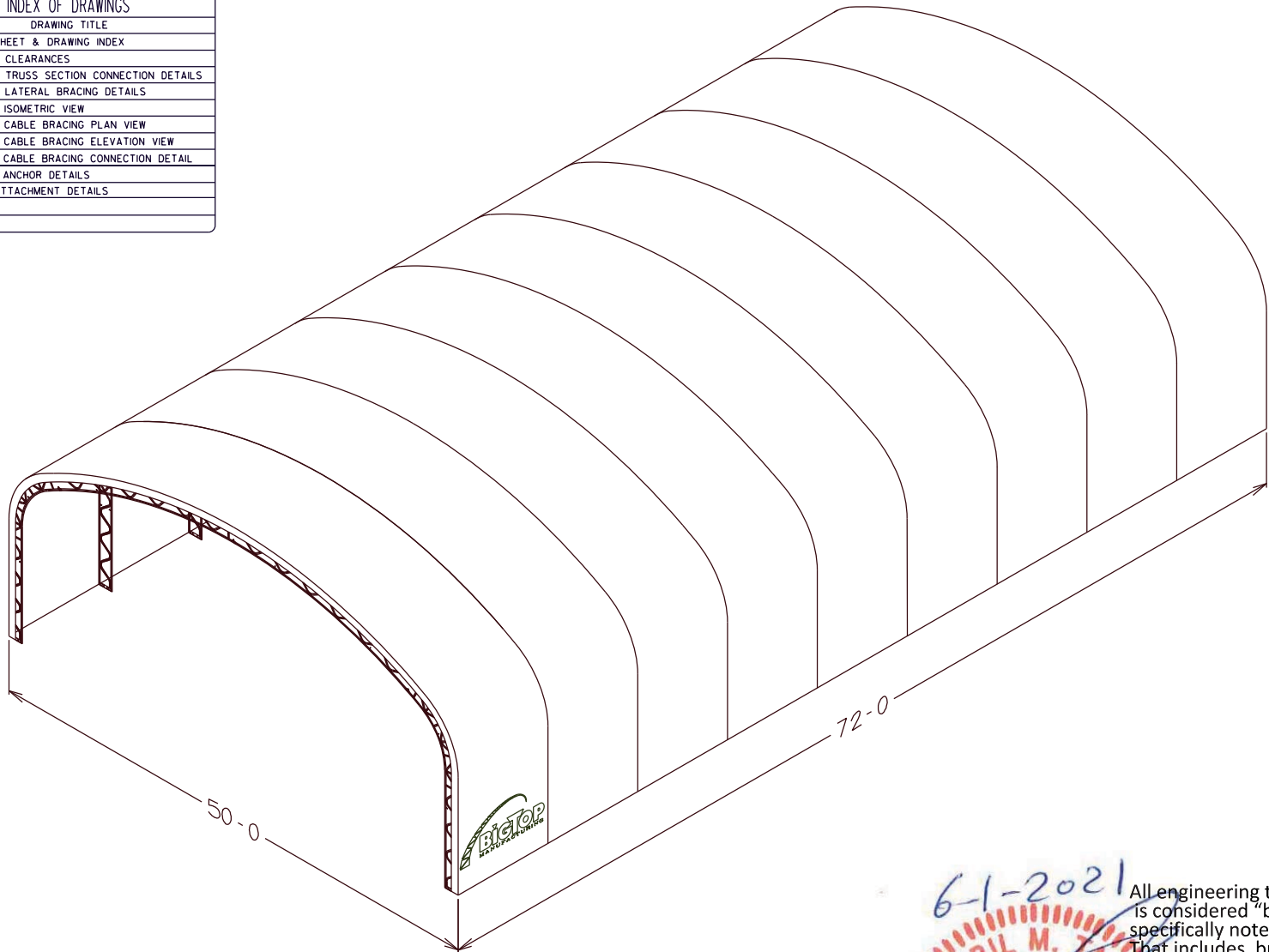


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	APPROVED BY:	

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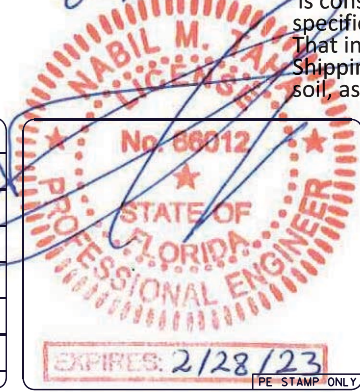
INDEX OF DRAWINGS	
DRAWING NUMBER	DRAWING TITLE
S1	COVER SHEET & DRAWING INDEX
S2	FRAME - CLEARANCES
S3	FRAME - TRUSS SECTION CONNECTION DETAILS
S4	FRAME - LATERAL BRACING DETAILS
S5	FRAME - ISOMETRIC VIEW
S6	FRAME - CABLE BRACING PLAN VIEW
S7	FRAME - CABLE BRACING ELEVATION VIEW
S8	FRAME - CABLE BRACING CONNECTION DETAIL
S9	FRAME - ANCHOR DETAILS
S10	FABRIC ATTACHMENT DETAILS



COVER SHEET & DRAWING INDEX

All engineering to support the structure is considered "by others", unless specifically noted on our drawings. That includes, but is not limited to, shipping containers, concrete, soil, asphalt, custom support steel, etc.

6-1-2021

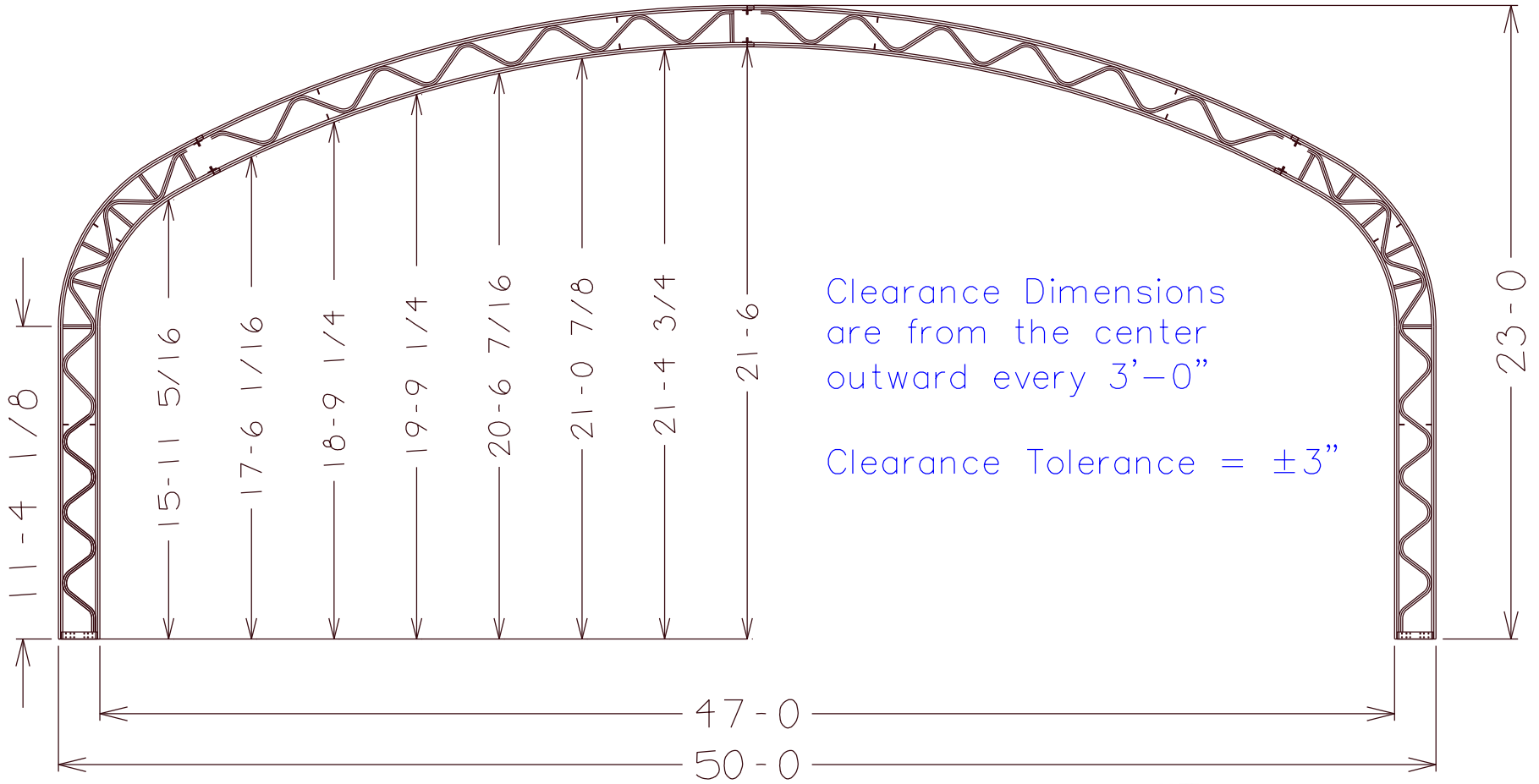


BIG TOP MANUFACTURING
BIG TOP MANUFACTURING INC.
3255 NORTH US 19
PERRY, FL 32347
PH: (850) 584 - 7786

CUSTOMER: DEM	
SIZE 50 x 72 x 23	
LOCATION Tallahassee, FL	
CUSTOMER CONTACT:	SALES: DH
DRAWN BY: Mo	DATE DRAWN: 5/27/21
APPROVED BY:	

NOTES:	
FOUNDATION TYPE:	
TITLE	
TITLE	
TITLE	
TITLE	
TITLE	
TITLE	

DRAWING TYPE: ENGINEERING	
PAGE: S-1	
*ALL INFORMATION IS PROPERTY OF BIG TOP MANUFACTURING INC.	



Clearance Dimensions
are from the center
outward every 3'-0"

Clearance Tolerance = $\pm 3''$

FRAME - CLEARANCES

61-2021

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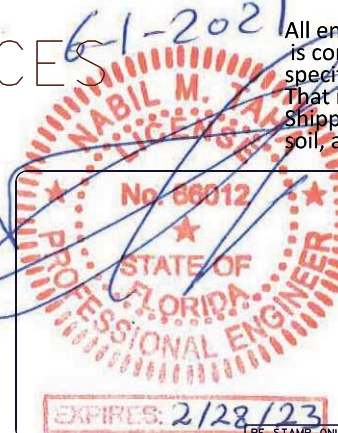


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PERRY, FL 32347
PH: (850) 584 - 7786

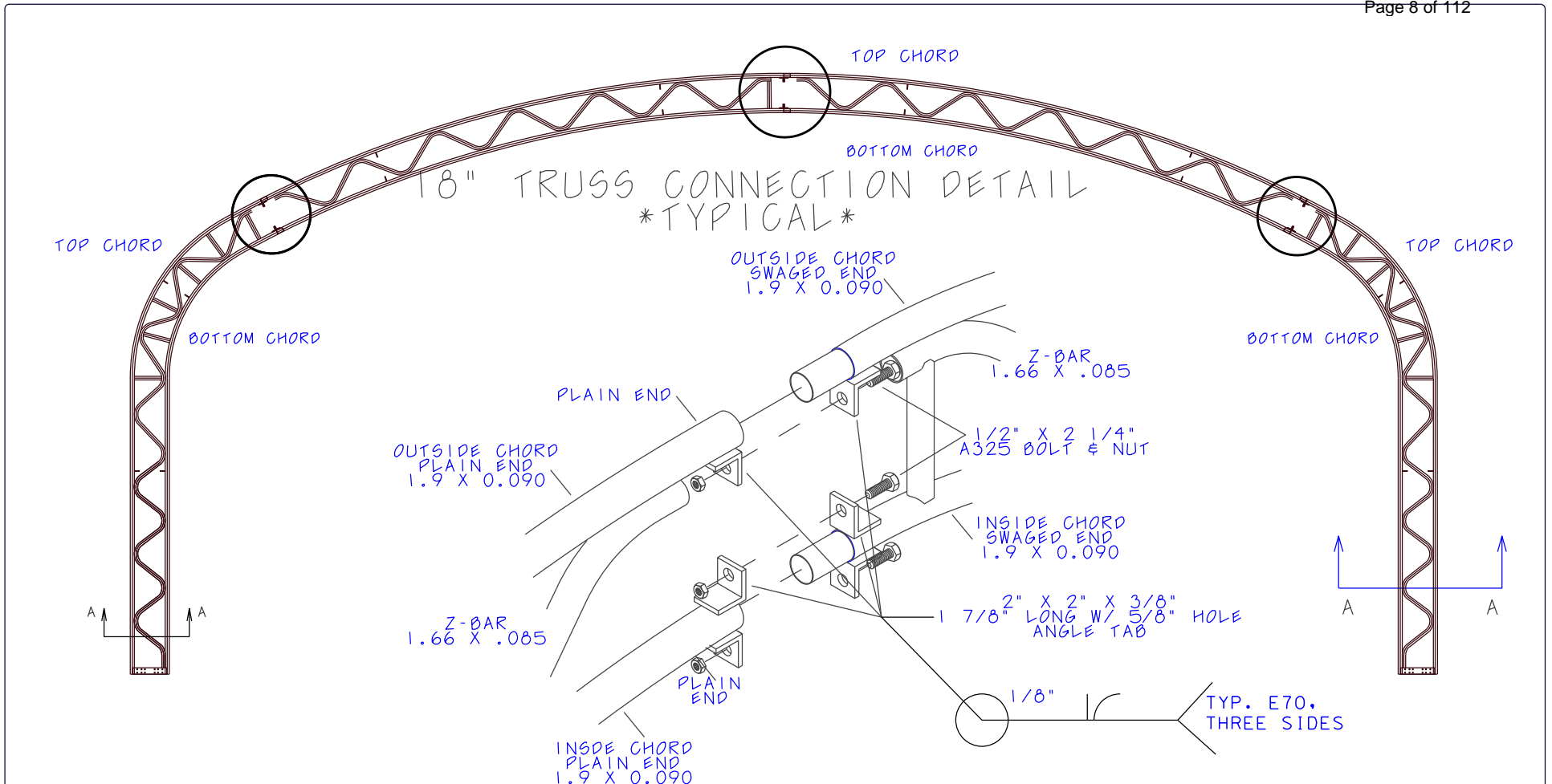
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APPROVED BY:	

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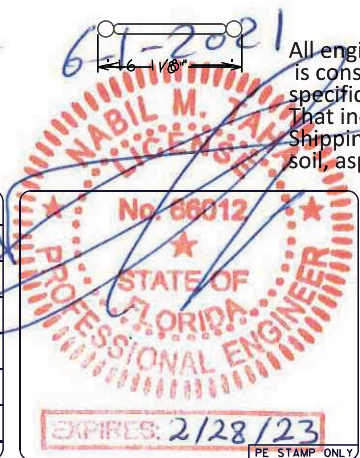


Professional Engineer Seal: NABIL M. J. LICATA, No. 86012, STATE OF FLORIDA, PROFESSIONAL ENGINEER, EXPIRES: 2/28/23

DRAWING TYPE: ENGINEERING
PAGE: S-2
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SECTION A-A
 TRUSS CHORD IS 1.90" X 0.090 WALL THICKNESS
 Z-BAR CHORD IS 1.66" X 0.085 WALL THICKNESS
 TENSILE: 60,000 PSI
 YIELD: 55,000 PSI



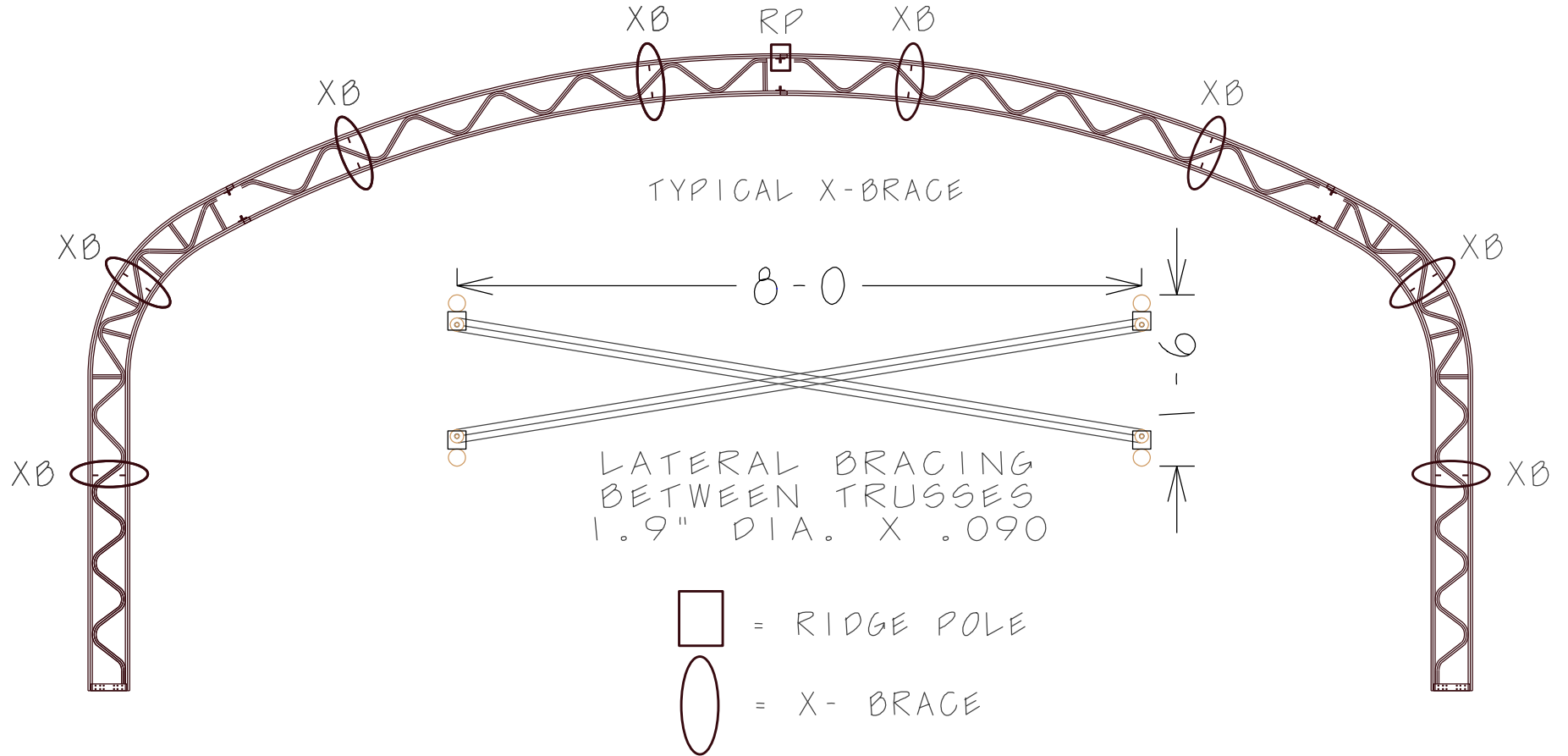
All engineering to support the structure is considered "by others", unless specifically noted on our drawings. That includes, but is not limited to, shipping containers, concrete, soil, asphalt, custom support steel, etc.

FRAME - TRUSS SECTION CONNECTION DETAILS

 BIG TOP MANUFACTURING INC. 3255 NORTH US 19 PERRY, FL 32347 PH: (850) 584 - 7786	CUSTOMER: DEM	
	SIZE 50 x 72 x 23	
	LOCATION Tallahassee, FL	
	CUSTOMER CONTACT: SALES: DH	
	DRAWN BY: Mo	DATE DRAWN: 5/27/21
	APPROVED BY:	

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DRAWING TYPE: ENGINEERING
PAGE: S-3
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FRAME - LATERAL BRACING DETAILS

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PH: (850) 584 - 7786

CUSTOMER: DEM	
SIZE 50 x 72 x 23	
LOCATION Tallahassee, FL	
CUSTOMER CONTACT:	SALES: DH
DRAWN BY: Mo	DATE DRAWN: 5/27/21
APPROVED BY:	

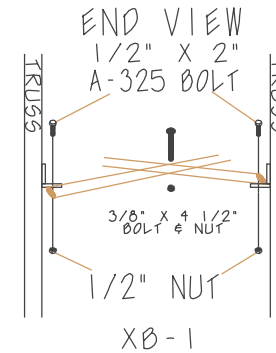
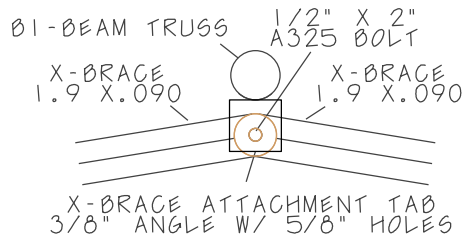
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6-1-2021

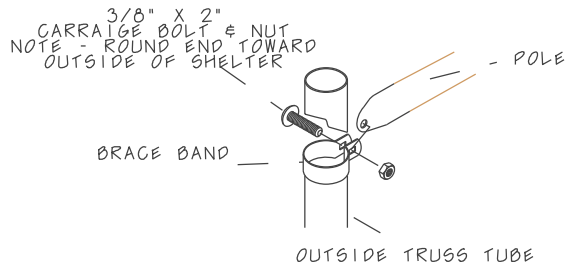
NABIL M. Taha
LICENSE No. 86012
STATE OF FLORIDA
PROFESSIONAL ENGINEER
EXPIRES: 2/28/23

All engineering to support the structure is considered "by others", unless specifically noted on our drawings. That includes, but is not limited to, Shipping containers, concrete, soil, asphalt, custom support steel, etc.

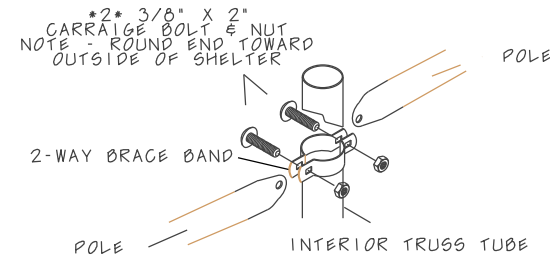
DRAWING TYPE: ENGINEERING	
PAGE:	S-4
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BRACE BAND DETAIL
TYPICAL



2-WAY BRACE BAND DETAIL
TYPICAL



RIDGE POLE



FRAME - LATERAL BRACING DETAILS

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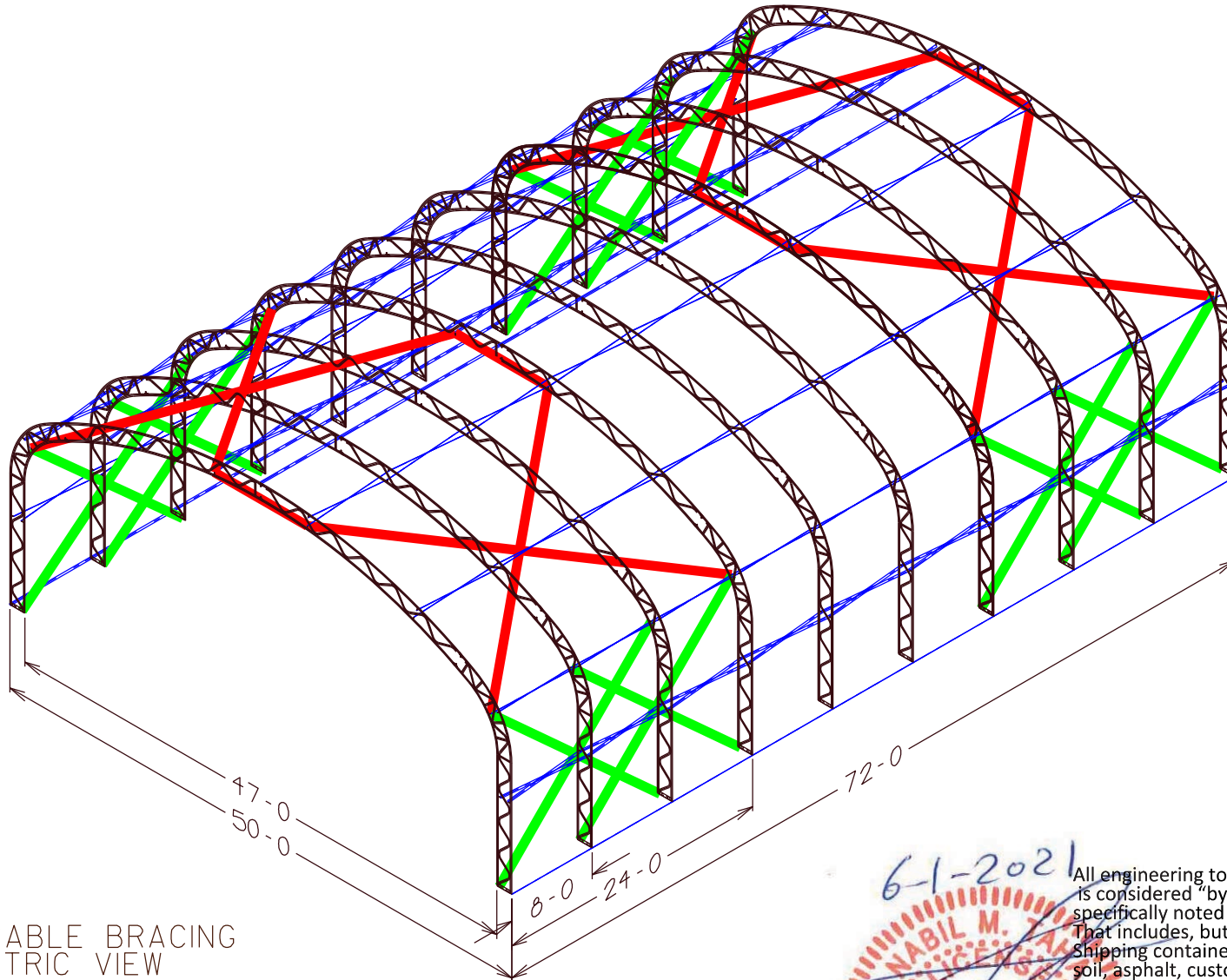
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DRAWN BY: Mo	DATE DRAWN: 5/27/21
APPROVED BY:	

NOTES:	
FOUNDATION TYPE:	
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6-1-2021

PROFESSIONAL ENGINEER
STATE OF FLORIDA
No. 86012
EXPIRES: 2/28/23
IPE-STAMP ONLY

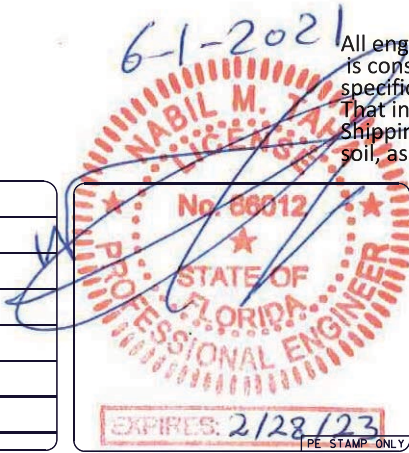
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PAGE:	S-4A
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FRAME - CABLE BRACING
ISOMETRIC VIEW

All engineering to support the structure is considered "by others", unless specifically noted on our drawings. That includes, but is not limited to, shipping containers, concrete, soil, asphalt, custom support steel, etc.

6-1-2021



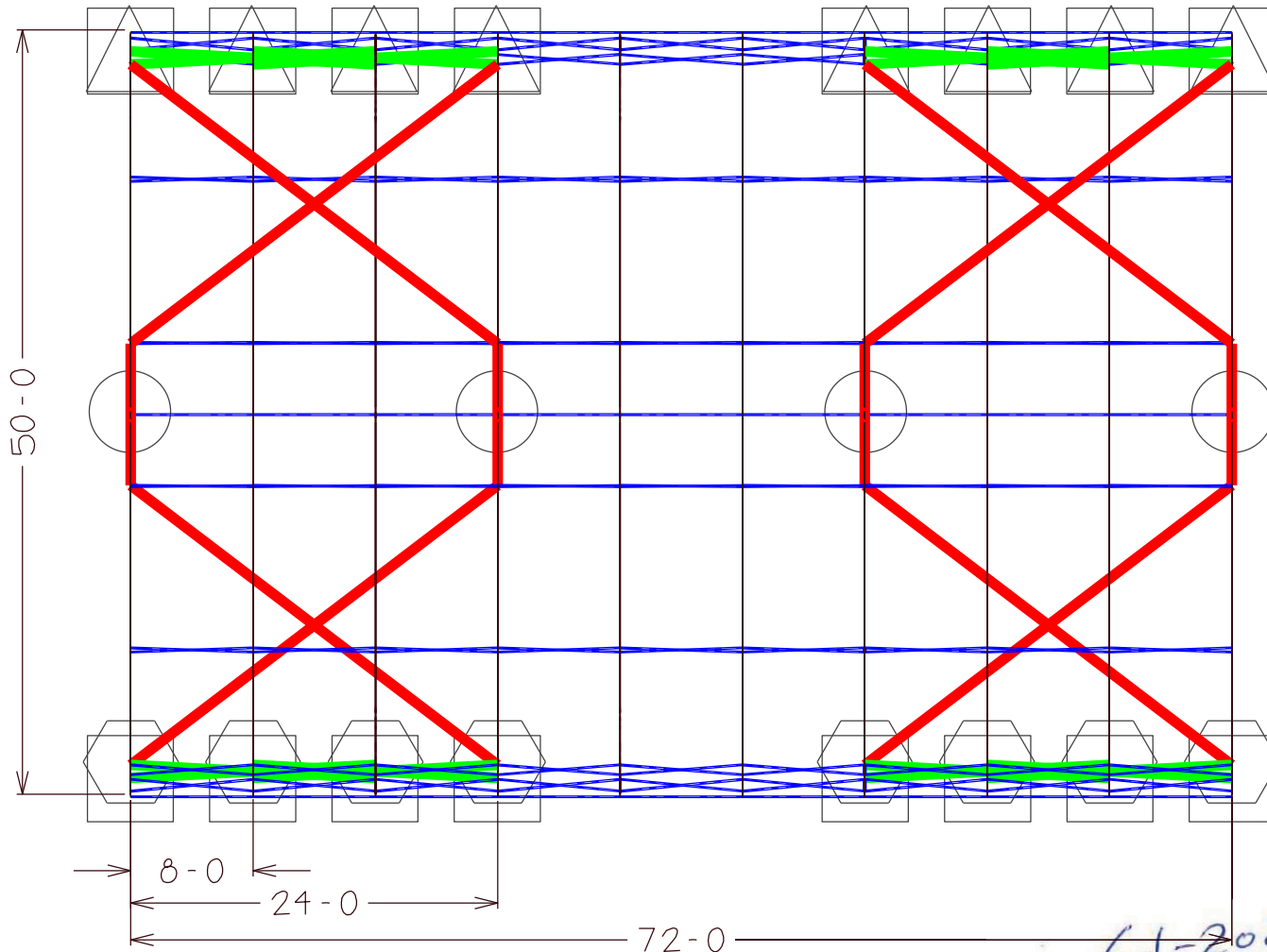
BIG TOP
MANUFACTURING

BIG TOP MANUFACTURING INC.
3255 NORTH US 19
PERRY, FL 32347
PH: (850) 584 - 7786

CUSTOMER: DEM	
SIZE 50 x 72 x 23	
LOCATION Tallahassee, FL	
CUSTOMER CONTACT:	SALES: DH
DRAWN BY: Mo	DATE DRAWN: 5/27/21
APPROVED BY:	

NOTES:	
FOUNDATION TYPE:	
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DRAWING TYPE: ENGINEERING	
PAGE: S-5	
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FRAME - CABLE BRACING
PLAN VIEW

All engineering to support the structure is considered "by others", unless specifically noted on our drawings. That includes, but is not limited to, shipping containers, concrete, soil, asphalt, custom support steel, etc.

6-1-2021

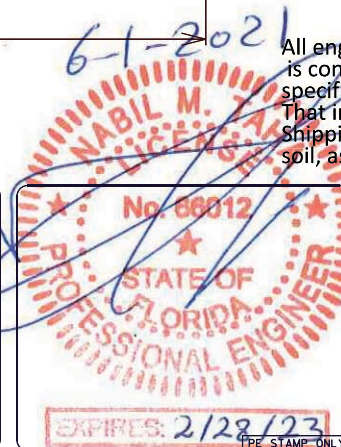


BIG TOP
MANUFACTURING INC.

BIG TOP MANUFACTURING INC.
3255 NORTH US 19
PERRY, FL 32347
PH: (850) 584 - 7786

CUSTOMER: DEM	
SIZE 50 x 72 x 23	
LOCATION Tallahassee, FL	
CUSTOMER CONTACT:	SALES: DH
DRAWN BY: Mo	DATE DRAWN: 5/27/21
APPROVED BY:	

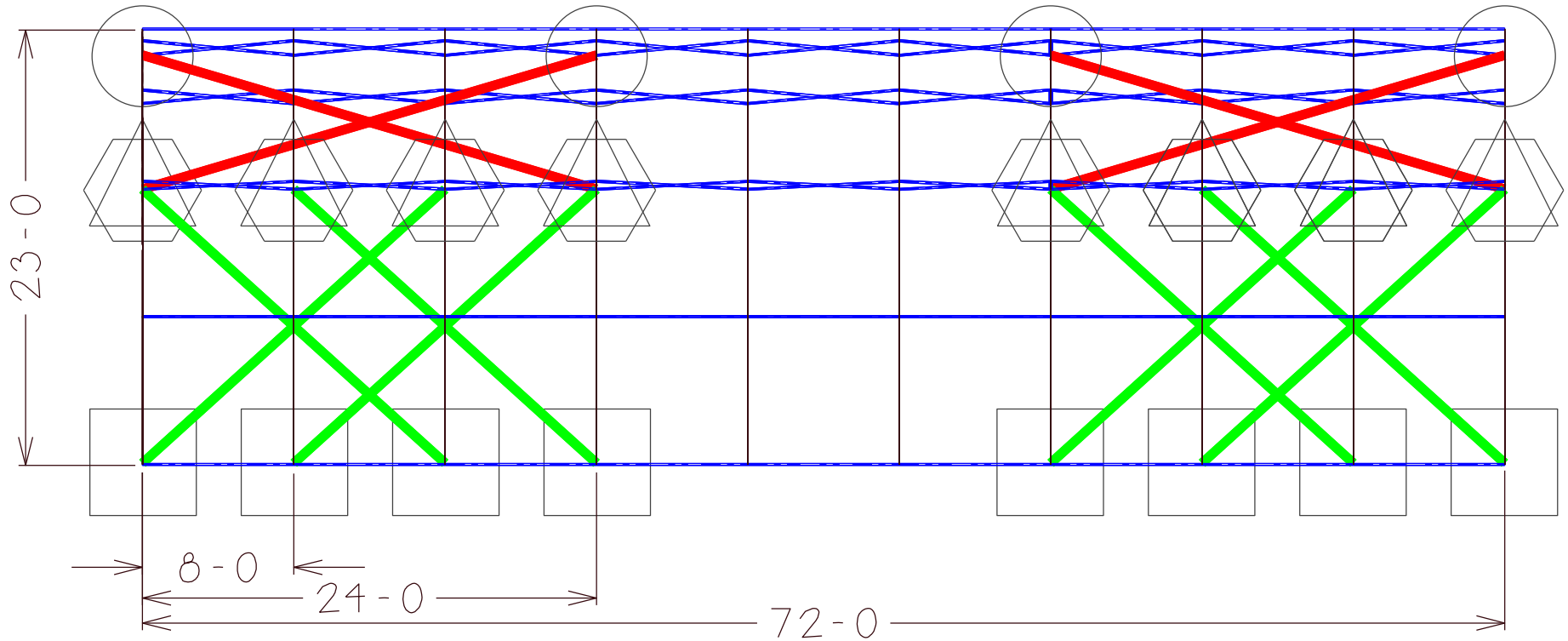
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STATE OF FLORIDA
No. 86012
EXPIRES: 2/28/23

DRAWING TYPE: ENGINEERING	
PAGE:	S-6
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FRAME - CABLE BRACING ELEVATION VIEW




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CUSTOMER: DEM	
SIZE 50 x 72 x 23	
LOCATION Tallahassee, FL	
CUSTOMER CONTACT:	SALES: DH
DRAWN BY: Mo	DATE DRAWN: 5/27/21
APPROVED BY:	

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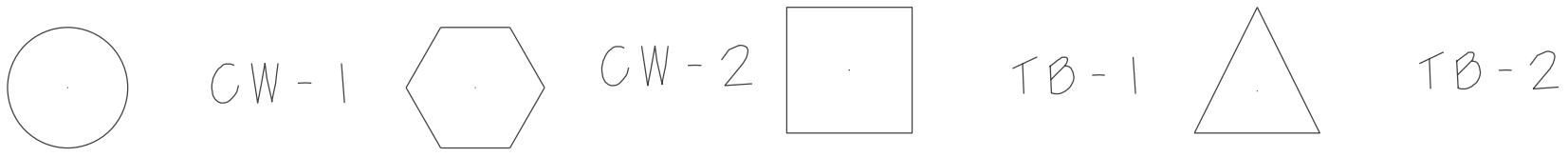
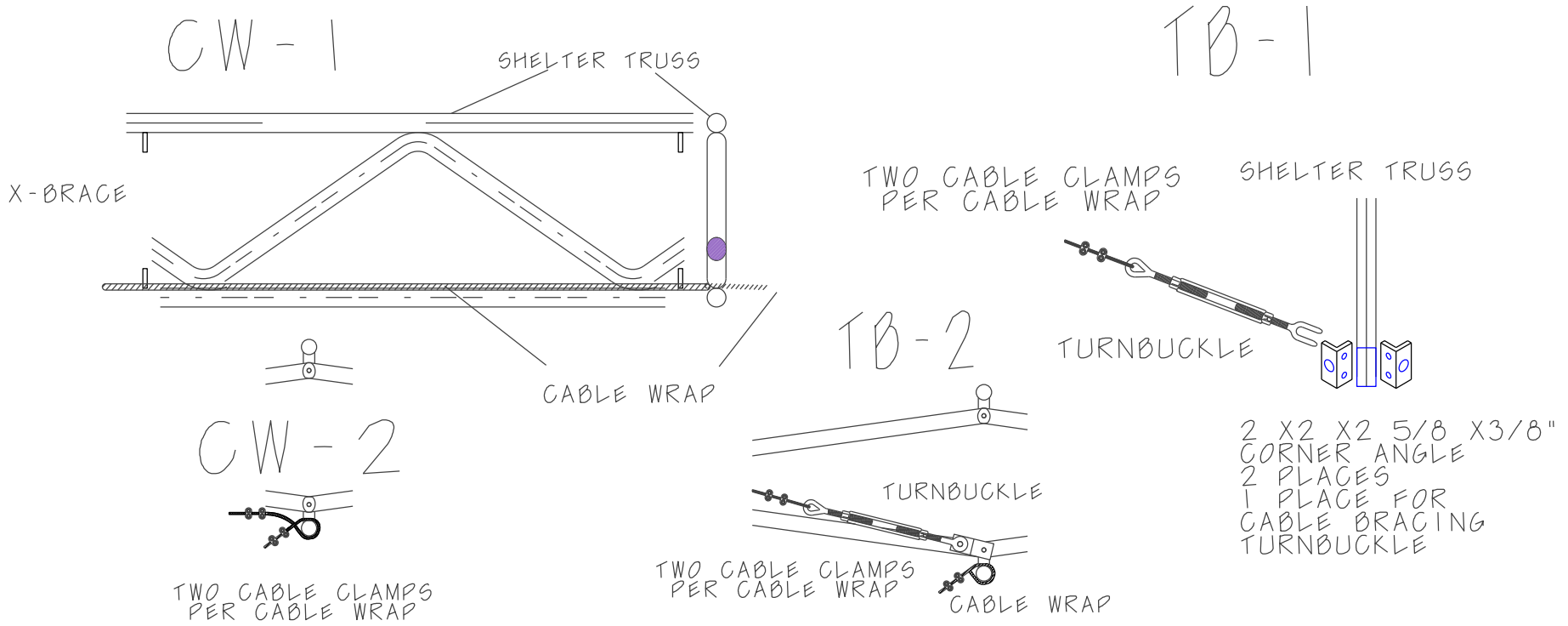
6-1-2021



Professional Engineer
NABIL M. TAHAM
No. 88012
STATE OF FLORIDA
EXPIRES: 2/28/23

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PAGE: S-7
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TURNBUCKLE
1/2" X 6" EYE/JAW
WLL 2, 200LBS.

WIRE ROPE *CABLE*
7X19 GAC
1/4" GAC
BREAKING STRENGTH 3.5 TONS

2 X2 X2 5/8 X3/8"
CORNER ANGLE
2 PLACES
1 PLACE FOR
CABLE BRACING
TURNBUCKLE

FRAME - CABLE BRACING CONNECTION DETAIL

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MANUFACTURING

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PH: (850) 584 - 7786

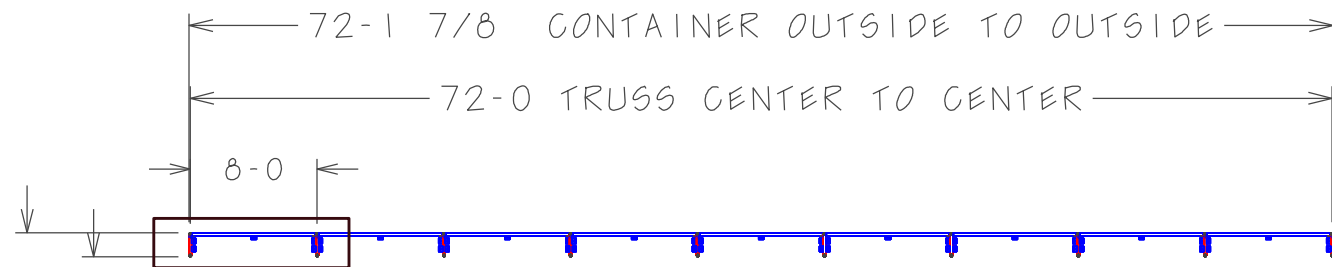
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DRAWN BY: Mo	DATE DRAWN: 5/27/21
APPROVED BY:	

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6-1-2021

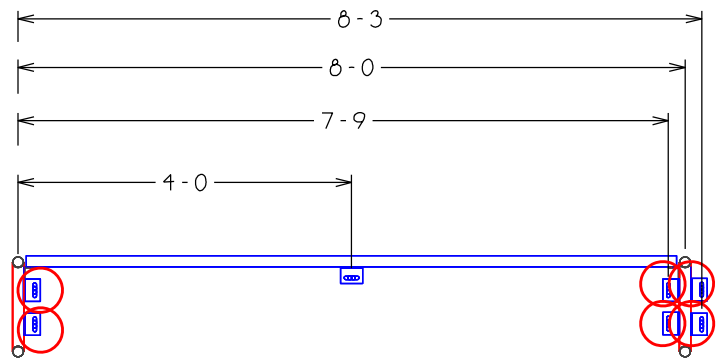
Professional Engineer
NABIL M. EL-HACHIMI
STATE OF FLORIDA
No. 66012
EXPIRES: 2/28/23
PE STAMP ONLY

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PAGE: S-8
*ALL INFORMATION IS PROPERTY OF BIG TOP MANUFACTURING INC.



50-0 TRUSS OUTSIDE TO OUTSIDE
47-0 TRUSS INSIDE TO INSIDE

SEE BLOW-UP VIEW

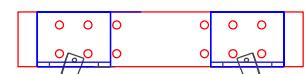
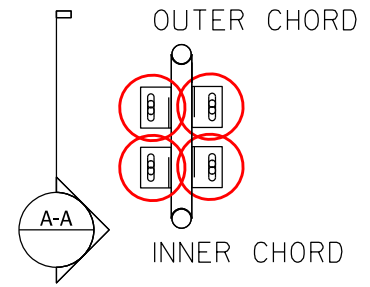


END TRUSS

SEE DETAIL A ON SHEET 5-9A

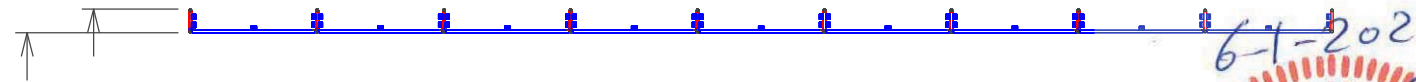
INTERMEDIATE TRUSS

ANCHORS SLOPED AT 15 DEGREES



40" SLOPED ANCHOR INCLINED AT 15 DEG

VIEW A-A



6-1-2021
All engineering to support the structure is considered "by others", unless specifically noted on our drawings. That includes, but is not limited to, shipping containers, concrete, soil, asphalt, custom support steel, etc.

FRAME - FRAME ANCHOR DETAIL

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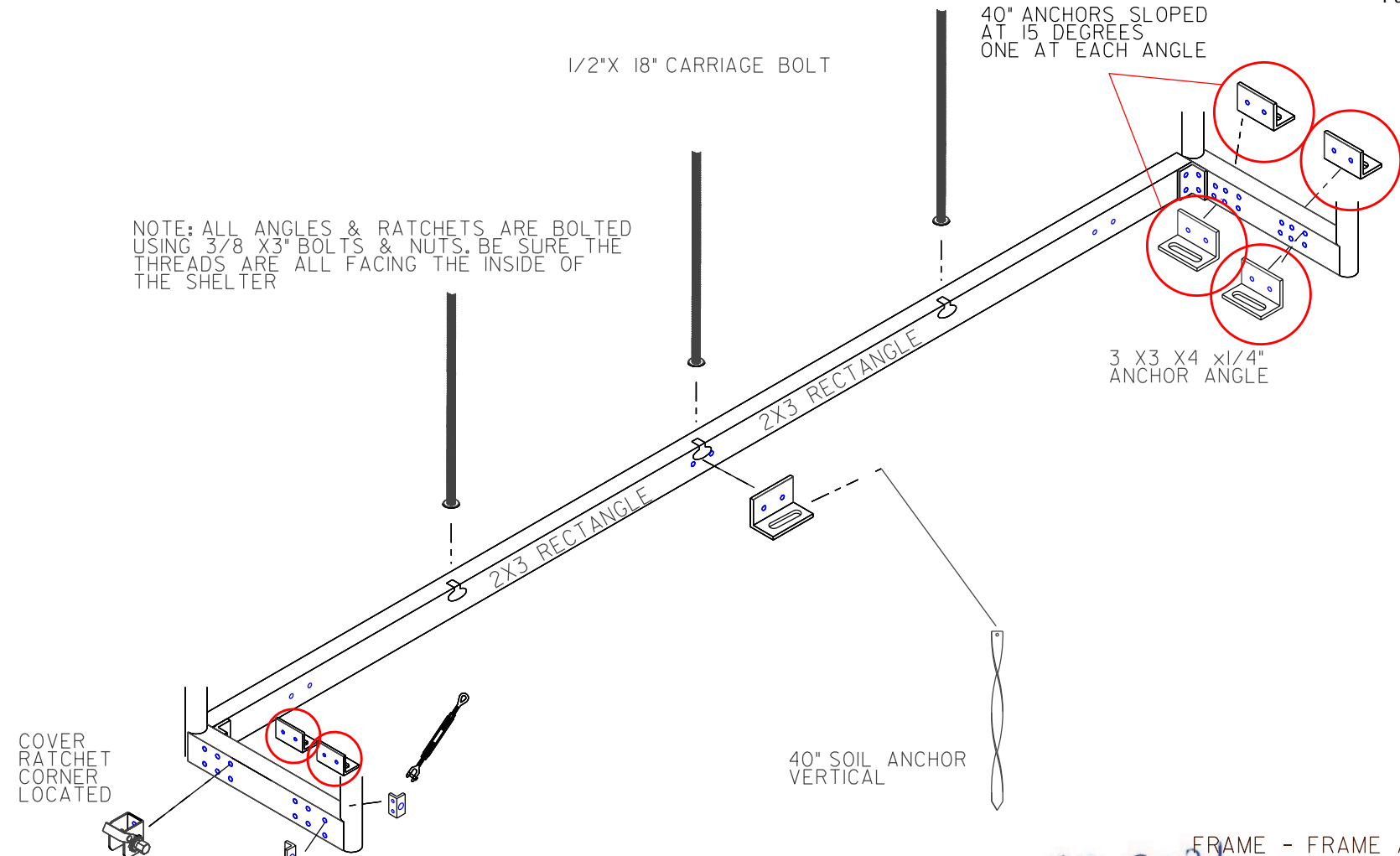
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APPROVED BY:	

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6-1-2021

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STATE OF FLORIDA
No. 86012
EXPIRES: 2/28/23
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DRAWING TYPE: ENGINEERING	
PAGE: S-9	
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NOTE: ALL ANGLES & RATCHETS ARE BOLTED USING 3/8 X3" BOLTS & NUTS. BE SURE THE THREADS ARE ALL FACING THE INSIDE OF THE SHELTER

40" ANCHORS SLOPED AT 15 DEGREES ONE AT EACH ANGLE

1/2"X 18" CARRIAGE BOLT

2X3 RECTANGLE

3 X3 X4 x1/4" ANCHOR ANGLE

40" SOIL ANCHOR VERTICAL

COVER RATCHET CORNER LOCATED

2 X2 X2 5/8 X3/8" CORNER ANGLE ONE PLACE FOR CABLE BRACING TURNBUCKLE

FRAME - FRAME ANCHOR DETAIL

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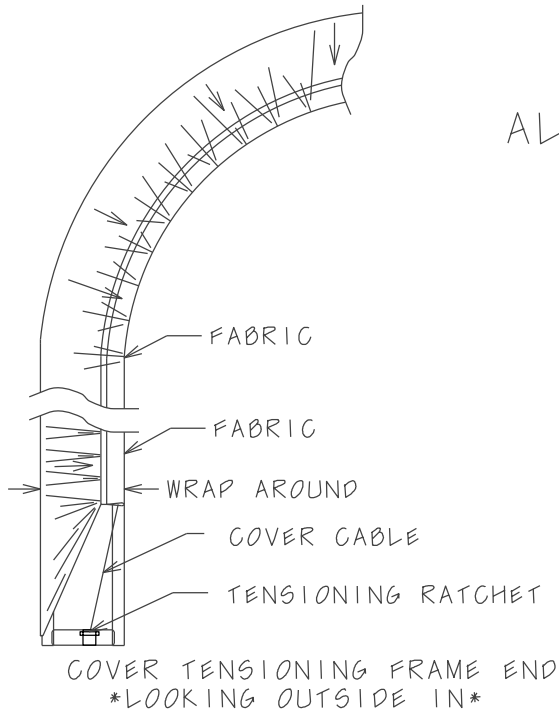
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STATE OF FLORIDA
No. 86012
EXPIRES: 2/28/23
PE - STAMP ONLY

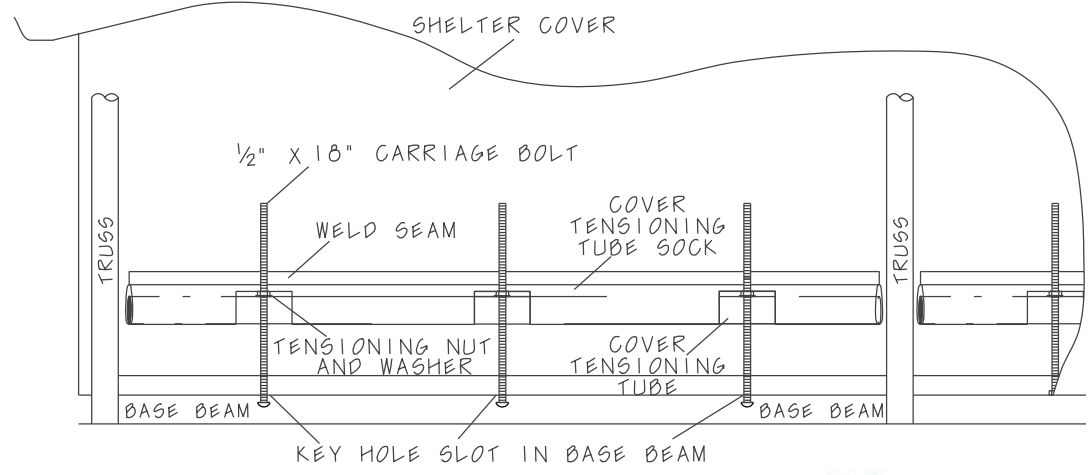
DRAWING TYPE: ENGINEERING	
PAGE:	S-9A
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FABRIC	
COLOR	4000 White
WEIGHT	18 OZ

18"

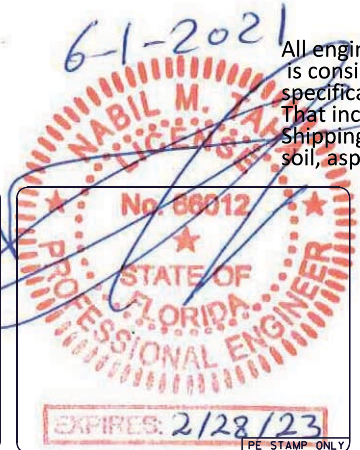


ALL-THREAD COVER TENSIONING ALONG SIDE
INSIDE LOOKING OUT



FABRIC ATTACHMENT DETAILS

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DRAWING TYPE: ENGINEERING	
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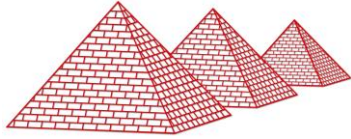
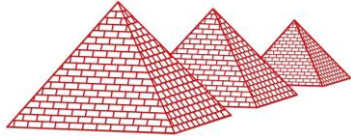


Table of Contents:

Subject:	Page:
1- References / Software:	10-19
2- Design Criteria:	100-199
3- Truss Analysis & Design – Main Truss:	1,000-1,999



References:

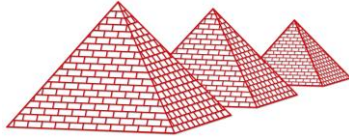
1- Literature:

2020 Edition of the Florida Building Code (7th Ed.) based on 2018 International Building Code (IBC 2018).

2- Software:

(a) **RISA-3D** Version 17.0.4

www.risa.com
26632 Towne Centre Drive, Suite 210
Foothill Ranch, CA 92610



Design Criteria:

- | | |
|-------------------|--|
| 1. Wind | Ultimate Wind speed: 110 mph (3-sec Gust) |
| | Exposure category: C |
| | Risk category: II |
| 2. Roof live load | 5 psf (Governs) |
| 3. Snow | |
| | Ground 0 psf |
| 4. Gravity loads | Self weight of truss plus 1 psf for weight of fabric and fixtures. |

**Other criteria assumed as stated in design calculations.

ATC Hazards by Location

Search Information

Address: 3266 Capital Cir SW, Tallahassee, FL 32310, USA

Coordinates: 30.39877509999999, -84.3515899

Elevation: 57 ft

Timestamp: 2021-05-27T13:18:19.993Z

Hazard Type: Wind



ASCE 7-16

MRI 10-Year 73 mph

MRI 25-Year 82 mph

MRI 50-Year 88 mph

MRI 100-Year 96 mph

Risk Category I 108 mph

Risk Category II 114 mph

Risk Category III 127 mph

Risk Category IV 128 mph

ASCE 7-10

MRI 10-Year 76 mph

MRI 25-Year 84 mph

MRI 50-Year 90 mph

MRI 100-Year 97 mph

Risk Category I 108 mph

Risk Category II 118 mph

Risk Category III-IV ... 127 mph

ASCE 7-05

ASCE 7-05 Wind Speed - 107 mph

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

Disclaimer

Hazard loads are interpolated from data provided in ASCE 7 and rounded up to the nearest whole integer. Per ASCE 7, islands and coastal areas outside the last contour should use the last wind speed contour of the coastal area – in some cases, this website will extrapolate past the last wind speed contour and therefore, provide a wind speed that is slightly higher. NOTE: For queries near wind-borne debris region boundaries, the resulting determination is sensitive to rounding which may affect whether or not it is considered to be within a wind-borne debris region.

Mountainous terrain, gorges, ocean promontories, and special wind regions shall be examined for unusual wind conditions.

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responsibility or liability for its accuracy. The material presented in the report should not be used or relied upon for any specific application without competent examination and verification of its accuracy, suitability and applicability by engineers or other licensed professionals. ATC does not intend that the use of this information replace the sound judgment of such competent professionals, having experience and knowledge in the field of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the results of the report provided by this website. Users of the information from this website assume all liability arising from such use. Use of the output of this website does not imply approval by the governing building code bodies responsible for building code approval and interpretation for the building site described by latitude/longitude location in the report.



Hazards by Location

Search Information

Address: 3266 Capital Cir SW, Tallahassee, FL 32310, USA

Coordinates: 30.39877509999999, -84.3515899

Elevation: 57 ft

Timestamp: 2021-05-27T13:24:26.896Z

Hazard Type: Snow



ASCE 7-16

ASCE 7-10

ASCE 7-05

Ground Snow Load 0 lb/sqft

Ground Snow Load 0 lb/sqft

Ground Snow Load 0 lb/sqft

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

Disclaimer

Hazard loads are interpolated from data provided in ASCE 7 and rounded up to the nearest whole integer.

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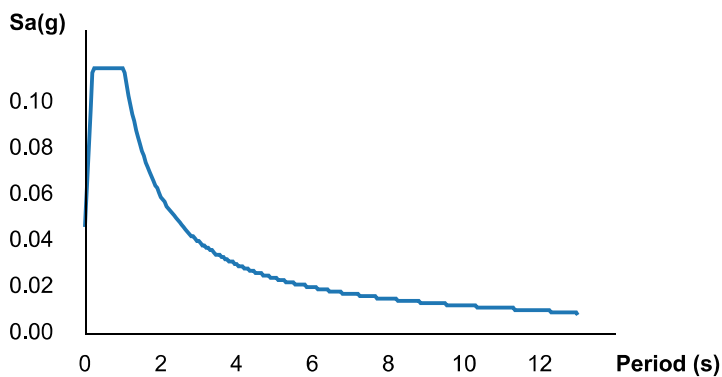
ATC Hazards by Location

Search Information

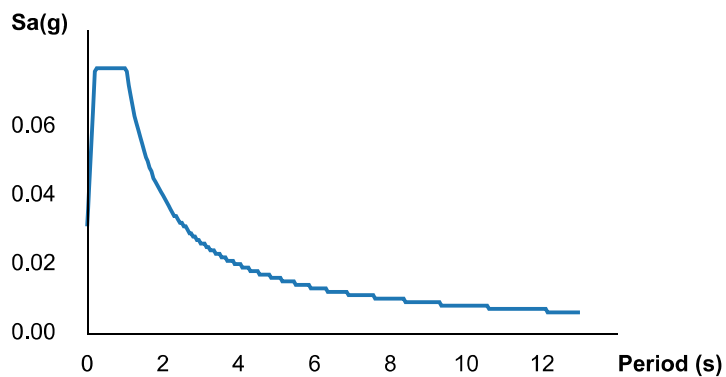
Address: 3266 Capital Cir SW, Tallahassee, FL 32310, USA
Coordinates: 30.398775099999999, -84.3515899
Elevation: 57 ft
Timestamp: 2021-05-27T13:24:39.148Z
Hazard Type: Seismic
Reference Document: ASCE7-16
Risk Category: II
Site Class: D-default



MCE_R Horizontal Response Spectrum



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	0.072	MCE _R ground motion (period=0.2s)
S ₁	0.05	MCE _R ground motion (period=1.0s)
S _{MS}	0.115	Site-modified spectral acceleration value
S _{M1}	0.119	Site-modified spectral acceleration value
S _{DS}	0.077	Numeric seismic design value at 0.2s SA
S _{D1}	0.079	Numeric seismic design value at 1.0s SA

Additional Information

Name	Value	Description
SDC	B	Seismic design category
F _a	1.6	Site amplification factor at 0.2s
F _v	2.4	Site amplification factor at 1.0s

CR _S	0.945	Coefficient of risk (0.2s)
CR ₁	0.892	Coefficient of risk (1.0s)
PGA	0.034	MCE _G peak ground acceleration
F _{PGA}	1.6	Site amplification factor at PGA
PGA _M	0.054	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	0.072	Probabilistic risk-targeted ground motion (0.2s)
SsUH	0.076	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	1.5	Factored deterministic acceleration value (0.2s)
S1RT	0.05	Probabilistic risk-targeted ground motion (1.0s)
S1UH	0.056	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	0.6	Factored deterministic acceleration value (1.0s)
PGAd	0.5	Factored deterministic acceleration value (PGA)

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

Disclaimer

Hazard loads are provided by the U.S. Geological Survey [Seismic Design Web Services](#).

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Big Top Seismic Forces

Ss =	<input type="text" value="0.072"/>	g	Sms =	<input type="text" value="0.153"/>	g	Sds =	<input type="text" value="0.102"/>	g
S1 =	<input type="text" value="0.050"/>	g	Sm1 =	<input type="text" value="0.128"/>	g	Sd1 =	<input type="text" value="0.085"/>	g
Site Class	<input type="text" value="D"/>		Risk Category	<input type="text" value="II"/>		R =	<input type="text" value="3"/>	
Importance Factor =	<input type="text" value="1"/>		T =	<input type="text" value="0.21"/>	seconds			
Sds Seismic Cat.	<input type="text" value="A"/>		Seismic Cat =	<input type="text" value="B"/>				
Sd1 Seismic Cat.	<input type="text" value="B"/>							
Truss Dimensions			Width =	<input type="text" value="50"/>	ft	Fabric DL =	<input type="text" value="0.25"/>	psf
			Length =	<input type="text" value="72"/>		Truss DL =	<input type="text" value="0.75"/>	psf
			Height =	<input type="text" value="23"/>		Add. DL =	<input type="text" value="0"/>	psf
			Total Weight =		<input type="text" value="5.753"/>	kips		
Cs =	<input type="text" value="0.034"/>							
Cs min =	<input type="text" value="0.0045"/>							
Cs max =	<input type="text" value="0.1349"/>							
Use Cs =	<input type="text" value="0.034"/>							
V = Cs x W =	<input type="text" value="0.1956"/>	kips						
V per truss =	<input type="text" value="0.0033"/>	kips < reactions due to wind. Hence wind design governs						



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PREFACE

▶ CHAPTER 1 SCOPE AND
ADMINISTRATION

▶ CHAPTER 2 DEFINITIONS

▶ CHAPTER 3 USE AND
OCCUPANCY CLASSIFICATION

▶ CHAPTER 4 SPECIAL DETAILED
REQUIREMENTS BASED ON
OCCUPANCY AND USE

▶ CHAPTER 5 GENERAL BUILDING
HEIGHTS AND AREAS

About this Title

The 7th Edition (2020) update to the Florida Building Code: Building is a fully integrated publication that updates the 6th Edition 2017 Florida Building Code: Building using the latest changes to the 2018 International Building Code® with customized amendments adopted statewide. Chapter tabs are also included. Effective Date: December 31, 2020

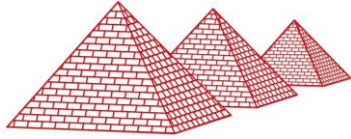
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PSE CONSULTING ENGINEERS INC.

TRUSS ANALYSIS & DESIGN – MAIN TRUSS:

Pages 1,000 - 1,999

Calculations Prepared by:

Date: May 26, 2021

File Location:

F:\Engineering Department\2021 Projects\
 Big Top 221-80 50x72x23 DEM 18BB - Tallahassee, FL\Dsg Engineering\Admin\
 7-1 Meca Wind.wnd

Basic Wind Parameters

Wind Load Standard = ASCE 7-16 Exposure Category = C
 Wind Design Speed = 110.0 mph Risk Category = II
 Structure Type = Building Building Type = Enclosed

General Wind Settings

Incl_LF = Include ASD Load Factor of 0.6 in Pressures = False
 DynType = Dynamic Type of Structure = Rigid
 NF = Natural Frequency of Structure (Mode 1) = 1.000 Hz
 Zg = Altitude (Ground Elevation) above Sea Level = 0.000 ft
 Bdist = Base Elevation of Structure = 0.000 ft
 SDB = Simple Diaphragm Building = False
 MWFRSType = MWFRS Method Selected = Ch 27 Pt 1

Topographic Factor per Fig 26.8-1

Topo = Topographic Feature = None
 Kzt = Topographic Factor = 1.000

Building Inputs

Roof: Building Roof Type = Arched EHT : Eave Height = 15.229 ft
 R : Enter Radius of Arch = 44.100 ft W : Building Width = 50.000 ft
 L : Building Length = 72.000 ft

Exposure Constants per Table 26.11-1:

Alpha: Const from Table 26.11-1= 9.500 Zg: Const from Table 26.11-1= 900.000 ft
 At: Const from Table 26.11-1= 0.105 Bt: Const from Table 26.11-1= 1.000
 Am: Const from Table 26.11-1= 0.154 Bm: Const from Table 26.11-1= 0.650
 C: Const from Table 26.11-1= 0.200 Eps: Const from Table 26.11-1= 0.200

Overhang Inputs:

Std = Overhangs on all sides are the same = True
 OHType = Type of Roof Wall Intersections = None

Main Wind Force Resisting System (MWFRS) Calculations per Ch 27 Part 1:

h = Mean Roof Height above grade = 19.114 ft
 Kh = 15 ft [4.572 m] < Z < Zg --> $(2.01 * (Z/zg)^{(2/\text{Alpha})})$ {Table 26.10-1} = 0.893
 Kzt = Topographic Factor is 1 since no Topographic feature specified = 1.000
 Kd = Wind Directionality Factor per Table 26.6-1 = 0.85
 Zg = Elevation above Sea Level = 0.000 ft
 Ke = Ground Elevation Factor: $Ke = e^{-(0.0000362 * Zg)}$ {Table 26.9-1} = 1.000
 GCPi = Ref Table 26.13-1 for Enclosed Building = +/-0.18
 RA = Roof Area = 3826.67 sq ft
 LF = Load Factor based upon STRENGTH Design = 1.00
 qh = $(0.00256 * Kh * Kzt * Kd * Ke * V^2) * LF$ = 23.52 psf
 qin = For Negative Internal Pressure of Enclosed Building use qh*LF = 23.52 psf
 qip = For Positive Internal Pressure of Enclosed Building use qh*LF = 23.52 psf

Gust Factor Calculation:

Gust Factor Category I Rigid Structures - Simplified Method
 G1 = For Rigid Structures (Nat. Freq.>1 Hz) use 0.85 = 0.85
 Gust Factor Category II Rigid Structures - Complete Analysis
 Zm = 0.6 * Ht = 15.000 ft
 Izm = $Cc * (33 / Zm) ^ 0.167$ = 0.228
 Lzm = $L * (Zm / 33) ^ \text{Epsilon}$ = 427.057
 Q = $(1 / (1 + 0.63 * ((B + Ht) / Lzm)^{0.63}))^{0.5}$ = 0.913
 G2 = $0.925 * ((1 + 1.7 * lzm^{3.4} * Q) / (1 + 1.7 * 3.4 * lzm))$ = 0.879
 Gust Factor Used in Analysis
 G = Lessor Of G1 Or G2 = 0.850

MWFRS Wind Normal to Ridge (Ref Fig 27.3-1)

h = Mean Roof Height Of Building = 19.114 ft
 RHt = Ridge Height Of Roof = 23.000 ft
 B = Horizontal Dimension Of Building Normal To Wind Direction = 72.000 ft
 L = Horizontal Dimension Of building Parallel To Wind Direction = 50.000 ft
 L/B = Ratio Of L/B used For Cp determination = 0.694
 h/L = Ratio Of h/L used For Cp determination = 0.382
 RHt = Ridge Height Of Roof = 23.000 ft

r = Rise To Span Ratio (RHt-EHt)/W = 0.155
 Elev = Is roof on Elevated Structure (Is EHT>0) = True
 Roof_CH = Roof Coefficient Center Half = -0.855, -0.855
 Roof_LQ = Roof Coefficient Leeward Quarter = -0.5, -0.5
 Roof_WQ = Roof Coefficient Windward Quarter = -0.9, -0.9

 Cp_WW = Windward Wall Coefficient (All L/B Values) = 0.80
 Cp_LW = Leeward Wall Coefficient using L/B = -0.50
 Cp_SW = Side Wall Coefficient (All L/B values) = -0.70
 GCpn_WW = Parapet Combined Net Pressure Coefficient (Windward Parapet) = 1.50
 GCpn_LW = Parapet Combined Net Pressure Coefficient (Leeward Parapet) = -1.00

Wall Wind Pressures based On Positive Internal Pressure (+GCPi) - Normal to Ridge
 All wind pressures include a load factor of 1.0

Elev	Kz	Kzt	qz	GCPi	Windward Press	Leeward Press	Side Press	Total Press	Minimum Pressure*
ft			psf		psf	psf	psf	psf	psf
19.11	0.893	1.000	23.52	0.18	11.76	-14.23	-18.23	25.99	16.00
15.23	0.852	1.000	22.42	0.18	11.01	-14.23	-18.23	25.24	16.00

Wall Wind Pressures based on Negative Internal Pressure (-GCPi) - Normal to Ridge
 All wind pressures include a load factor of 1.0

Elev	Kz	Kzt	qz	GCPi	Windward Press	Leeward Press	Side Press	Total Press	Minimum Pressure*
ft			psf		psf	psf	psf	psf	psf
19.11	0.893	1.000	23.52	-0.18	20.23	-5.76	-9.76	25.99	16.00
15.23	0.852	1.000	22.42	-0.18	19.48	-5.76	-9.76	25.24	16.00

Notes Wall Pressures:

Kz = Velocity Press Exp Coeff Kzt = Topographical Factor
 qz = $0.00256 * Kz * Kzt * Kd * V^2$ GCpi = Internal Press Coefficient
 Side = $qh * G * Cp_{SW} - qip * +GCpi$ Windward = $qz * G * Cp_{WW} - qip * +GCpi$
 Leeward = $qh * G * Cp_{LW} - qip * +GCpi$ Total = Windward Press - Leeward Press
 * Minimum Pressure: Para 27.1.5 no less than 16.00 psf (Incl LF) applied to Walls
 + Pressures Acting TOWARD Surface - Pressures Acting AWAY from Surface

Roof Wind Pressures for Positive & Negative Internal Pressure (+/- GCpi) - Normal to Ridge
 All wind pressures include a load factor of 1.0

Roof Var	Start Dist	End Dist	Cp_min	Cp_max	GCpi	Pressure Pn_min*	Pressure Pp_min*	Pressure Pn_max	Pressure Pp_max
	ft	ft				psf	psf	psf	psf
Roof_CH	N/A	N/A	-0.855	-0.855	0.180	-12.87	-21.34	-12.87	-21.34
Roof_LQ	N/A	N/A	-0.500	-0.500	0.180	-5.76	-14.23	-5.76	-14.23
Roof_WQ	N/A	N/A	-0.900	-0.900	0.180	-13.76	-22.23	-13.76	-22.23

Notes Roof Pressures:

Start Dist = Start Dist from Windward Edge End Dist = End Dist from Windward Edge
 Cp_Max = Largest Coefficient Magnitude Cp_Min = Smallest Coefficient Magnitude
 Pp_max = $qh * G * Cp_{max} - qip * (+GCpi)$ Pn_max = $qh * G * Cp_{max} - qin * (-GCpi)$
 Pp_min* = $qh * G * Cp_{min} - qip * (+GCpi)$ Pn_min* = $qh * G * Cp_{min} - qin * (-GCpi)$
 OH = Overhang X = Dir along Ridge Y = Dir Perpendicular to Ridge Z = Vertical
 * The smaller uplift pressures due to Cp_Min can become critical when wind is combined with roof live load or snow load; load combinations are given in ASCE 7
 + Pressures Acting TOWARD Surface - Pressures Acting AWAY from Surface

MWFRS Wind Parallel to Ridge (Ref Fig 27.3-1)

h = Mean Roof Height Of Building = 19.114 ft
 RHt = Ridge Height Of Roof = 23.000 ft
 B = Horizontal Dimension Of Building Normal To Wind Direction = 50.000 ft
 L = Horizontal Dimension Of building Parallel To Wind Direction = 72.000 ft
 L/B = Ratio Of L/B used For Cp determination = 1.440
 h/L = Ratio Of h/L used For Cp determination = 0.265
 RHt = Ridge Height Of Roof = 23.000 ft
 r = Rise To Span Ratio (RHt-EHt)/W = 0.155
 Elev = Is roof on Elevated Structure (Is EHT>0) = True
 Roof_1 = Roof Coeff (0 to h) (0.000 ft to 19.114 ft) = -0.18, -0.9
 Roof_2 = Roof Coeff (h to 2h) (19.114 ft to 38.229 ft) = -0.18, -0.5
 Roof_3 = Roof Coeff (>2h) (>38.229 ft) = -0.18, -0.3

 Cp_WW = Windward Wall Coefficient (All L/B Values) = 0.80
 Cp_LW = Leeward Wall Coefficient using L/B = -0.41

Cp_SW = Side Wall Coefficient (All L/B values) = -0.70
 GCpn_WW = Parapet Combined Net Pressure Coefficient (Windward Parapet) = 1.50
 GCpn_LW = Parapet Combined Net Pressure Coefficient (Leeward Parapet) = -1.00

Wall Wind Pressures based On Positive Internal Pressure (+GCPi) - Parallel to Ridge
 All wind pressures include a load factor of 1.0

Elev	Kz	Kzt	qz	GCPi	Windward Press	Leeward Press	Side Press	Total Press	Minimum Pressure*
ft			psf		psf	psf	psf	psf	psf
23.00	0.929	1.000	24.46	0.18	12.40	-12.47	-18.23	24.87	16.00
19.11	0.893	1.000	23.52	0.18	11.76	-12.47	-18.23	24.23	16.00
15.23	0.852	1.000	22.42	0.18	11.01	-12.47	-18.23	23.48	16.00

Wall Wind Pressures based on Negative Internal Pressure (-GCPi) - Parallel to Ridge
 All wind pressures include a load factor of 1.0

Elev	Kz	Kzt	qz	GCPi	Windward Press	Leeward Press	Side Press	Total Press	Minimum Pressure*
ft			psf		psf	psf	psf	psf	psf
23.00	0.929	1.000	24.46	-0.18	20.86	-4.00	-9.76	24.87	16.00
19.11	0.893	1.000	23.52	-0.18	20.23	-4.00	-9.76	24.23	16.00
15.23	0.852	1.000	22.42	-0.18	19.48	-4.00	-9.76	23.48	16.00

Notes Wall Pressures:

Kz = Velocity Press Exp Coeff
 Kzt = Topographical Factor
 qz = $0.00256 * Kz * Kzt * Kd * V^2$
 GCPi = Internal Press Coefficient
 Side = $q_h * G * Cp_{SW} - q_{ip} * +GCPi$
 Windward = $q_z * G * Cp_{WW} - q_{ip} * +GCPi$
 Leeward = $q_h * G * Cp_{LW} - q_{ip} * +GCPi$
 Total = Windward Press - Leeward Press
 * Minimum Pressure: Para 27.1.5 no less than 16.00 psf (Incl LF) applied to Walls
 + Pressures Acting TOWARD Surface
 - Pressures Acting AWAY from Surface

Roof Wind Pressures for Positive & Negative Internal Pressure (+/- GCPi) - Parallel to Ridge
 All wind pressures include a load factor of 1.0

Roof Var	Start Dist	End Dist	Cp_min	Cp_max	GCPi	Pressure Pn_min*	Pressure Pp_min*	Pressure Pn_max	Pressure Pp_max
	ft	ft				psf	psf	psf	psf
Roof_1	0.000	19.114	-0.180	-0.900	0.180	0.64	-7.83	-13.76	-22.23
Roof_2	19.114	38.229	-0.180	-0.500	0.180	0.64	-7.83	-5.76	-14.23
Roof_3	38.229	72.000	-0.180	-0.300	0.180	0.64	-7.83	-1.76	-10.23

Notes Roof Pressures:

Start Dist = Start Dist from Windward Edge
 End Dist = End Dist from Windward Edge
 Cp_Max = Largest Coefficient Magnitude
 Cp_Min = Smallest Coefficient Magnitude
 Pp_max = $q_h * G * Cp_{max} - q_{ip} * (+GCPi)$
 Pn_max = $q_h * G * Cp_{max} - q_{in} * (-GCPi)$
 Pp_min* = $q_h * G * Cp_{min} - q_{ip} * (+GCPi)$
 Pn_min* = $q_h * G * Cp_{min} - q_{in} * (-GCPi)$
 OH = Overhang X = Dir along Ridge Y = Dir Perpendicular to Ridge Z = Vertical
 * The smaller uplift pressures due to Cp_Min can become critical when wind is combined with roof live load or snow load; load combinations are given in ASCE 7
 + Pressures Acting TOWARD Surface
 - Pressures Acting AWAY from Surface

Job: _____

Designer: _____
Date: _____

Tributary Width = 8 ft

Dead Load

DL =	1	psf	x	8	ft	=	8	plf
------	---	-----	---	---	----	---	---	-----

Roof Live Load

RLL =	5	psf	x	8	ft	=	40	plf
-------	---	-----	---	---	----	---	----	-----

Wind Loads

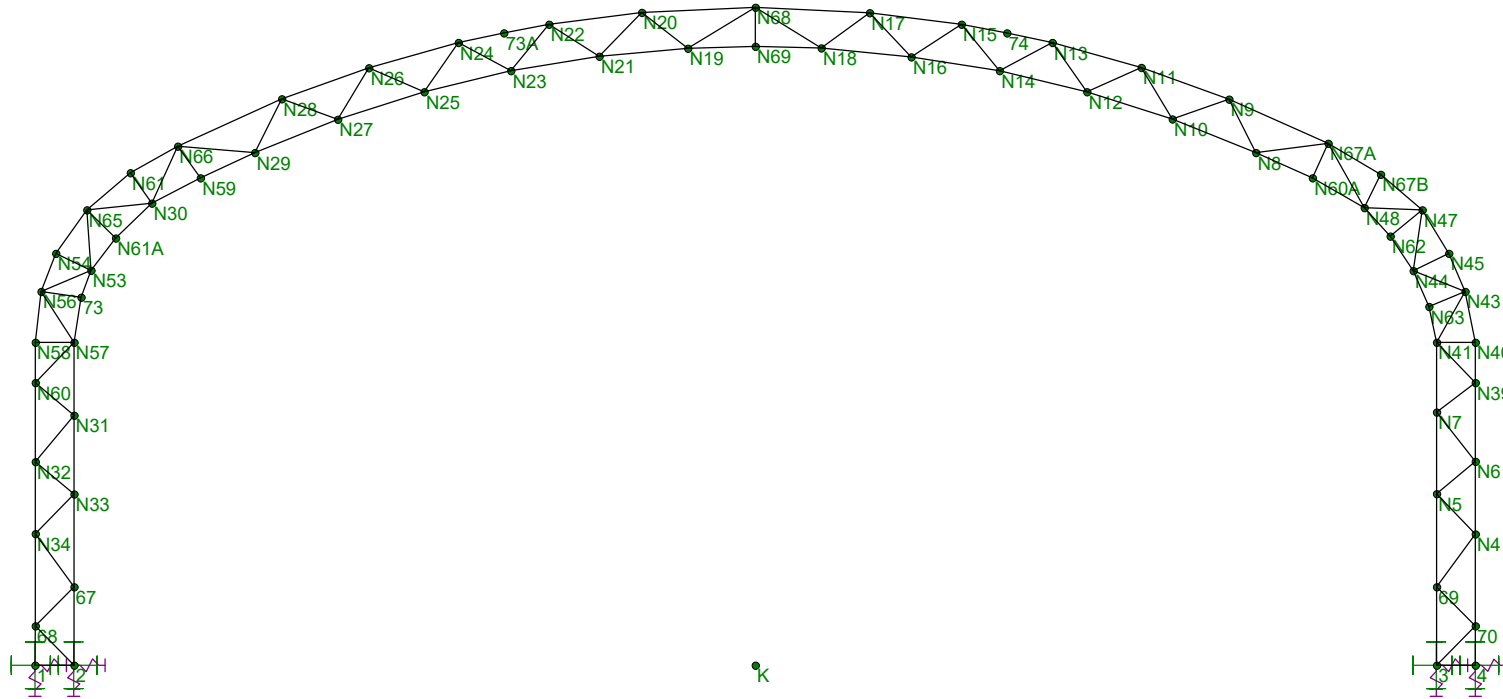
Wind Speed: 110 mph

Walls:

+GC _{pi}	Windward	11.76	psf	x	8	ft	=	94.08	plf
	Leeward	-14.23	psf	x	8	ft	=	-113.84	plf
-GC _{pi}	Windward	20.23	psf	x	8	ft	=	161.84	plf
	Leeward	-5.76	psf	x	8	ft	=	-46.08	plf

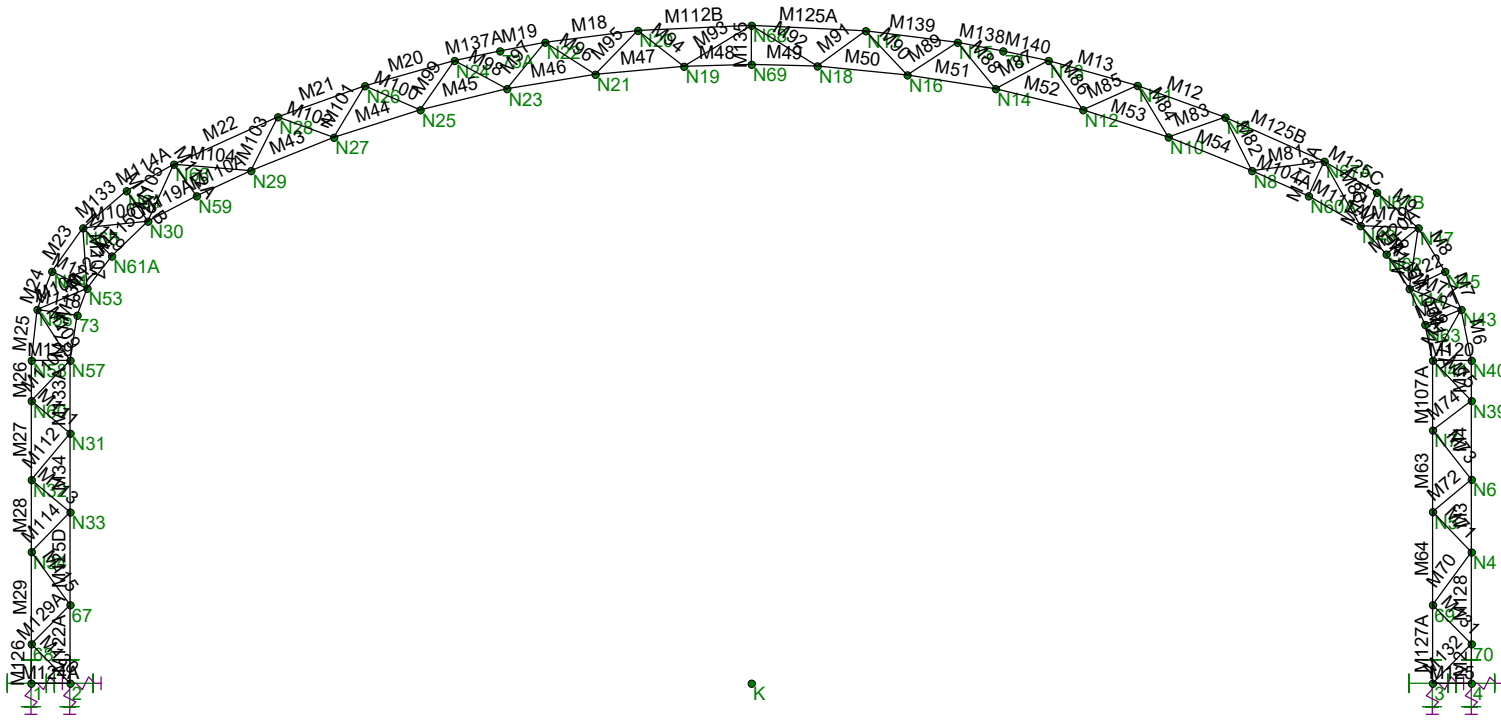
Roof:

+GC _{pi}	Windward Quarter	-22.23	psf	x	8	ft	=	-177.84	plf
	Center Half	-21.34	psf	x	8	ft	=	-170.7	plf
	Leeward Quarter	-14.23	psf	x	8	ft	=	-113.84	plf
-GC _{pi}	Windward Quarter	-13.76	psf	x	8	ft	=	-110.08	plf
	Center Half	-12.87	psf	x	8	ft	=	-102.96	plf
	Leeward Quarter	-5.76	psf	x	8	ft	=	-46.08	plf



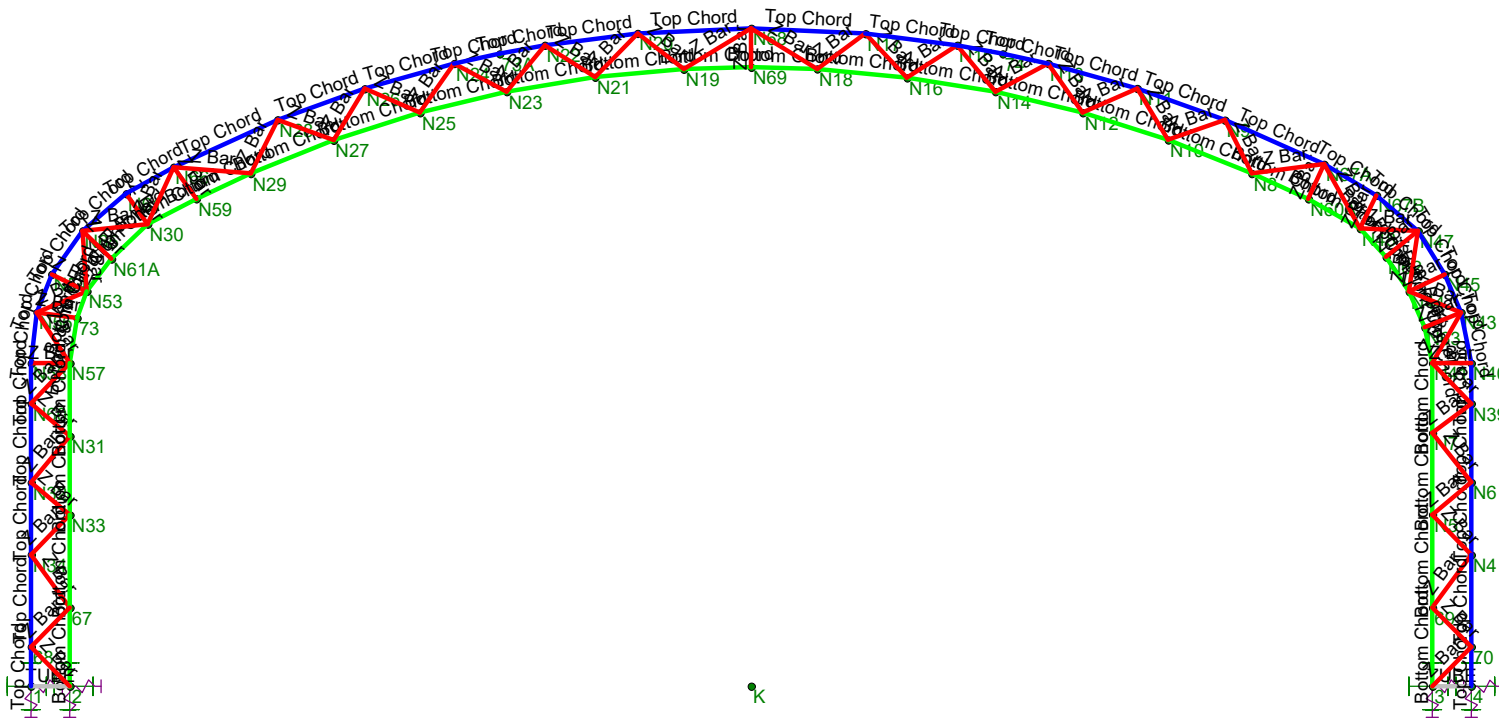
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 Reaction and Moment Units are k and k-ft (Enveloped)

Big Top	50x72x23 DEM 18BB - Tallahassee, FL	SK - 1
Mo		May 27, 2021 at 10:41 AM
221-80		50x72x23 DEM 18BB - Tallahassee, FL.r3d



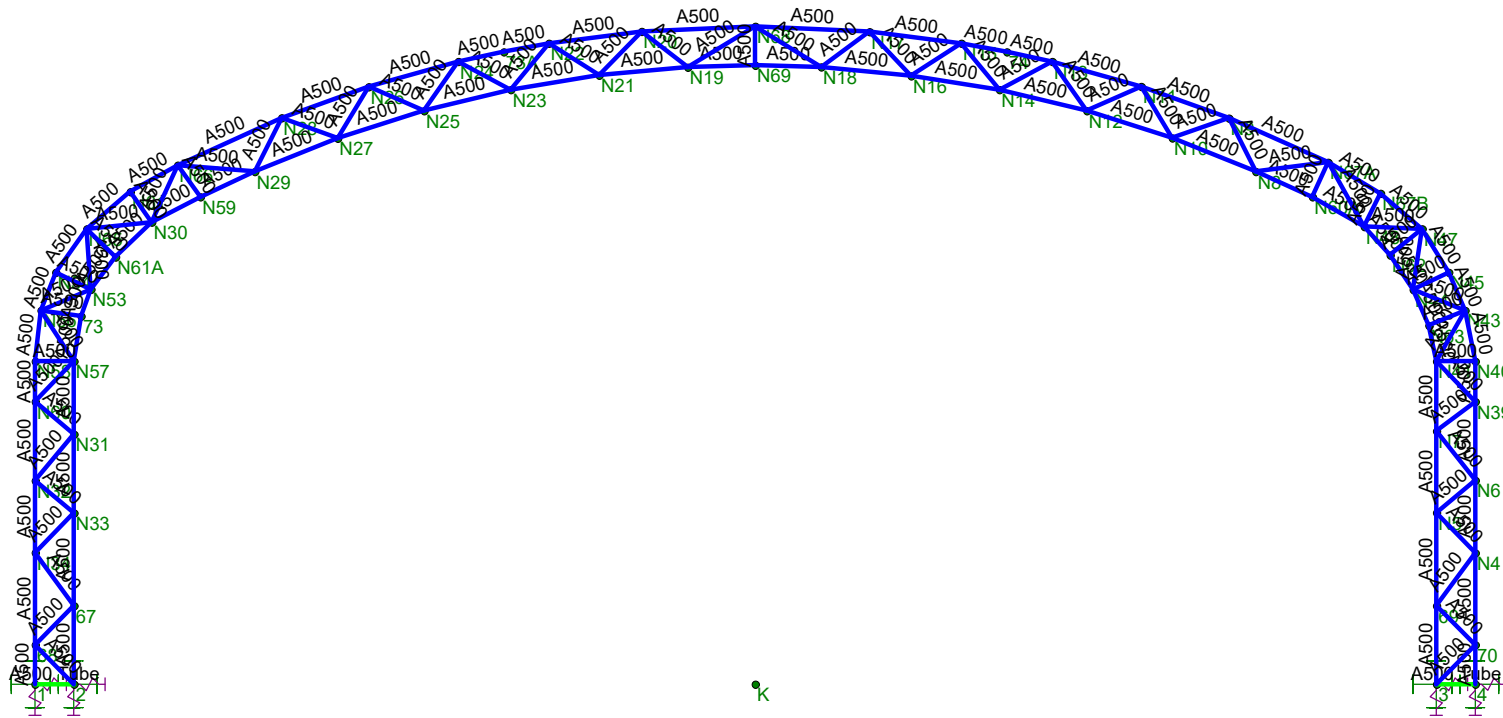
Envelope Only Solution
 Reaction and Moment Units are k and k-ft (Enveloped)

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Mo		May 27, 2021 at 10:41 AM
221-80		50x72x23 DEM 18BB - Tallahassee, FL.r3d



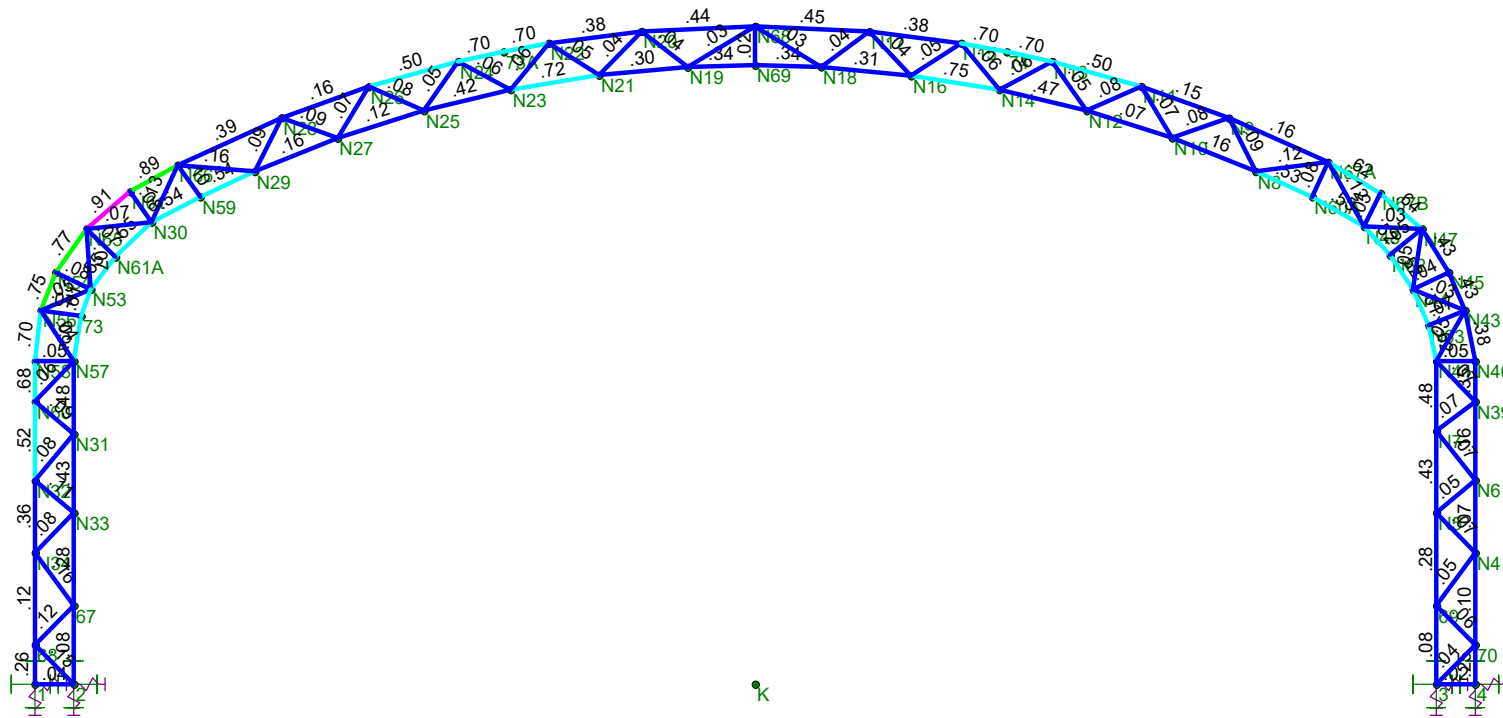
Envelope Only Solution
 Reaction and Moment Units are k and k-ft (Enveloped)

Big Top	50x72x23 DEM 18BB - Tallahassee, FL	SK - 3
Mo		May 27, 2021 at 10:41 AM
221-80		50x72x23 DEM 18BB - Tallahassee, FL.r3d



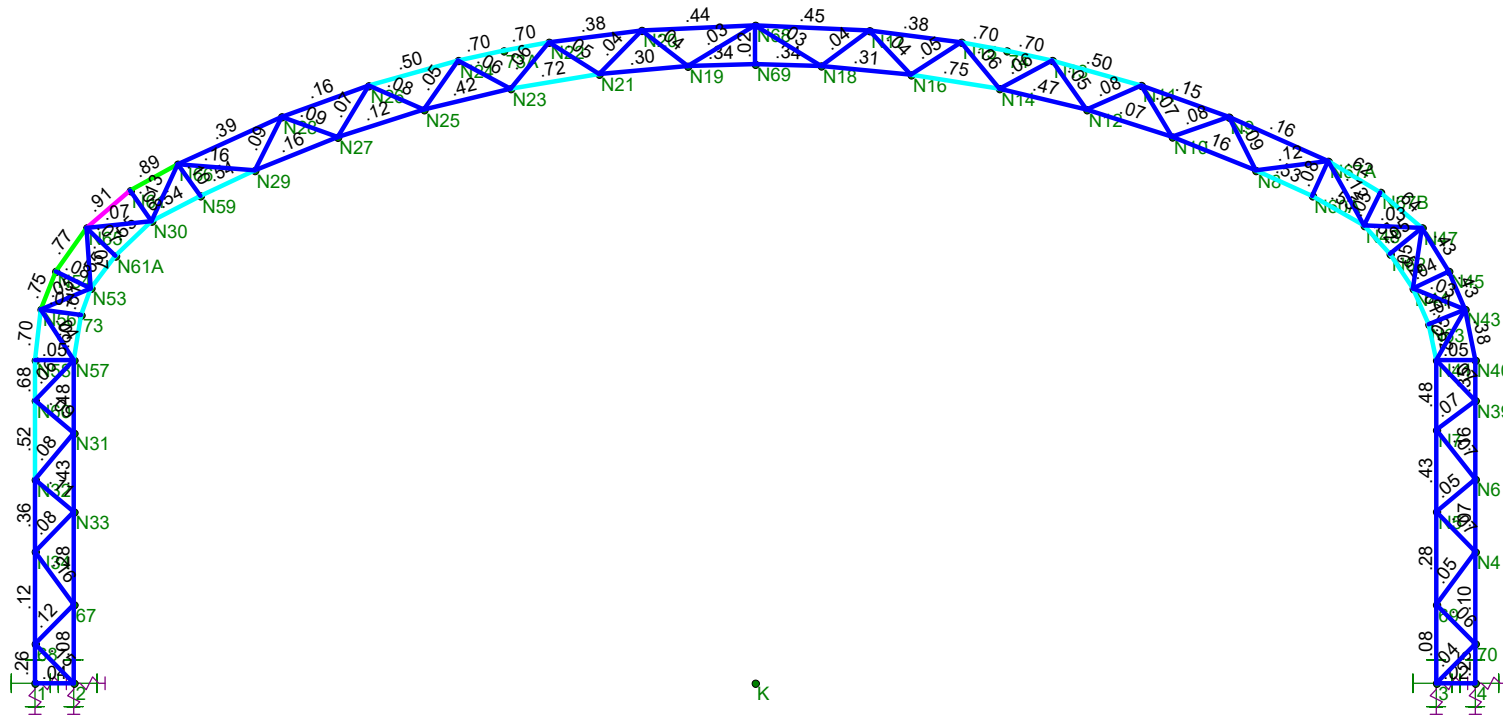
Envelope Only Solution
 Reaction and Moment Units are k and k-ft (Enveloped)

Big Top	50x72x23 DEM 18BB - Tallahassee, FL	SK - 4
Mo		May 27, 2021 at 10:41 AM
221-80		50x72x23 DEM 18BB - Tallahassee, FL.r3d



Member Code Checks Displayed (Enveloped)
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Big Top	50x72x23 DEM 18BB - Tallahassee, FL	SK - 5
Mo		May 27, 2021 at 10:41 AM
221-80		50x72x23 DEM 18BB - Tallahassee, FL.r3d



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 Envelope Only Solution
 Reaction and Moment Units are k and k-ft (Enveloped)

Big Top	50x72x23 DEM 18BB - Tallahassee, FL	SK - 6
Mo		May 27, 2021 at 10:42 AM
221-80		50x72x23 DEM 18BB - Tallahassee, FL.r3d



Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm (/1E...	Density[k/ft...	Yield[ksi]	Ry	Fu[ksi]	Rt
1	A36 Gr.36	29000	11154	.3	.65	.49	36	1.5	58	1.2
2	A572 Gr.50	29000	11154	.3	.65	.49	50	1.1	65	1.1
3	A992	29000	11154	.3	.65	.49	50	1.1	65	1.1
4	A500 Gr.B RND	29000	11154	.3	.65	.527	42	1.4	58	1.3
5	A500 Gr.B Rect	29000	11154	.3	.65	.527	46	1.4	58	1.3
6	A53 Gr.B	29000	11154	.3	.65	.49	35	1.6	60	1.2
7	A1085	29000	11154	.3	.65	.49	50	1.4	65	1.3
8	A500	29000	11154	.3	.65	.49	55	1.5	60	1.2
9	A500 Tube	29000	11154	.3	.65	.49	50	1.5	55	1.2

Hot Rolled Steel Section Sets

	Label	Shape	Type	Design List	Material	Design Rul...	A [in2]	Iyy [in4]	Izz [in4]	J [in4]
1	Top Chord	1.9x0.09	Beam	pipe	A500	Typical	.512	.21	.21	.42
2	Bottom Ch...	1.9x0.09	Beam	pipe	A500	Typical	.512	.21	.21	.42
3	Z Bar	1.66" x 0.085"	Beam	pipe	A500	Typical	.421	.131	.131	.262
4	TUBE	2" x 3" x 0.085_HRA	Beam	Tube	A500 Tube	Typical	.821	.555	1.044	1.599

Joint Coordinates and Temperatures

	Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Diaphragm
1	4	0	0	0	0	
2	N4	0	4.54402	0	0	
3	N5	0	5.937425	1.342617	0	
4	N6	0	7.062501	.000208	0	
5	N7	0	8.763718	1.342617	0	
6	N8	0	17.744401	7.597053	0	
7	N9	0	19.597085	8.528475	0	
8	N10	0	18.906915	10.492788	0	
9	N11	0	20.687479	11.560188	0	
10	N12	0	19.84965	13.448197	0	
11	N13	0	21.548065	14.642898	0	
12	N14	0	20.575947	16.468847	0	
13	N15	0	22.183845	17.789965	0	
14	N16	0	21.059978	19.53114	0	
15	N17	0	22.587854	20.969305	0	
16	N18	0	21.360603	22.634184	0	
17	N19	0	21.358088	27.253696	0	
18	N20	0	22.590051	28.847784	0	
19	N21	0	21.078546	30.321601	0	
20	N22	0	22.18268	32.058638	0	
21	N23	0	20.57353	33.384614	0	
22	N24	0	21.548065	35.198617	0	
23	N25	0	19.851642	36.386185	0	
24	N26	0	20.683322	38.294359	0	
25	N27	0	18.900269	39.367195	0	
26	N28	0	19.599048	41.308151	0	
27	N29	0	17.748948	42.234232	0	
28	N30	0	15.989399	45.80603	0	
29	N31	0	8.652807	48.497462	0	
30	N32	0	7.050734	49.841307	0	
31	N33	0	5.932535	48.497462	0	
32	N34	0	4.549053	49.841369	0	
33	1	0	0	49.841432	0	
34	N39	0	9.778993	0	0	



Joint Coordinates and Temperatures (Continued)

	Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Diaphragm
35	N40	0	11.179751	-0.000415	0	
36	N41	0	11.17937	1.342617	0	
37	N43	0	12.934971	0.356554	0	
38	N44	0	13.658254	2.154954	0	
39	N45	0	14.25	0.921186	0	
40	N47	0	15.757562	1.845699	0	
41	N48	0	15.8434	3.846632	0	
42	N53	0	13.664443	47.913487	0	
43	N54	0	14.249955	49.123036	0	
44	N56	0	12.934971	49.638676	0	
45	N57	0	11.179699	48.497462	0	
46	N58	0	11.179699	49.841212	0	
47	N60	0	9.784097	49.841244	0	
48	N65	0	15.757562	48.0546	0	
49	N66	0	17.962567	44.907439	0	
50	N68	0	22.765704	24.920758	0	
51	N69	0	21.421954	24.920758	0	
52	K	0	0	24.92004	0	
53	N59	0	16.864173	44.120131	0	
54	N60A	0	16.864173	5.641548	0	
55	N61	0	17.05	46.55	0	
56	N61A	0	14.791921	47.059759	0	
57	N62	0	14.856672	2.950499	0	
58	N63	0	12.422071	1.608786	0	
59	2	0	0	48.497462	0	
60	3	0	0	1.342617	0	
61	N67A	0	18.06927	5.093754	0	
62	N67B	0	16.990064	3.280432	0	
63	67	0	2.72027	48.497462	0	
64	68	0	1.360135	49.8414	0	
65	69	0	2.72027	1.342617	0	
66	70	0	1.360135	0	0	
67	73	0	12.7389	48.25	0	
68	73A	0	21.89	33.628627	0	
69	74	0	21.89	16.216432	0	

Joint Boundary Conditions

	Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]
1	1	Reaction	S40	S40		Reaction	Reaction
2	2	Reaction	S40	S40		Reaction	Reaction
3	3	Reaction	S40	S40		Reaction	Reaction
4	4	Reaction	S40	S40		Reaction	Reaction

Hot Rolled Steel Design Parameters

	Label	Shape	Length[ft]	Lbyy[ft]	Lbzz[ft]	Lcomp top[ft]	Lcomp bot[ft]	L-torqu...	Kyy	Kzz	Cb	Function
1	M43	Bottom Chord	3.09	8.8		8.8	8.8	8.8	.7	.7		Lateral
2	M44	Bottom Chord	3.129	10.9		10.9	10.9	10.9	.7	.7		Lateral
3	M45	Bottom Chord	3.087	10.9		10.9	10.9	10.9	.7	.7		Lateral
4	M46	Bottom Chord	3.104	10.9		10.9	10.9	10.9	.7	.7		Lateral
5	M47	Bottom Chord	3.081	4.7		4.7	4.7	4.7	.7	.7		Lateral
6	M48	Bottom Chord	2.334	4.7		4.7	4.7	4.7	.7	.7		Lateral
7	M49	Bottom Chord	2.287	4.7		4.7	4.7	4.7	.7	.7		Lateral
8	M50	Bottom Chord	3.118	4.7		4.7	4.7	4.7	.7	.7		Lateral
9	M51	Bottom Chord	3.1	10.9		10.9	10.9	10.9	.7	.7		Lateral



Hot Rolled Steel Design Parameters (Continued)

Label	Shape	Length[ft]	Lby[ft]	Lbz[ft]	Lcomp top[ft]	Lcomp bot[ft]	L-torqu...	Kyy	Kzz	Cb	Function
10	M52	Bottom Chord	3.107	10.9		10.9	10.9	10.9	.7	.7	Lateral
11	M53	Bottom Chord	3.102	10.9		10.9	10.9	10.9	.7	.7	Lateral
12	M54	Bottom Chord	3.12	8.8		8.8	8.8	8.8	.7	.7	Lateral
13	M104A	Bottom Chord	2.144	8.8		8.8	8.8	8.8	.7	.7	Lateral
14	M110A	Bottom Chord	2.083	8.8		8.8	8.8	8.8	.7	.7	Lateral
15	M34	Bottom Chord	2.72	7.8		7.8	7.8	7.8	.7	.7	Lateral
16	M63	Bottom Chord	2.826	7.8		7.8	7.8	7.8	.7	.7	Lateral
17	M64	Bottom Chord	3.217	7.8		7.8	7.8	7.8	.7	.7	Lateral
18	M121A	Bottom Chord	1.414	6.7		6.7	6.7	6.7	.7	.7	Lateral
19	M119A	Bottom Chord	1.899	8.8		8.8	8.8	8.8	.7	.7	Lateral
20	M117	Bottom Chord	1.579	6.7		6.7	6.7	6.7	.7	.7	Lateral
21	M105A	Bottom Chord	1.333	6.7		6.7	6.7	6.7	.7	.7	Lateral
22	M106A	Bottom Chord	1.351	6.7		6.7	6.7	6.7	.7	.7	Lateral
23	M107A	Bottom Chord	2.416	6.7		6.7	6.7	6.7	.7	.7	Lateral
24	M111A	Bottom Chord	2.065	8.8		8.8	8.8	8.8	.7	.7	Lateral
25	M115C	Bottom Chord	1.734	6.7		6.7	6.7	6.7	.7	.7	Lateral
26	M116A	Bottom Chord	1.438	6.7		6.7	6.7	6.7	.7	.7	Lateral
27	M117A	Bottom Chord	1.271	6.7		6.7	6.7	6.7	.7	.7	Lateral
28	M122A	Bottom Chord	2.72	7.8		7.8	7.8	7.8	.7	.7	Lateral
29	M125D	Bottom Chord	3.212	7.8		7.8	7.8	7.8	.7	.7	Lateral
30	M127A	Bottom Chord	2.72	7.8		7.8	7.8	7.8	.7	.7	Lateral
31	M133A	Bottom Chord	2.527	6.7		6.7	6.7	6.7	.7	.7	Lateral
32	M137	Bottom Chord	.985	6.7		6.7	6.7	6.7	.7	.7	Lateral
33	M124A	TUBE	1.344						.7	.7	Lateral
34	M125	TUBE	1.343						.7	.7	Lateral
35	M2	Top Chord	1.36	7.8		7.8	7.8	7.8	.7	.7	Lateral
36	M3	Top Chord	2.518	7.8		7.8	7.8	7.8	.7	.7	Lateral
37	M4	Top Chord	2.716	6.7		6.7	6.7	6.7	.7	.7	Lateral
38	M5	Top Chord	1.401	6.7		6.7	6.7	6.7	.7	.7	Lateral
39	M6	Top Chord	1.791	6.7		6.7	6.7	6.7	.7	.7	Lateral
40	M7	Top Chord	1.431	6.7		6.7	6.7	6.7	.7	.7	Lateral
41	M8	Top Chord	1.768	6.7		6.7	6.7	6.7	.7	.7	Lateral
42	M9	Top Chord	1.891	8.8		8.8	8.8	8.8	.7	.7	Lateral
43	M12	Top Chord	3.222	10.9		10.9	10.9	10.9	.7	.7	Lateral
44	M13	Top Chord	3.201	10.9		10.9	10.9	10.9	.7	.7	Lateral
45	M18	Top Chord	3.237	4.7		4.7	4.7	4.7	.7	.7	Lateral
46	M19	Top Chord	1.597	10.9		10.9	10.9	10.9	.7	.7	Lateral
47	M20	Top Chord	3.214	10.9		10.9	10.9	10.9	.7	.7	Lateral
48	M21	Top Chord	3.203	10.9		10.9	10.9	10.9	.7	.7	Lateral
49	M22	Top Chord	3.954	8.8		8.8	8.8	8.8	.7	.7	Lateral
50	M23	Top Chord	1.848	6.7		6.7	6.7	6.7	.7	.7	Lateral
51	M24	Top Chord	1.412	6.7		6.7	6.7	6.7	.7	.7	Lateral
52	M25	Top Chord	1.767	6.7		6.7	6.7	6.7	.7	.7	Lateral
53	M26	Top Chord	1.396	6.7		6.7	6.7	6.7	.7	.7	Lateral
54	M27	Top Chord	2.733	6.7		6.7	6.7	6.7	.7	.7	Lateral
55	M28	Top Chord	2.502	7.8		7.8	7.8	7.8	.7	.7	Lateral
56	M29	Top Chord	3.189	7.8		7.8	7.8	7.8	.7	.7	Lateral
57	M133	Top Chord	1.983	8.8		8.8	8.8	8.8	.7	.7	Lateral
58	M114A	Top Chord	1.879	8.8		8.8	8.8	8.8	.7	.7	Lateral
59	M112B	Top Chord	3.931	4.7		4.7	4.7	4.7	.7	.7	Lateral
60	M125A	Top Chord	3.955	4.7		4.7	4.7	4.7	.7	.7	Lateral
61	M125B	Top Chord	3.759	8.8		8.8	8.8	8.8	.7	.7	Lateral
62	M125C	Top Chord	2.11	8.8		8.8	8.8	8.8	.7	.7	Lateral
63	M126	Top Chord	1.36	7.8		7.8	7.8	7.8	.7	.7	Lateral
64	M128	Top Chord	3.184	7.8		7.8	7.8	7.8	.7	.7	Lateral
65	M139	Top Chord	3.205	4.7		4.7	4.7	4.7	.7	.7	Lateral
66	M140	Top Chord	1.61	10.9		10.9	10.9	10.9	.7	.7	Lateral



Company : Big Top
 Designer : Mo
 Job Number : 221-80
 Model Name : 50x72x23 DEM 18BB - Tallahassee, FL

May 27, 2021
 10:42 AM
 Checked By: PSE

Hot Rolled Steel Design Parameters (Continued)

	Label	Shape	Length[ft]	Lbyy[ft]	Lbzz[ft]	Lcomp top[ft]	Lcomp bot[ft]	L-torqu...	Kyy	Kzz	Cb	Function
67	M137A	Top Chord	1.607	10.9		10.9	10.9	10.9	.7	.7		Lateral
68	M138	Top Chord	1.601	10.9		10.9	10.9	10.9	.7	.7		Lateral
69	M70	Z Bar	2.265						.7	.7		Lateral
70	M71	Z Bar	1.935						.7	.7		Lateral
71	M72	Z Bar	1.752						.7	.7		Lateral
72	M73	Z Bar	2.167						.7	.7		Lateral
73	M74	Z Bar	1.683						.7	.7		Lateral
74	M75	Z Bar	1.94						.7	.7		Lateral
75	M76	Z Bar	2.014						.7	.7		Lateral
76	M77	Z Bar	1.938						.7	.7		Lateral
77	M78	Z Bar	2.122						.7	.7		Lateral
78	M79	Z Bar	2.003						.7	.7		Lateral
79	M80	Z Bar	2.551						.7	.7		Lateral
80	M81	Z Bar	2.524						.7	.7		Lateral
81	M82	Z Bar	2.074						.7	.7		Lateral
82	M83	Z Bar	2.082						.7	.7		Lateral
83	M84	Z Bar	2.076						.7	.7		Lateral
84	M85	Z Bar	2.066						.7	.7		Lateral
85	M86	Z Bar	2.077						.7	.7		Lateral
86	M87	Z Bar	2.069						.7	.7		Lateral
87	M88	Z Bar	2.081						.7	.7		Lateral
88	M89	Z Bar	2.072						.7	.7		Lateral
89	M90	Z Bar	2.098						.7	.7		Lateral
90	M91	Z Bar	2.068						.7	.7		Lateral
91	M92	Z Bar	2.684						.7	.7		Lateral
92	M93	Z Bar	2.725						.7	.7		Lateral
93	M94	Z Bar	2.015						.7	.7		Lateral
94	M95	Z Bar	2.111						.7	.7		Lateral
95	M96	Z Bar	2.058						.7	.7		Lateral
96	M97	Z Bar	2.085						.7	.7		Lateral
97	M98	Z Bar	2.059						.7	.7		Lateral
98	M99	Z Bar	2.071						.7	.7		Lateral
99	M100	Z Bar	2.082						.7	.7		Lateral
100	M101	Z Bar	2.081						.7	.7		Lateral
101	M102	Z Bar	2.063						.7	.7		Lateral
102	M103	Z Bar	2.069						.7	.7		Lateral
103	M104	Z Bar	2.682						.7	.7		Lateral
104	M105	Z Bar	2.168						.7	.7		Lateral
105	M106	Z Bar	2.26						.7	.7		Lateral
106	M107	Z Bar	2.098						.7	.7		Lateral
107	M108	Z Bar	1.873						.7	.7		Lateral
108	M109	Z Bar	2.094						.7	.7		Lateral
109	M110	Z Bar	1.937						.7	.7		Lateral
110	M111	Z Bar	1.757						.7	.7		Lateral
111	M112	Z Bar	2.091						.7	.7		Lateral
112	M113	Z Bar	1.748						.7	.7		Lateral
113	M114	Z Bar	1.929						.7	.7		Lateral
114	M115	Z Bar	2.269						.7	.7		Lateral
115	M120	Z Bar	1.343						.7	.7		Lateral
116	M122	Z Bar	1.368						.7	.7		Lateral
117	M124	Z Bar	1.279						.7	.7		Lateral
118	M127	Z Bar	1.344						.7	.7		Lateral
119	M129	Z Bar	1.344						.7	.7		Lateral
120	M135	Z Bar	1.344						.7	.7		Lateral
121	M112A	Z Bar	1.351						.7	.7		Lateral
122	M113A	Z Bar	1.324						.7	.7		Lateral
123	M115B	Z Bar	1.296						.7	.7		Lateral



Hot Rolled Steel Design Parameters (Continued)

	Label	Shape	Length[ft]	Lbyy[ft]	Lbzz[ft]	Lcomp top[ft]	Lcomp bot[ft]	L-torqu...	Kyy	Kzz	Cb	Function
124	M118	Z Bar	1.402						.7	.7		Lateral
125	M119	Z Bar	1.386						.7	.7		Lateral
126	M120A	Z Bar	1.426						.7	.7		Lateral
127	M121	Z Bar	1.353						.7	.7		Lateral
128	M129A	Z Bar	1.912						.7	.7		Lateral
129	M130	Z Bar	1.912						.7	.7		Lateral
130	M131	Z Bar	1.911						.7	.7		Lateral
131	M132	Z Bar	1.911						.7	.7		Lateral

Member Distributed Loads (BLC 1 : DL)

	Member Label	Direction	Start Magnitude[k/ft,...	End Magnitude[k/ft.F,...	Start Location[ft.%]	End Location[ft.%]
1	M29	Y	-0.008	-0.008	0	0
2	M28	Y	-0.008	-0.008	0	0
3	M27	Y	-0.008	-0.008	0	0
4	M26	Y	-0.008	-0.008	0	0
5	M25	Y	-0.008	-0.008	0	0
6	M24	Y	-0.008	-0.008	0	0
7	M23	Y	-0.008	-0.008	0	0
8	M133	Y	-0.008	-0.008	0	0
9	M22	Y	-0.008	-0.008	0	0
10	M21	Y	-0.008	-0.008	0	0
11	M20	Y	-0.008	-0.008	0	0
12	M19	Y	-0.008	-0.008	0	0
13	M18	Y	-0.008	-0.008	0	0
14	M13	Y	-0.008	-0.008	0	0
15	M12	Y	-0.008	-0.008	0	0
16	M9	Y	-0.008	-0.008	0	0
17	M8	Y	-0.008	-0.008	0	0
18	M7	Y	-0.008	-0.008	0	0
19	M6	Y	-0.008	-0.008	0	0
20	M5	Y	-0.008	-0.008	0	0
21	M4	Y	-0.008	-0.008	0	0
22	M3	Y	-0.008	-0.008	0	0
23	M2	Y	-0.008	-0.008	0	0
24	M114A	Y	-0.008	-0.008	0	0
25	M112B	Y	-0.008	-0.008	0	0
26	M125C	Y	-0.008	-0.008	0	0
27	M125A	Y	-0.008	-0.008	0	0
28	M125B	Y	-0.008	-0.008	0	0
29	M126	Y	-0.008	-0.008	0	0
30	M128	Y	-0.008	-0.008	0	0
31	M139	Y	-0.008	-0.008	0	0
32	M140	Y	-0.008	-0.008	0	0
33	M137A	Y	-0.008	-0.008	0	0
34	M138	Y	-0.008	-0.008	0	0

Member Distributed Loads (BLC 2 : RLL)

	Member Label	Direction	Start Magnitude[k/ft,...	End Magnitude[k/ft.F,...	Start Location[ft.%]	End Location[ft.%]
1	M23	Y	-0.04	-0.04	0	0
2	M133	Y	-0.04	-0.04	0	0
3	M22	Y	-0.04	-0.04	0	0
4	M8	Y	-0.04	-0.04	0	0
5	M9	Y	-0.04	-0.04	0	0
6	M21	Y	-0.04	-0.04	0	0
7	M12	Y	-0.04	-0.04	0	0



Member Distributed Loads (BLC 2 : RLL) (Continued)

	Member Label	Direction	Start Magnitude[k/ft....	End Magnitude[k/ft.F....	Start Location[ft.%]	End Location[ft.%]
8	M20	Y	-.04	-.04	0	0
9	M19	Y	-.04	-.04	0	0
10	M18	Y	-.04	-.04	0	0
11	M13	Y	-.04	-.04	0	0
12	M114A	Y	-.04	-.04	0	0
13	M112B	Y	-.04	-.04	0	0
14	M24	Y	-.04	-.04	0	0
15	M7	Y	-.04	-.04	0	0
16	M125C	Y	-.04	-.04	0	0
17	M125A	Y	-.04	-.04	0	0
18	M125B	Y	-.04	-.04	0	0
19	M139	Y	-.04	-.04	0	0
20	M140	Y	-.04	-.04	0	0
21	M137A	Y	-.04	-.04	0	0
22	M138	Y	-.04	-.04	0	0

Member Distributed Loads (BLC 3 : WL+Z)

	Member Label	Direction	Start Magnitude[k/ft....	End Magnitude[k/ft.F....	Start Location[ft.%]	End Location[ft.%]
1	M126	y	.094	.094	0	0
2	M29	y	.094	.094	0	0
3	M28	y	.094	.094	0	0
4	M27	y	.094	.094	0	0
5	M26	y	.094	.094	0	0
6	M2	y	-.114	-.114	0	0
7	M128	y	-.114	-.114	0	0
8	M3	y	-.114	-.114	0	0
9	M4	y	-.114	-.114	0	0
10	M5	y	-.114	-.114	0	0
11	M6	y	-.114	-.114	0	0
12	M24	y	-.178	-.178	0	0
13	M23	y	-.178	-.178	0	0
14	M133	y	-.178	-.178	0	0
15	M114A	y	-.178	-.178	0	0
16	M22	y	-.178	-.178	0	0
17	M21	y	-.178	-.178	0	0
18	M7	y	-.114	-.114	0	0
19	M8	y	-.114	-.114	0	0
20	M9	y	-.114	-.114	0	0
21	M125C	y	-.114	-.114	0	0
22	M125B	y	-.114	-.114	0	0
23	M19	y	-.171	-.171	0	0
24	M18	y	-.171	-.171	0	0
25	M112B	y	-.171	-.171	0	0
26	M125A	y	-.171	-.171	0	0
27	M13	y	-.171	-.171	0	0
28	M139	y	-.171	-.171	0	0
29	M140	y	-.171	-.171	0	0
30	M20	y	-.171	-.171	0	0
31	M12	y	-.114	-.114	0	0
32	M25	y	.094	.094	0	0
33	M137A	y	-.178	-.178	0	0
34	M138	y	-.171	-.171	0	0

Member Distributed Loads (BLC 4 : WL-Z)

	Member Label	Direction	Start Magnitude[k/ft....	End Magnitude[k/ft.F....	Start Location[ft.%]	End Location[ft.%]
1	M126	y	.162	.162	0	0



Member Distributed Loads (BLC 4 : WL-Z) (Continued)

	Member Label	Direction	Start Magnitude[k/ft....	End Magnitude[k/ft.F....	Start Location[ft.%]	End Location[ft.%]
2	M29	y	.162	.162	0	0
3	M28	y	.162	.162	0	0
4	M27	y	.162	.162	0	0
5	M26	y	.162	.162	0	0
6	M2	y	-.046	-.046	0	0
7	M128	y	-.046	-.046	0	0
8	M3	y	-.046	-.046	0	0
9	M4	y	-.046	-.046	0	0
10	M5	y	-.046	-.046	0	0
11	M6	y	-.046	-.046	0	0
12	M24	y	-.11	-.11	0	0
13	M23	y	-.11	-.11	0	0
14	M133	y	-.11	-.11	0	0
15	M114A	y	-.11	-.11	0	0
16	M22	y	-.11	-.11	0	0
17	M21	y	-.11	-.11	0	0
18	M7	y	-.046	-.046	0	0
19	M8	y	-.046	-.046	0	0
20	M9	y	-.046	-.046	0	0
21	M125C	y	-.046	-.046	0	0
22	M125B	y	-.046	-.046	0	0
23	M12	y	-.046	-.046	0	0
24	M25	y	-.11	-.11	0	0
25	M20	y	0	0	0	0
26	M20	y	0	0	0	0
27	M20	y	-.103	-.103	0	0
28	M137A	y	-.103	-.103	0	0
29	M19	y	-.103	-.103	0	0
30	M18	y	-.103	-.103	0	0
31	M112B	y	-.103	-.103	0	0
32	M125A	y	-.103	-.103	0	0
33	M139	y	-.103	-.103	0	0
34	M138	y	-.103	-.103	0	0
35	M140	y	-.103	-.103	0	0
36	M13	y	-.103	-.103	0	0

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distributed Area(Me...	Surface(P...
1	DL	DL		-1				34	
2	RLL	RLL						22	
3	WL+Z	WL+Z						34	
4	WL-Z	WL-Z						36	

Load Combinations

	Description So...	PDe...S...	BLC	Fac...	BLC	Fac...	BLC	Fac...	BLC	Fac...	BLC	Fac...	BLC	Fac...	BLC	Fac...	BLC	Fac...
1	IBC 16-8	Yes Y	DL	1														
2	IBC 16-9	Yes Y	DL	1	LL	1	LLS	1										
3	IBC 16-1...	Yes Y	DL	1	RLL	1												
4	IBC 16-1...	Yes Y	DL	1	LL	.75	LLS	.75	RLL	.75								
5	IBC 16-1...	Yes Y	DL	1	WL+Z	.6												
6	IBC 16-1...	Yes Y	DL	1	WL+Z	.45	LL	.75	LLS	.75	RLL	.75						
7	IBC 16-1...	Yes Y	DL	1	WL+Z	.45	LL	.75	LLS	.75								
8	IBC 16-15	Yes Y	DL	.6	WL+Z	.6												
9	IBC 16-1...	Yes Y	DL	1	WL-Z	.6												



Load Combinations (Continued)

	Description	So...	PDe...	S...	BLC	Fac...	BLC	Fac...	BLC	Fac...	BLC	Fac...	BLC	Fac...	BLC	Fac...	BLC	Fac...
10	IBC 16-1...	Yes	Y		DL	1	WL-Z	.45	LL	.75	LLS	.75	RLL	.75				
11	IBC 16-1...	Yes	Y		DL	1	WL-Z	.45	LL	.75	LLS	.75						
12	IBC 16-15	Yes	Y		DL	.6	WL-Z	.6										
13	DL		Y		DL	1												
14	RLL		Y		RLL	1												
15	WL+Z		Y		WL+Z	1												
16	WL-Z		Y		WL-Z	1												

Envelope Joint Reactions

	Joint		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	1	max	0	12	1.706	3	.706	8	0	12	0	12	0	12
2		min	0	1	-3.111	8	-.285	3	0	1	0	1	0	1
3	2	max	0	12	.887	5	.726	8	0	12	0	12	0	12
4		min	0	1	-.035	3	-.294	3	0	1	0	1	0	1
5	3	max	0	12	.062	2	.294	3	0	12	0	12	0	12
6		min	0	1	-.605	8	-.098	12	0	1	0	1	0	1
7	4	max	0	12	1.686	3	.285	3	0	12	0	12	0	12
8		min	0	1	-1.209	8	-.095	12	0	1	0	1	0	1
9	Totals:	max	0	12	3.336	3	1.315	8						
10		min	0	1	-4.067	8	0	1						

Envelope Member Section Forces

	Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...]	LC	y-y Mome...	LC	z-z Mome...	LC
1	M43	1	max	.933	3	-.001	8	0	12	0	12	0	12	0	8
2			min	-1.867	8	-.003	3	0	1	0	1	0	1	-.003	10
3		2	max	.933	3	0	8	0	12	0	12	0	12	.001	5
4			min	-1.867	8	-.002	3	0	1	0	1	0	1	-.001	12
5		3	max	.932	3	0	8	0	12	0	12	0	12	.001	5
6			min	-1.868	8	0	3	0	1	0	1	0	1	0	12
7		4	max	.932	3	.001	5	0	12	0	12	0	12	0	6
8			min	-1.868	8	0	3	0	1	0	1	0	1	-.001	12
9		5	max	.931	3	.003	5	0	12	0	12	0	12	0	3
10			min	-1.868	8	.002	12	0	1	0	1	0	1	-.003	9
11	M44	1	max	.47	12	.003	8	0	12	0	12	0	12	.001	8
12			min	-.39	3	-.006	3	0	1	0	1	0	1	-.003	3
13		2	max	.47	12	.003	8	0	12	0	12	0	12	.001	3
14			min	-.39	3	-.004	3	0	1	0	1	0	1	-.002	12
15		3	max	.47	12	.004	8	0	12	0	12	0	12	.004	3
16			min	-.39	3	-.003	3	0	1	0	1	0	1	-.004	8
17		4	max	.469	12	.005	5	0	12	0	12	0	12	.006	3
18			min	-.391	3	-.002	3	0	1	0	1	0	1	-.007	8
19		5	max	.469	12	.006	5	0	12	0	12	0	12	.007	3
20			min	-.391	3	0	3	0	1	0	1	0	1	-.011	8
21	M45	1	max	1.523	8	0	8	0	12	0	12	0	12	.004	3
22			min	-1.46	3	-.004	3	0	1	0	1	0	1	-.008	5
23		2	max	1.523	8	.002	8	0	12	0	12	0	12	.007	3
24			min	-1.46	3	-.003	3	0	1	0	1	0	1	-.009	8
25		3	max	1.522	8	.002	8	0	12	0	12	0	12	.009	3
26			min	-1.46	3	-.002	3	0	1	0	1	0	1	-.011	8
27		4	max	1.522	8	.004	5	0	12	0	12	0	12	.01	3
28			min	-1.461	3	0	3	0	1	0	1	0	1	-.013	8
29		5	max	1.522	8	.005	5	0	12	0	12	0	12	.01	3
30			min	-1.461	3	0	3	0	1	0	1	0	1	-.016	8
31	M46	1	max	2.625	8	.002	8	0	12	0	12	0	12	.007	3



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
32		min	-2.265	3	-.005	3	0	1	0	1	0	1	-.012	8
33	2	max	2.625	8	.003	8	0	12	0	12	0	12	.01	3
34		min	-2.266	3	-.004	3	0	1	0	1	0	1	-.013	8
35	3	max	2.625	8	.004	8	0	12	0	12	0	12	.013	3
36		min	-2.266	3	-.003	3	0	1	0	1	0	1	-.016	8
37	4	max	2.624	8	.005	5	0	12	0	12	0	12	.014	3
38		min	-2.266	3	-.001	3	0	1	0	1	0	1	-.019	8
39	5	max	2.624	8	.006	5	0	12	0	12	0	12	.015	3
40		min	-2.266	3	0	3	0	1	0	1	0	1	-.023	8
41	M47	1	max	3.378	8	.003	8	0	12	0	12	0	.009	3
42		min	-2.814	3	-.005	3	0	1	0	1	0	1	-.014	8
43	2	max	3.377	8	.003	8	0	12	0	12	0	12	.012	3
44		min	-2.814	3	-.004	3	0	1	0	1	0	1	-.016	8
45	3	max	3.377	8	.004	8	0	12	0	12	0	12	.015	3
46		min	-2.814	3	-.002	3	0	1	0	1	0	1	-.019	8
47	4	max	3.377	8	.005	5	0	12	0	12	0	12	.016	3
48		min	-2.814	3	-.001	3	0	1	0	1	0	1	-.023	8
49	5	max	3.377	8	.007	5	0	12	0	12	0	12	.016	3
50		min	-2.814	3	0	3	0	1	0	1	0	1	-.027	8
51	M48	1	max	3.803	8	0	3	0	12	0	12	0	.016	3
52		min	-3.114	3	-.007	5	0	1	0	1	0	1	-.026	8
53	2	max	3.803	8	0	3	0	12	0	12	0	12	.016	3
54		min	-3.114	3	-.006	5	0	1	0	1	0	1	-.023	8
55	3	max	3.803	8	.002	3	0	12	0	12	0	12	.015	3
56		min	-3.114	3	-.005	8	0	1	0	1	0	1	-.019	8
57	4	max	3.803	8	.003	3	0	12	0	12	0	12	.014	3
58		min	-3.114	3	-.005	8	0	1	0	1	0	1	-.016	8
59	5	max	3.803	8	.004	3	0	12	0	12	0	12	.012	3
60		min	-3.114	3	-.004	8	0	1	0	1	0	1	-.014	8
61	M49	1	max	3.804	8	.005	8	0	12	0	12	0	.012	3
62		min	-3.114	3	-.004	3	0	1	0	1	0	1	-.013	8
63	2	max	3.804	8	.006	8	0	12	0	12	0	12	.014	3
64		min	-3.114	3	-.003	3	0	1	0	1	0	1	-.016	8
65	3	max	3.804	8	.006	8	0	12	0	12	0	12	.015	3
66		min	-3.114	3	-.002	3	0	1	0	1	0	1	-.02	8
67	4	max	3.804	8	.007	5	0	12	0	12	0	12	.016	3
68		min	-3.114	3	0	3	0	1	0	1	0	1	-.023	8
69	5	max	3.804	8	.008	5	0	12	0	12	0	12	.016	3
70		min	-3.114	3	0	3	0	1	0	1	0	1	-.027	8
71	M50	1	max	3.409	8	0	3	0	12	0	12	0	.017	3
72		min	-2.791	3	-.007	5	0	1	0	1	0	1	-.028	8
73	2	max	3.409	8	.002	3	0	12	0	12	0	12	.016	3
74		min	-2.79	3	-.006	5	0	1	0	1	0	1	-.023	8
75	3	max	3.409	8	.003	3	0	12	0	12	0	12	.015	3
76		min	-2.79	3	-.005	8	0	1	0	1	0	1	-.019	8
77	4	max	3.409	8	.004	3	0	12	0	12	0	12	.012	3
78		min	-2.79	3	-.004	8	0	1	0	1	0	1	-.016	8
79	5	max	3.409	8	.006	3	0	12	0	12	0	12	.008	3
80		min	-2.79	3	-.003	8	0	1	0	1	0	1	-.013	8
81	M51	1	max	2.715	8	0	3	0	12	0	12	0	.014	3
82		min	-2.252	3	-.005	5	0	1	0	1	0	1	-.022	8
83	2	max	2.715	8	0	3	0	12	0	12	0	12	.014	3
84		min	-2.252	3	-.004	5	0	1	0	1	0	1	-.019	8
85	3	max	2.715	8	.002	3	0	12	0	12	0	12	.012	3
86		min	-2.252	3	-.003	8	0	1	0	1	0	1	-.016	8
87	4	max	2.716	8	.003	3	0	12	0	12	0	12	.01	3
88		min	-2.252	3	-.002	8	0	1	0	1	0	1	-.014	8



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
89	5	max	2.716	8	.005	3	0	12	0	12	0	12	.007	3
90		min	-2.251	3	-.001	8	0	1	0	1	0	1	-.013	8
91	M52	1	max	1.684	8	0	3	0	12	0	12	0	.01	3
92		min	-1.461	3	-.005	5	0	1	0	1	0	1	-.017	8
93		2	max	1.684	8	0	3	0	12	0	12	0	.01	3
94		min	-1.461	3	-.004	5	0	1	0	1	0	1	-.014	8
95		3	max	1.684	8	.002	3	0	12	0	12	0	.009	3
96		min	-1.461	3	-.003	8	0	1	0	1	0	1	-.011	8
97		4	max	1.684	8	.003	3	0	12	0	12	0	.007	3
98		min	-1.46	3	-.002	8	0	1	0	1	0	1	-.01	8
99		5	max	1.684	8	.005	3	0	12	0	12	0	.004	3
100		min	-1.46	3	-.001	8	0	1	0	1	0	1	-.009	5
101	M53	1	max	.251	8	0	3	0	12	0	12	0	.007	3
102		min	-.398	3	-.007	5	0	1	0	1	0	1	-.013	8
103		2	max	.251	8	.002	3	0	12	0	12	0	.006	3
104		min	-.397	3	-.006	5	0	1	0	1	0	1	-.008	8
105		3	max	.252	8	.003	3	0	12	0	12	0	.004	3
106		min	-.397	3	-.005	8	0	1	0	1	0	1	-.004	8
107		4	max	.252	8	.004	3	0	12	0	12	0	.002	10
108		min	-.396	3	-.004	8	0	1	0	1	0	1	-.001	8
109		5	max	.252	8	.006	3	0	12	0	12	0	.003	12
110		min	-.396	3	-.003	8	0	1	0	1	0	1	-.003	3
111	M54	1	max	.933	3	0	3	0	12	0	12	0	0	3
112		min	-1.472	8	-.004	5	0	1	0	1	0	1	-.004	5
113		2	max	.934	3	0	3	0	12	0	12	0	.001	10
114		min	-1.471	8	-.003	5	0	1	0	1	0	1	-.001	8
115		3	max	.934	3	.002	3	0	12	0	12	0	.002	9
116		min	-1.471	8	-.002	8	0	1	0	1	0	1	0	3
117		4	max	.935	3	.003	3	0	12	0	12	0	.003	12
118		min	-1.471	8	-.001	8	0	1	0	1	0	1	-.002	3
119		5	max	.935	3	.004	3	0	12	0	12	0	.003	12
120		min	-1.47	8	0	8	0	1	0	1	0	1	-.005	3
121	M104A	1	max	2.873	3	.013	3	0	12	0	12	0	.005	3
122		min	-3.785	8	-.021	8	0	1	0	1	0	1	-.01	8
123		2	max	2.873	3	.013	3	0	12	0	12	0	.003	12
124		min	-3.785	8	-.021	8	0	1	0	1	0	1	-.002	3
125		3	max	2.873	3	.014	3	0	12	0	12	0	.012	8
126		min	-3.785	8	-.02	8	0	1	0	1	0	1	-.009	3
127		4	max	2.874	3	.015	3	0	12	0	12	0	.023	8
128		min	-3.785	8	-.02	8	0	1	0	1	0	1	-.017	3
129		5	max	2.874	3	.016	3	0	12	0	12	0	.034	8
130		min	-3.784	8	-.019	8	0	1	0	1	0	1	-.025	3
131	M110A	1	max	2.938	3	.03	8	0	12	0	12	0	.05	8
132		min	-4.912	8	-.021	3	0	1	0	1	0	1	-.031	3
133		2	max	2.938	3	.031	8	0	12	0	12	0	.034	8
134		min	-4.912	8	-.02	3	0	1	0	1	0	1	-.02	3
135		3	max	2.937	3	.031	8	0	12	0	12	0	.017	8
136		min	-4.912	8	-.019	3	0	1	0	1	0	1	-.01	3
137		4	max	2.937	3	.032	8	0	12	0	12	0	0	5
138		min	-4.913	8	-.018	3	0	1	0	1	0	1	-.001	10
139		5	max	2.937	3	.032	8	0	12	0	12	0	.009	3
140		min	-4.913	8	-.017	3	0	1	0	1	0	1	-.016	8
141	M34	1	max	3.004	3	.003	3	0	12	0	12	0	.013	12
142		min	-5.501	8	-.005	8	0	1	0	1	0	1	-.006	3
143		2	max	3.003	3	.003	3	0	12	0	12	0	.016	8
144		min	-5.502	8	-.005	8	0	1	0	1	0	1	-.008	3
145		3	max	3.001	3	.003	3	0	12	0	12	0	.019	8



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
146		min	-5.503	8	-.005	8	0	1	0	1	0	1	-.01	3
147	4	max	3	3	.003	3	0	12	0	12	0	12	.023	8
148		min	-5.504	8	-.005	8	0	1	0	1	0	1	-.012	3
149	5	max	2.999	3	.003	3	0	12	0	12	0	12	.026	8
150		min	-5.504	8	-.005	8	0	1	0	1	0	1	-.014	3
151	M63	1	max	3.02	3	.004	8	0	12	0	12	0	.013	8
152		min	-2.454	8	-.003	3	0	1	0	1	0	1	-.015	3
153	2	max	3.021	3	.004	8	0	12	0	12	0	12	.01	8
154		min	-2.453	8	-.003	3	0	1	0	1	0	1	-.012	3
155	3	max	3.023	3	.004	8	0	12	0	12	0	12	.007	8
156		min	-2.453	8	-.003	3	0	1	0	1	0	1	-.01	3
157	4	max	3.024	3	.004	8	0	12	0	12	0	12	.004	8
158		min	-2.452	8	-.003	3	0	1	0	1	0	1	-.008	3
159	5	max	3.025	3	.004	8	0	12	0	12	0	12	0	12
160		min	-2.451	8	-.003	3	0	1	0	1	0	1	-.005	3
161	M64	1	max	1.932	3	.004	8	0	12	0	12	0	.008	8
162		min	-1.483	8	-.005	3	0	1	0	1	0	1	-.012	3
163	2	max	1.933	3	.004	8	0	12	0	12	0	12	.005	8
164		min	-1.483	8	-.005	3	0	1	0	1	0	1	-.009	3
165	3	max	1.935	3	.004	8	0	12	0	12	0	12	.002	8
166		min	-1.482	8	-.005	3	0	1	0	1	0	1	-.005	3
167	4	max	1.936	3	.004	8	0	12	0	12	0	12	0	12
168		min	-1.481	8	-.005	3	0	1	0	1	0	1	-.001	3
169	5	max	1.937	3	.004	8	0	12	0	12	0	12	.002	3
170		min	-1.48	8	-.005	3	0	1	0	1	0	1	-.003	8
171	M121A	1	max	4.73	3	.002	3	0	12	0	12	0	.032	8
172		min	-7.728	8	-.004	5	0	1	0	1	0	1	-.02	3
173	2	max	4.729	3	.002	3	0	12	0	12	0	12	.033	8
174		min	-7.728	8	-.004	8	0	1	0	1	0	1	-.02	3
175	3	max	4.729	3	.003	3	0	12	0	12	0	12	.035	8
176		min	-7.728	8	-.004	8	0	1	0	1	0	1	-.021	3
177	4	max	4.728	3	.003	3	0	12	0	12	0	12	.036	8
178		min	-7.729	8	-.004	8	0	1	0	1	0	1	-.022	3
179	5	max	4.728	3	.004	3	0	12	0	12	0	12	.037	8
180		min	-7.729	8	-.003	8	0	1	0	1	0	1	-.024	3
181	M119A	1	max	2.964	3	.016	8	0	12	0	12	0	.039	8
182		min	-4.955	8	-.012	3	0	1	0	1	0	1	-.025	3
183	2	max	2.963	3	.016	8	0	12	0	12	0	12	.031	8
184		min	-4.955	8	-.011	3	0	1	0	1	0	1	-.019	3
185	3	max	2.963	3	.016	8	0	12	0	12	0	12	.023	8
186		min	-4.956	8	-.01	3	0	1	0	1	0	1	-.014	3
187	4	max	2.962	3	.017	8	0	12	0	12	0	12	.015	8
188		min	-4.956	8	-.01	3	0	1	0	1	0	1	-.01	3
189	5	max	2.962	3	.017	8	0	12	0	12	0	12	.007	8
190		min	-4.956	8	-.009	3	0	1	0	1	0	1	-.005	3
191	M117	1	max	5.055	3	.022	3	0	12	0	12	0	.014	12
192		min	-8.458	8	-.03	8	0	1	0	1	0	1	-.004	3
193	2	max	5.054	3	.022	3	0	12	0	12	0	12	.026	8
194		min	-8.459	8	-.03	8	0	1	0	1	0	1	-.013	3
195	3	max	5.054	3	.022	3	0	12	0	12	0	12	.038	8
196		min	-8.459	8	-.03	8	0	1	0	1	0	1	-.022	3
197	4	max	5.053	3	.022	3	0	12	0	12	0	12	.05	8
198		min	-8.459	8	-.03	8	0	1	0	1	0	1	-.031	3
199	5	max	5.052	3	.022	3	0	12	0	12	0	12	.061	8
200		min	-8.46	8	-.03	8	0	1	0	1	0	1	-.039	3
201	M105A	1	max	4.518	3	.002	3	0	12	0	12	0	.021	8
202		min	-5.39	8	-.006	5	0	1	0	1	0	1	-.02	3



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
203	2	max	4.518	3	.003	3	0	12	0	12	0	12	.023	8
204		min	-5.39	8	-.006	8	0	1	0	1	0	1	-.021	3
205	3	max	4.519	3	.003	3	0	12	0	12	0	12	.025	8
206		min	-5.39	8	-.006	8	0	1	0	1	0	1	-.022	3
207	4	max	4.519	3	.003	3	0	12	0	12	0	12	.027	8
208		min	-5.389	8	-.005	8	0	1	0	1	0	1	-.023	3
209	5	max	4.52	3	.004	3	0	12	0	12	0	12	.029	8
210		min	-5.389	8	-.005	8	0	1	0	1	0	1	-.024	3
211	M106A	1	max	5.069	3	.033	3	0	12	0	12	0	.002	12
212		min	-5.385	8	-.035	8	0	1	0	1	0	1	0	3
213	2	max	5.07	3	.033	3	0	12	0	12	0	12	.012	8
214		min	-5.384	8	-.035	8	0	1	0	1	0	1	-.012	3
215	3	max	5.07	3	.034	3	0	12	0	12	0	12	.024	8
216		min	-5.384	8	-.034	8	0	1	0	1	0	1	-.023	3
217	4	max	5.071	3	.034	3	0	12	0	12	0	12	.036	8
218		min	-5.384	8	-.034	8	0	1	0	1	0	1	-.034	3
219	5	max	5.071	3	.034	3	0	12	0	12	0	12	.047	8
220		min	-5.383	8	-.034	8	0	1	0	1	0	1	-.046	3
221	M107A	1	max	4.181	3	.005	8	0	12	0	12	0	.018	8
222		min	-3.852	8	-.003	3	0	1	0	1	0	1	-.019	3
223	2	max	4.182	3	.005	8	0	12	0	12	0	12	.015	8
224		min	-3.851	8	-.003	3	0	1	0	1	0	1	-.017	3
225	3	max	4.183	3	.005	8	0	12	0	12	0	12	.012	8
226		min	-3.851	8	-.003	3	0	1	0	1	0	1	-.015	3
227	4	max	4.184	3	.005	8	0	12	0	12	0	12	.009	8
228		min	-3.85	8	-.003	3	0	1	0	1	0	1	-.013	3
229	5	max	4.185	3	.005	8	0	12	0	12	0	12	.006	8
230		min	-3.85	8	-.003	3	0	1	0	1	0	1	-.011	3
231	M111A	1	max	2.932	3	.015	3	0	12	0	12	0	.004	12
232		min	-3.853	8	-.016	8	0	1	0	1	0	1	0	1
233	2	max	2.933	3	.016	3	0	12	0	12	0	12	.011	8
234		min	-3.853	8	-.015	8	0	1	0	1	0	1	-.007	3
235	3	max	2.933	3	.017	3	0	12	0	12	0	12	.019	8
236		min	-3.852	8	-.015	8	0	1	0	1	0	1	-.016	3
237	4	max	2.934	3	.018	3	0	12	0	12	0	12	.027	8
238		min	-3.852	8	-.014	8	0	1	0	1	0	1	-.025	3
239	5	max	2.934	3	.019	3	0	12	0	12	0	12	.034	8
240		min	-3.852	8	-.014	8	0	1	0	1	0	1	-.034	3
241	M115C	1	max	4.682	3	.024	8	0	12	0	12	0	.051	8
242		min	-7.656	8	-.016	3	0	1	0	1	0	1	-.032	3
243	2	max	4.682	3	.024	8	0	12	0	12	0	12	.041	8
244		min	-7.657	8	-.016	3	0	1	0	1	0	1	-.025	3
245	3	max	4.681	3	.025	8	0	12	0	12	0	12	.03	8
246		min	-7.657	8	-.015	3	0	1	0	1	0	1	-.019	3
247	4	max	4.681	3	.025	8	0	12	0	12	0	12	.019	8
248		min	-7.657	8	-.015	3	0	1	0	1	0	1	-.012	3
249	5	max	4.68	3	.025	8	0	12	0	12	0	12	.008	8
250		min	-7.658	8	-.014	3	0	1	0	1	0	1	-.006	3
251	M116A	1	max	4.538	3	.019	8	0	12	0	12	0	.032	8
252		min	-5.402	8	-.007	3	0	1	0	1	0	1	-.021	3
253	2	max	4.539	3	.019	8	0	12	0	12	0	12	.025	8
254		min	-5.401	8	-.007	3	0	1	0	1	0	1	-.019	3
255	3	max	4.539	3	.019	8	0	12	0	12	0	12	.018	8
256		min	-5.401	8	-.007	3	0	1	0	1	0	1	-.016	3
257	4	max	4.54	3	.019	8	0	12	0	12	0	12	.011	8
258		min	-5.401	8	-.006	3	0	1	0	1	0	1	-.014	3
259	5	max	4.54	3	.019	8	0	12	0	12	0	12	.004	8



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
260		min	-5.401	8	-.006	3	0	1	0	1	0	1	-.012	3
261	M117A	1	max	5.144	3	.053	8	0	12	0	12	0	.057	8
262		min	-5.444	8	-.038	3	0	1	0	1	0	1	-.048	3
263		2	max	5.145	3	.054	8	0	12	0	12	0	.04	8
264		min	-5.444	8	-.038	3	0	1	0	1	0	1	-.036	3
265		3	max	5.145	3	.054	8	0	12	0	12	0	.023	8
266		min	-5.443	8	-.038	3	0	1	0	1	0	1	-.024	3
267		4	max	5.146	3	.054	8	0	12	0	12	0	.006	8
268		min	-5.443	8	-.038	3	0	1	0	1	0	1	-.012	3
269		5	max	5.146	3	.054	8	0	12	0	12	0	0	3
270		min	-5.443	8	-.038	3	0	1	0	1	0	1	-.011	5
271	M122A	1	max	.55	3	.006	3	0	12	0	12	0	.011	3
272		min	-.622	12	-.014	8	0	1	0	1	0	1	-.027	8
273		2	max	.549	3	.006	3	0	12	0	12	0	.007	3
274		min	-.623	12	-.014	8	0	1	0	1	0	1	-.017	8
275		3	max	.548	3	.006	3	0	12	0	12	0	.003	3
276		min	-.623	12	-.014	8	0	1	0	1	0	1	-.007	8
277		4	max	.547	3	.006	3	0	12	0	12	0	.005	12
278		min	-.624	12	-.014	8	0	1	0	1	0	1	0	3
279		5	max	.545	3	.006	3	0	12	0	12	0	.014	12
280		min	-.625	12	-.014	8	0	1	0	1	0	1	-.005	3
281	M125D	1	max	1.925	3	.005	3	0	12	0	12	0	.002	3
282		min	-3.49	8	-.009	8	0	1	0	1	0	1	-.004	8
283		2	max	1.923	3	.005	3	0	12	0	12	0	.005	12
284		min	-3.491	8	-.009	8	0	1	0	1	0	1	-.001	3
285		3	max	1.922	3	.005	3	0	12	0	12	0	.01	8
286		min	-3.492	8	-.009	8	0	1	0	1	0	1	-.005	3
287		4	max	1.92	3	.005	3	0	12	0	12	0	.018	8
288		min	-3.493	8	-.009	8	0	1	0	1	0	1	-.009	3
289		5	max	1.919	3	.005	3	0	12	0	12	0	.025	8
290		min	-3.494	8	-.009	8	0	1	0	1	0	1	-.012	3
291	M127A	1	max	.56	3	.002	12	0	12	0	12	0	0	12
292		min	-.74	8	-.006	3	0	1	0	1	0	1	-.005	3
293		2	max	.561	3	.002	12	0	12	0	12	0	0	2
294		min	-.739	8	-.006	3	0	1	0	1	0	1	-.001	6
295		3	max	.562	3	.002	12	0	12	0	12	0	.003	3
296		min	-.738	8	-.006	3	0	1	0	1	0	1	-.002	8
297		4	max	.563	3	.002	12	0	12	0	12	0	.007	3
298		min	-.738	8	-.006	3	0	1	0	1	0	1	-.003	12
299		5	max	.564	3	.002	12	0	12	0	12	0	.011	3
300		min	-.737	8	-.006	3	0	1	0	1	0	1	-.004	12
301	M133A	1	max	4.171	3	.004	3	0	12	0	12	0	.021	8
302		min	-7.395	8	-.006	8	0	1	0	1	0	1	-.01	3
303		2	max	4.17	3	.004	3	0	12	0	12	0	.024	8
304		min	-7.395	8	-.006	8	0	1	0	1	0	1	-.013	3
305		3	max	4.169	3	.004	3	0	12	0	12	0	.028	8
306		min	-7.396	8	-.006	8	0	1	0	1	0	1	-.015	3
307		4	max	4.168	3	.004	3	0	12	0	12	0	.031	8
308		min	-7.397	8	-.006	8	0	1	0	1	0	1	-.017	3
309		5	max	4.167	3	.004	3	0	12	0	12	0	.035	8
310		min	-7.397	8	-.006	8	0	1	0	1	0	1	-.02	3
311	M137	1	max	5.156	3	.061	8	0	12	0	12	0	.07	8
312		min	-8.618	8	-.033	3	0	1	0	1	0	1	-.041	3
313		2	max	5.155	3	.061	8	0	12	0	12	0	.055	8
314		min	-8.619	8	-.033	3	0	1	0	1	0	1	-.033	3
315		3	max	5.155	3	.061	8	0	12	0	12	0	.04	8
316		min	-8.619	8	-.033	3	0	1	0	1	0	1	-.025	3



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
317	4	max	5.154	3	.061	8	0	12	0	12	0	12	.025	8
318		min	-8.619	8	-.033	3	0	1	0	1	0	1	-.017	3
319	5	max	5.154	3	.061	8	0	12	0	12	0	12	.01	8
320		min	-8.619	8	-.033	3	0	1	0	1	0	1	-.009	3
321	M124A	1	max	.267	3	.066	8	0	12	0	12	0	.035	8
322		min	-.601	8	-.03	3	0	1	0	1	0	1	-.018	3
323	2	max	.267	3	.065	8	0	12	0	12	0	12	.013	8
324		min	-.601	8	-.031	3	0	1	0	1	0	1	-.008	3
325	3	max	.267	3	.065	8	0	12	0	12	0	12	.003	3
326		min	-.601	8	-.032	3	0	1	0	1	0	1	-.009	12
327	4	max	.267	3	.064	8	0	12	0	12	0	12	.014	3
328		min	-.601	8	-.033	3	0	1	0	1	0	1	-.03	8
329	5	max	.267	3	.063	8	0	12	0	12	0	12	.025	3
330		min	-.601	8	-.034	3	0	1	0	1	0	1	-.052	8
331	M125	1	max	.267	3	.018	8	0	12	0	12	0	.011	8
332		min	-.093	12	-.03	3	0	1	0	1	0	1	-.018	3
333	2	max	.267	3	.017	8	0	12	0	12	0	12	.005	8
334		min	-.093	12	-.031	3	0	1	0	1	0	1	-.008	3
335	3	max	.267	3	.016	8	0	12	0	12	0	12	.003	3
336		min	-.093	12	-.032	3	0	1	0	1	0	1	0	12
337	4	max	.267	3	.016	8	0	12	0	12	0	12	.014	3
338		min	-.093	12	-.033	3	0	1	0	1	0	1	-.006	8
339	5	max	.267	3	.015	8	0	12	0	12	0	12	.025	3
340		min	-.093	12	-.033	3	0	1	0	1	0	1	-.011	8
341	M2	1	max	1.652	3	.026	6	0	12	0	12	0	.025	3
342		min	-1.193	8	0	12	0	1	0	1	0	1	-.011	8
343	2	max	1.648	3	.026	3	0	12	0	12	0	12	.016	3
344		min	-1.195	8	-.012	8	0	1	0	1	0	1	-.011	8
345	3	max	1.645	3	.026	3	0	12	0	12	0	12	.007	3
346		min	-1.197	8	-.035	8	0	1	0	1	0	1	-.003	12
347	4	max	1.642	3	.026	3	0	12	0	12	0	12	.013	8
348		min	-1.199	8	-.058	8	0	1	0	1	0	1	-.002	3
349	5	max	1.638	3	.026	3	0	12	0	12	0	12	.037	8
350		min	-1.201	8	-.081	8	0	1	0	1	0	1	-.01	3
351	M3	1	max	.377	12	.087	5	0	12	0	12	0	.044	8
352		min	-.949	3	0	1	0	1	0	1	0	1	-.004	3
353	2	max	.373	12	.044	5	0	12	0	12	0	12	.003	8
354		min	-.955	3	0	1	0	1	0	1	0	1	-.006	3
355	3	max	.37	12	.003	3	0	12	0	12	0	12	-.002	2
356		min	-.961	3	0	12	0	1	0	1	0	1	-.013	6
357	4	max	.366	12	.003	3	0	12	0	12	0	12	.003	12
358		min	-.967	3	-.042	8	0	1	0	1	0	1	-.009	3
359	5	max	.362	12	.003	3	0	12	0	12	0	12	.043	8
360		min	-.973	3	-.085	8	0	1	0	1	0	1	-.011	3
361	M4	1	max	1.445	8	.09	5	0	12	0	12	0	.044	8
362		min	-2.196	3	.001	1	0	1	0	1	0	1	-.005	3
363	2	max	1.441	8	.043	5	0	12	0	12	0	12	.002	12
364		min	-2.203	3	.001	1	0	1	0	1	0	1	-.009	3
365	3	max	1.437	8	.005	3	0	12	0	12	0	12	-.003	12
366		min	-2.21	3	-.004	8	0	1	0	1	0	1	-.019	6
367	4	max	1.433	8	.005	3	0	12	0	12	0	12	.005	12
368		min	-2.216	3	-.05	8	0	1	0	1	0	1	-.017	3
369	5	max	1.429	8	.005	3	0	12	0	12	0	12	.054	8
370		min	-2.223	3	-.096	8	0	1	0	1	0	1	-.02	3
371	M5	1	max	2.841	8	.055	8	0	12	0	12	0	.035	8
372		min	-3.269	3	-.002	3	0	1	0	1	0	1	-.017	3
373	2	max	2.839	8	.031	8	0	12	0	12	0	12	.02	8



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
374		min	-3.272	3	-.002	3	0	1	0	1	0	1	-.016	3
375	3	max	2.837	8	.008	8	0	12	0	12	0	12	.013	8
376		min	-3.276	3	-.002	3	0	1	0	1	0	1	-.015	3
377	4	max	2.835	8	0	2	0	12	0	12	0	12	.014	8
378		min	-3.279	3	-.016	5	0	1	0	1	0	1	-.014	3
379	5	max	2.833	8	0	2	0	12	0	12	0	12	.024	8
380		min	-3.282	3	-.04	5	0	1	0	1	0	1	-.014	3
381	M6	1	max	2.918	8	.038	6	0	12	0	12	0	.013	8
382		min	-3.364	3	.003	1	0	1	0	1	0	1	-.004	3
383	2	max	2.916	8	.016	6	0	12	0	12	0	12	.004	12
384		min	-3.368	3	0	12	0	1	0	1	0	1	-.011	3
385	3	max	2.913	8	.016	3	0	12	0	12	0	12	.007	12
386		min	-3.372	3	-.023	8	0	1	0	1	0	1	-.018	3
387	4	max	2.911	8	.017	3	0	12	0	12	0	12	.024	8
388		min	-3.376	3	-.053	8	0	1	0	1	0	1	-.025	3
389	5	max	2.908	8	.018	3	0	12	0	12	0	12	.054	8
390		min	-3.381	3	-.083	8	0	1	0	1	0	1	-.033	3
391	M7	1	max	3.47	8	.064	8	0	12	0	12	0	.044	8
392		min	-3.435	3	-.029	3	0	1	0	1	0	1	-.033	3
393	2	max	3.468	8	.04	8	0	12	0	12	0	12	.025	8
394		min	-3.451	3	-.022	3	0	1	0	1	0	1	-.024	3
395	3	max	3.466	8	.017	8	0	12	0	12	0	12	.015	8
396		min	-3.467	3	-.015	3	0	1	0	1	0	1	-.017	3
397	4	max	3.464	8	0	12	0	12	0	12	0	12	.013	8
398		min	-3.484	3	-.011	6	0	1	0	1	0	1	-.013	3
399	5	max	3.462	8	-.001	2	0	12	0	12	0	12	.02	8
400		min	-3.5	3	-.031	5	0	1	0	1	0	1	-.011	3
401	M8	1	max	3.474	8	.049	8	0	12	0	12	0	.024	8
402		min	-3.506	3	-.021	3	0	1	0	1	0	1	-.019	3
403	2	max	3.472	8	.02	8	0	12	0	12	0	12	.009	8
404		min	-3.525	3	-.01	3	0	1	0	1	0	1	-.012	3
405	3	max	3.47	8	.002	3	0	12	0	12	0	12	.007	12
406		min	-3.544	3	-.009	8	0	1	0	1	0	1	-.011	3
407	4	max	3.468	8	.013	3	0	12	0	12	0	12	.017	8
408		min	-3.563	3	-.037	8	0	1	0	1	0	1	-.014	3
409	5	max	3.466	8	.025	3	0	12	0	12	0	12	.04	8
410		min	-3.581	3	-.066	8	0	1	0	1	0	1	-.023	3
411	M9	1	max	3.419	8	.062	8	0	12	0	12	0	.04	8
412		min	-3.156	3	-.035	3	0	1	0	1	0	1	-.027	3
413	2	max	3.417	8	.032	8	0	12	0	12	0	12	.017	8
414		min	-3.172	3	-.018	3	0	1	0	1	0	1	-.015	3
415	3	max	3.415	8	.002	5	0	12	0	12	0	12	.009	8
416		min	-3.187	3	0	12	0	1	0	1	0	1	-.011	3
417	4	max	3.414	8	.018	3	0	12	0	12	0	12	.016	8
418		min	-3.202	3	-.028	8	0	1	0	1	0	1	-.015	3
419	5	max	3.412	8	.036	3	0	12	0	12	0	12	.036	8
420		min	-3.218	3	-.059	8	0	1	0	1	0	1	-.028	3
421	M12	1	max	.563	3	.104	8	0	12	0	12	0	.061	8
422		min	-1.21	8	-.079	3	0	1	0	1	0	1	-.048	3
423	2	max	.549	3	.053	8	0	12	0	12	0	12	.002	10
424		min	-1.212	8	-.042	3	0	1	0	1	0	1	-.002	8
425	3	max	.536	3	.003	8	0	12	0	12	0	12	.02	3
426		min	-1.214	8	-.004	3	0	1	0	1	0	1	-.025	8
427	4	max	.522	3	.034	3	0	12	0	12	0	12	.008	3
428		min	-1.215	8	-.048	8	0	1	0	1	0	1	-.006	8
429	5	max	.509	3	.071	3	0	12	0	12	0	12	.053	8
430		min	-1.217	8	-.099	8	0	1	0	1	0	1	-.034	3



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
431	M13	1	max	1.721	3	.161	8	0	12	0	12	0	.077	8
432			min	-2.826	8	-.082	3	0	1	0	1	0	-.041	3
433		2	max	1.71	3	.083	8	0	12	0	12	0	.009	3
434			min	-2.827	8	-.044	3	0	1	0	1	0	-.021	8
435		3	max	1.699	3	.006	8	0	12	0	12	0	.029	3
436			min	-2.828	8	-.006	3	0	1	0	1	0	-.056	8
437		4	max	1.689	3	.033	3	0	12	0	12	0	.018	3
438			min	-2.829	8	-.072	8	0	1	0	1	0	-.03	8
439		5	max	1.678	3	.071	3	0	12	0	12	0	.058	8
440			min	-2.831	8	-.149	8	0	1	0	1	0	-.023	3
441	M18	1	max	3.246	3	.165	8	0	12	0	12	0	.08	8
442			min	-4.88	8	-.085	3	0	1	0	1	0	-.038	3
443		2	max	3.251	3	.087	8	0	12	0	12	0	.015	3
444			min	-4.88	8	-.045	3	0	1	0	1	0	-.022	8
445		3	max	3.256	3	.009	8	0	12	0	12	0	.035	3
446			min	-4.879	8	-.005	3	0	1	0	1	0	-.06	8
447		4	max	3.261	3	.035	3	0	12	0	12	0	.023	3
448			min	-4.879	8	-.069	8	0	1	0	1	0	-.036	8
449		5	max	3.267	3	.075	3	0	12	0	12	0	.052	8
450			min	-4.878	8	-.148	8	0	1	0	1	0	-.021	3
451	M19	1	max	2.574	3	.092	8	0	12	0	12	0	.025	5
452			min	-3.925	8	-.038	3	0	1	0	1	0	-.003	3
453		2	max	2.577	3	.054	8	0	12	0	12	0	.008	3
454			min	-3.924	8	-.018	3	0	1	0	1	0	-.005	12
455		3	max	2.581	3	.016	5	0	12	0	12	0	.012	3
456			min	-3.924	8	.001	3	0	1	0	1	0	-.018	8
457		4	max	2.584	3	.021	3	0	12	0	12	0	.007	3
458			min	-3.924	8	-.023	8	0	1	0	1	0	-.017	8
459		5	max	2.588	3	.04	3	0	12	0	12	0	.003	12
460			min	-3.923	8	-.062	8	0	1	0	1	0	-.005	3
461	M20	1	max	1.68	3	.147	8	0	12	0	12	0	.057	8
462			min	-2.639	8	-.071	3	0	1	0	1	0	-.023	3
463		2	max	1.69	3	.069	8	0	12	0	12	0	.019	3
464			min	-2.638	8	-.033	3	0	1	0	1	0	-.03	8
465		3	max	1.701	3	.006	3	0	12	0	12	0	.029	3
466			min	-2.636	8	-.009	8	0	1	0	1	0	-.054	8
467		4	max	1.712	3	.044	3	0	12	0	12	0	.009	3
468			min	-2.635	8	-.087	8	0	1	0	1	0	-.015	8
469		5	max	1.723	3	.083	3	0	12	0	12	0	.085	8
470			min	-2.634	8	-.164	8	0	1	0	1	0	-.042	3
471	M21	1	max	.5	3	.153	8	0	12	0	12	0	.075	8
472			min	-.896	8	-.07	3	0	1	0	1	0	-.034	3
473		2	max	.514	3	.072	8	0	12	0	12	0	.008	3
474			min	-.895	8	-.033	3	0	1	0	1	0	-.015	8
475		3	max	.527	3	.005	3	0	12	0	12	0	.019	3
476			min	-.893	8	-.009	8	0	1	0	1	0	-.04	8
477		4	max	.541	3	.042	3	0	12	0	12	0	0	6
478			min	-.891	8	-.091	8	0	1	0	1	0	-.002	12
479		5	max	.554	3	.08	3	0	12	0	12	0	.105	8
480			min	-.89	8	-.172	8	0	1	0	1	0	-.048	3
481	M22	1	max	1.29	8	.193	8	0	12	0	12	0	.12	8
482			min	-.92	3	-.084	3	0	1	0	1	0	-.052	3
483		2	max	1.293	8	.092	8	0	12	0	12	0	.009	3
484			min	-.899	3	-.04	3	0	1	0	1	0	-.021	8
485		3	max	1.295	8	.005	3	0	12	0	12	0	.026	3
486			min	-.879	3	-.008	8	0	1	0	1	0	-.063	8
487		4	max	1.298	8	.05	3	0	12	0	12	0	0	2



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
488		min	-859	3	-108	8	0	1	0	1	0	1	-006	5
489	5	max	1.3	8	.095	3	0	12	0	12	0	12	.151	8
490		min	-838	3	-.208	8	0	1	0	1	0	1	-.072	3
491	M23	1	max	6.322	8	.105	8	0	12	0	12	0	.066	8
492		min	-3.902	3	-.032	3	0	1	0	1	0	1	-.031	3
493	2	max	6.325	8	.057	8	0	12	0	12	0	12	.028	8
494		min	-3.883	3	-.019	3	0	1	0	1	0	1	-.019	3
495	3	max	6.327	8	.009	8	0	12	0	12	0	12	.013	8
496		min	-3.864	3	-.006	3	0	1	0	1	0	1	-.013	3
497	4	max	6.329	8	.008	3	0	12	0	12	0	12	.02	8
498		min	-3.845	3	-.039	8	0	1	0	1	0	1	-.014	3
499	5	max	6.331	8	.021	3	0	12	0	12	0	12	.049	8
500		min	-3.827	3	-.086	8	0	1	0	1	0	1	-.02	3
501	M24	1	max	6.275	8	.061	5	0	12	0	12	0	.037	8
502		min	-3.791	3	-.002	3	0	1	0	1	0	1	-.014	3
503	2	max	6.276	8	.025	5	0	12	0	12	0	12	.021	8
504		min	-3.775	3	.001	1	0	1	0	1	0	1	-.014	3
505	3	max	6.278	8	.011	3	0	12	0	12	0	12	.019	8
506		min	-3.759	3	-.016	12	0	1	0	1	0	1	-.017	3
507	4	max	6.28	8	.017	3	0	12	0	12	0	12	.031	8
508		min	-3.742	3	-.05	8	0	1	0	1	0	1	-.022	3
509	5	max	6.282	8	.024	3	0	12	0	12	0	12	.055	8
510		min	-3.726	3	-.087	8	0	1	0	1	0	1	-.029	3
511	M25	1	max	5.939	8	.067	12	0	12	0	12	0	.039	12
512		min	-3.31	3	-.036	5	0	1	0	1	0	1	-.028	3
513	2	max	5.941	8	.039	12	0	12	0	12	0	12	.042	8
514		min	-3.305	3	-.015	6	0	1	0	1	0	1	-.022	3
515	3	max	5.944	8	.016	8	0	12	0	12	0	12	.04	8
516		min	-3.301	3	-.012	3	0	1	0	1	0	1	-.017	3
517	4	max	5.946	8	.041	8	0	12	0	12	0	12	.027	8
518		min	-3.297	3	-.022	10	0	1	0	1	0	1	-.012	3
519	5	max	5.949	8	.067	8	0	12	0	12	0	12	.022	12
520		min	-3.292	3	-.049	9	0	1	0	1	0	1	-.007	3
521	M26	1	max	5.896	8	0	2	0	12	0	12	0	.019	8
522		min	-3.257	3	-.046	9	0	1	0	1	0	1	-.016	3
523	2	max	5.898	8	0	2	0	12	0	12	0	12	.027	8
524		min	-3.253	3	-.014	5	0	1	0	1	0	1	-.016	3
525	3	max	5.9	8	.022	12	0	12	0	12	0	12	.029	8
526		min	-3.25	3	0	3	0	1	0	1	0	1	-.016	3
527	4	max	5.902	8	.056	12	0	12	0	12	0	12	.023	8
528		min	-3.247	3	0	3	0	1	0	1	0	1	-.016	3
529	5	max	5.904	8	.089	12	0	12	0	12	0	12	.011	8
530		min	-3.243	3	0	3	0	1	0	1	0	1	-.021	10
531	M27	1	max	4.276	8	-.001	2	0	12	0	12	0	.004	8
532		min	-2.155	3	-.127	9	0	1	0	1	0	1	-.036	10
533	2	max	4.28	8	-.001	2	0	12	0	12	0	12	.037	8
534		min	-2.148	3	-.061	9	0	1	0	1	0	1	-.016	3
535	3	max	4.284	8	.01	8	0	12	0	12	0	12	.051	12
536		min	-2.141	3	-.005	3	0	1	0	1	0	1	-.012	3
537	4	max	4.288	8	.072	12	0	12	0	12	0	12	.024	12
538		min	-2.135	3	-.005	3	0	1	0	1	0	1	-.009	3
539	5	max	4.292	8	.139	12	0	12	0	12	0	12	-.001	2
540		min	-2.128	3	-.005	3	0	1	0	1	0	1	-.048	9
541	M28	1	max	2.281	8	0	2	0	12	0	12	0	-.003	2
542		min	-.95	3	-.115	9	0	1	0	1	0	1	-.034	9
543	2	max	2.285	8	0	2	0	12	0	12	0	12	.021	8
544		min	-.944	3	-.054	9	0	1	0	1	0	1	-.01	3



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC	
545	3	max	2.289	8	.008	8	0	12	0	12	0	12	.034	12	
546		min	-938	3	-.003	3	0	1	0	1	0	1	-.008	3	
547	4	max	2.292	8	.068	12	0	12	0	12	0	12	.012	8	
548		min	-.932	3	-.003	3	0	1	0	1	0	1	-.006	3	
549	5	max	2.296	8	.129	12	0	12	0	12	0	12	0	2	
550		min	-.926	3	-.003	3	0	1	0	1	0	1	-.051	9	
551	M29	1	max	.566	10	0	2	0	12	0	12	0	12	-.002	2
552		min	-.465	8	-.152	9	0	1	0	1	0	1	-.066	9	
553	2	max	.574	10	0	2	0	12	0	12	0	12	.025	12	
554		min	-.461	8	-.075	9	0	1	0	1	0	1	-.005	3	
555	3	max	.582	10	.005	8	0	12	0	12	0	12	.054	12	
556		min	-.456	8	-.003	3	0	1	0	1	0	1	-.003	3	
557	4	max	.589	10	.08	12	0	12	0	12	0	12	.021	9	
558		min	-.451	8	-.003	3	0	1	0	1	0	1	0	3	
559	5	max	.597	10	.158	12	0	12	0	12	0	12	.003	3	
560		min	-.447	8	-.003	3	0	1	0	1	0	1	-.074	12	
561	M133	1	max	4.738	8	.124	8	0	12	0	12	0	12	.079	8
562		min	-2.935	3	-.049	3	0	1	0	1	0	1	-.039	3	
563	2	max	4.736	8	.073	8	0	12	0	12	0	12	.031	8	
564		min	-2.951	3	-.031	3	0	1	0	1	0	1	-.019	3	
565	3	max	4.734	8	.023	8	0	12	0	12	0	12	.007	8	
566		min	-2.967	3	-.012	3	0	1	0	1	0	1	-.009	3	
567	4	max	4.732	8	.007	3	0	12	0	12	0	12	.008	8	
568		min	-2.983	3	-.028	8	0	1	0	1	0	1	-.007	3	
569	5	max	4.73	8	.025	3	0	12	0	12	0	12	.035	8	
570		min	-2.999	3	-.079	8	0	1	0	1	0	1	-.015	3	
571	M114A	1	max	4.706	8	.084	8	0	12	0	12	0	12	.051	8
572		min	-2.983	3	-.037	3	0	1	0	1	0	1	-.027	3	
573	2	max	4.705	8	.036	8	0	12	0	12	0	12	.023	8	
574		min	-2.994	3	-.017	3	0	1	0	1	0	1	-.015	3	
575	3	max	4.704	8	.004	3	0	12	0	12	0	12	.017	8	
576		min	-3.005	3	-.012	8	0	1	0	1	0	1	-.012	3	
577	4	max	4.702	8	.024	3	0	12	0	12	0	12	.034	8	
578		min	-3.017	3	-.06	8	0	1	0	1	0	1	-.018	3	
579	5	max	4.701	8	.045	3	0	12	0	12	0	12	.073	8	
580		min	-3.028	3	-.107	8	0	1	0	1	0	1	-.034	3	
581	M112B	1	max	3.646	3	.187	8	0	12	0	12	0	12	.096	8
582		min	-5.434	8	-.096	3	0	1	0	1	0	1	-.046	3	
583	2	max	3.644	3	.092	8	0	12	0	12	0	12	.025	3	
584		min	-5.434	8	-.048	3	0	1	0	1	0	1	-.04	8	
585	3	max	3.642	3	.001	3	0	12	0	12	0	12	.047	3	
586		min	-5.435	8	-.003	8	0	1	0	1	0	1	-.084	8	
587	4	max	3.639	3	.05	3	0	12	0	12	0	12	.022	3	
588		min	-5.435	8	-.098	8	0	1	0	1	0	1	-.034	8	
589	5	max	3.637	3	.099	3	0	12	0	12	0	12	.109	8	
590		min	-5.435	8	-.193	8	0	1	0	1	0	1	-.051	3	
591	M125A	1	max	3.642	3	.194	8	0	12	0	12	0	12	.11	8
592		min	-5.479	8	-.099	3	0	1	0	1	0	1	-.051	3	
593	2	max	3.644	3	.099	8	0	12	0	12	0	12	.023	3	
594		min	-5.478	8	-.05	3	0	1	0	1	0	1	-.035	8	
595	3	max	3.646	3	.003	8	0	12	0	12	0	12	.048	3	
596		min	-5.478	8	-.001	3	0	1	0	1	0	1	-.085	8	
597	4	max	3.649	3	.048	3	0	12	0	12	0	12	.025	3	
598		min	-5.478	8	-.092	8	0	1	0	1	0	1	-.041	8	
599	5	max	3.651	3	.097	3	0	12	0	12	0	12	.098	8	
600		min	-5.478	8	-.188	8	0	1	0	1	0	1	-.047	3	
601	M125B	1	max	.851	12	.124	8	0	12	0	12	0	12	.089	8



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
602		min	-.834	3	-.09	3	0	1	0	1	0	1	-.065	3
603	2	max	.849	12	.065	8	0	12	0	12	0	12	.005	12
604		min	-.853	3	-.047	3	0	1	0	1	0	1	0	1
605	3	max	.847	12	.006	8	0	12	0	12	0	12	.024	3
606		min	-.872	3	-.004	3	0	1	0	1	0	1	-.034	8
607	4	max	.845	12	.039	3	0	12	0	12	0	12	.007	3
608		min	-.891	3	-.053	8	0	1	0	1	0	1	-.012	8
609	5	max	.842	12	.081	3	0	12	0	12	0	12	.066	8
610		min	-.91	3	-.112	8	0	1	0	1	0	1	-.049	3
611	M125C	1	max	3.281	8	.069	8	0	12	0	12	0	.047	8
612		min	-3.095	3	-.052	3	0	1	0	1	0	1	-.04	3
613	2	max	3.279	8	.036	8	0	12	0	12	0	12	.02	8
614		min	-3.108	3	-.029	3	0	1	0	1	0	1	-.019	3
615	3	max	3.278	8	.004	12	0	12	0	12	0	12	.01	8
616		min	-3.122	3	-.006	3	0	1	0	1	0	1	-.01	3
617	4	max	3.276	8	.016	3	0	12	0	12	0	12	.017	8
618		min	-3.135	3	-.031	8	0	1	0	1	0	1	-.012	3
619	5	max	3.275	8	.039	3	0	12	0	12	0	12	.042	8
620		min	-3.148	3	-.064	8	0	1	0	1	0	1	-.027	3
621	M126	1	max	1.658	3	-.005	8	0	12	0	12	0	-.003	2
622		min	-3.061	8	-.06	10	0	1	0	1	0	1	-.029	9
623	2	max	1.661	3	.014	8	0	12	0	12	0	12	0	2
624		min	-3.059	8	-.035	10	0	1	0	1	0	1	-.014	9
625	3	max	1.664	3	.034	8	0	12	0	12	0	12	.007	3
626		min	-3.057	8	-.026	3	0	1	0	1	0	1	-.016	8
627	4	max	1.668	3	.053	8	0	12	0	12	0	12	.016	3
628		min	-3.055	8	-.026	3	0	1	0	1	0	1	-.031	8
629	5	max	1.671	3	.075	12	0	12	0	12	0	12	.025	3
630		min	-3.053	8	-.026	3	0	1	0	1	0	1	-.052	8
631	M128	1	max	.475	3	.106	5	0	12	0	12	0	.049	5
632		min	-.772	8	0	1	0	1	0	1	0	1	0	1
633	2	max	.467	3	.051	5	0	12	0	12	0	12	0	2
634		min	-.777	8	0	1	0	1	0	1	0	1	-.013	8
635	3	max	.459	3	.003	3	0	12	0	12	0	12	0	2
636		min	-.782	8	-.003	8	0	1	0	1	0	1	-.033	5
637	4	max	.452	3	.003	3	0	12	0	12	0	12	-.001	2
638		min	-.786	8	-.058	8	0	1	0	1	0	1	-.01	6
639	5	max	.444	3	.003	3	0	12	0	12	0	12	.059	8
640		min	-.791	8	-.112	8	0	1	0	1	0	1	-.008	3
641	M139	1	max	3.229	3	.145	8	0	12	0	12	0	.05	8
642		min	-4.919	8	-.074	3	0	1	0	1	0	1	-.021	3
643	2	max	3.224	3	.068	8	0	12	0	12	0	12	.022	3
644		min	-4.92	8	-.034	3	0	1	0	1	0	1	-.036	8
645	3	max	3.219	3	.005	3	0	12	0	12	0	12	.034	3
646		min	-4.92	8	-.009	8	0	1	0	1	0	1	-.059	8
647	4	max	3.214	3	.045	3	0	12	0	12	0	12	.014	3
648		min	-4.921	8	-.087	8	0	1	0	1	0	1	-.021	8
649	5	max	3.209	3	.084	3	0	12	0	12	0	12	.08	8
650		min	-4.921	8	-.164	8	0	1	0	1	0	1	-.037	3
651	M140	1	max	2.609	3	.097	8	0	12	0	12	0	.033	8
652		min	-4.062	8	-.043	3	0	1	0	1	0	1	-.01	3
653	2	max	2.605	3	.058	8	0	12	0	12	0	12	.004	10
654		min	-4.062	8	-.023	3	0	1	0	1	0	1	.001	8
655	3	max	2.6	3	.02	5	0	12	0	12	0	12	.009	3
656		min	-4.063	8	-.004	3	0	1	0	1	0	1	-.014	8
657	4	max	2.596	3	.016	3	0	12	0	12	0	12	.007	3
658		min	-4.063	8	-.019	8	0	1	0	1	0	1	-.014	8



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
659	5	max	2.592	3	.036	3	0	12	0	12	0	12	.001	8
660		min	-4.064	8	-.058	8	0	1	0	1	0	1	-.004	10
661	M137A	1	max	2.588	3	.06	8	0	12	0	12	0	.003	12
662		min	-3.924	8	-.037	3	0	1	0	1	0	1	-.005	3
663		2	max	2.592	3	.019	8	0	12	0	12	0	.006	3
664		min	-3.924	8	-.017	3	0	1	0	1	0	1	-.015	8
665		3	max	2.596	3	.003	3	0	12	0	12	0	.009	3
666		min	-3.923	8	-.022	5	0	1	0	1	0	1	-.015	8
667		4	max	2.601	3	.022	3	0	12	0	12	0	.004	6
668		min	-3.923	8	-.062	8	0	1	0	1	0	1	-.002	12
669		5	max	2.605	3	.042	3	0	12	0	12	0	.035	5
670		min	-3.922	8	-.103	8	0	1	0	1	0	1	-.009	3
671	M138	1	max	2.592	3	.064	8	0	12	0	12	0	.001	8
672		min	-4.063	8	-.039	3	0	1	0	1	0	1	-.004	10
673		2	max	2.589	3	.026	8	0	12	0	12	0	.008	3
674		min	-4.063	8	-.02	3	0	1	0	1	0	1	-.017	8
675		3	max	2.585	3	0	3	0	12	0	12	0	.012	3
676		min	-4.064	8	-.014	5	0	1	0	1	0	1	-.019	8
677		4	max	2.581	3	.019	3	0	12	0	12	0	.008	3
678		min	-4.064	8	-.052	8	0	1	0	1	0	1	-.006	8
679		5	max	2.578	3	.039	3	0	12	0	12	0	.023	5
680		min	-4.064	8	-.09	8	0	1	0	1	0	1	-.003	3
681	M70	1	max	.523	8	.005	3	0	12	0	12	0	.003	3
682		min	-.969	3	0	12	0	1	0	1	0	1	0	8
683		2	max	.523	8	.005	3	0	12	0	12	0	0	3
684		min	-.97	3	0	12	0	1	0	1	0	1	-.001	8
685		3	max	.522	8	.004	3	0	12	0	12	0	0	12
686		min	-.97	3	0	12	0	1	0	1	0	1	-.002	6
687		4	max	.522	8	.004	3	0	12	0	12	0	0	12
688		min	-.971	3	0	12	0	1	0	1	0	1	-.004	3
689		5	max	.521	8	.003	3	0	12	0	12	0	0	12
690		min	-.972	3	-.001	12	0	1	0	1	0	1	-.006	3
691	M71	1	max	.843	3	.011	8	0	12	0	12	0	.015	8
692		min	-.744	8	-.008	3	0	1	0	1	0	1	-.01	3
693		2	max	.843	3	.011	8	0	12	0	12	0	.009	8
694		min	-.745	8	-.008	3	0	1	0	1	0	1	-.006	3
695		3	max	.842	3	.012	8	0	12	0	12	0	.004	8
696		min	-.745	8	-.007	3	0	1	0	1	0	1	-.003	3
697		4	max	.842	3	.012	8	0	12	0	12	0	0	3
698		min	-.745	8	-.007	3	0	1	0	1	0	1	-.002	8
699		5	max	.841	3	.012	8	0	12	0	12	0	.004	3
700		min	-.746	8	-.006	3	0	1	0	1	0	1	-.008	8
701	M72	1	max	.661	8	.001	2	0	12	0	12	0	.001	12
702		min	-.753	3	-.003	8	0	1	0	1	0	1	-.003	3
703		2	max	.661	8	0	2	0	12	0	12	0	.001	12
704		min	-.753	3	-.003	8	0	1	0	1	0	1	-.004	3
705		3	max	.661	8	0	2	0	12	0	12	0	.003	8
706		min	-.754	3	-.004	8	0	1	0	1	0	1	-.004	3
707		4	max	.661	8	0	2	0	12	0	12	0	.004	8
708		min	-.754	3	-.004	5	0	1	0	1	0	1	-.004	3
709		5	max	.66	8	0	2	0	12	0	12	0	.006	8
710		min	-.755	3	-.004	5	0	1	0	1	0	1	-.003	3
711	M73	1	max	.937	3	0	8	0	12	0	12	0	.004	8
712		min	-1.103	8	-.004	3	0	1	0	1	0	1	-.009	3
713		2	max	.936	3	.001	8	0	12	0	12	0	.004	8
714		min	-1.104	8	-.004	3	0	1	0	1	0	1	-.007	3
715		3	max	.935	3	.001	8	0	12	0	12	0	.003	8



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
716		min	-1.104	8	-.003	3	0	1	0	1	0	1	-.005	3
717	4	max	.935	3	.002	8	0	12	0	12	0	12	.003	8
718		min	-1.105	8	-.003	3	0	1	0	1	0	1	-.003	3
719	5	max	.934	3	.002	5	0	12	0	12	0	12	.002	8
720		min	-1.105	8	-.002	3	0	1	0	1	0	1	-.002	3
721	M74	1	max	.865	8	.007	5	0	12	0	12	0	.008	8
722		min	-.715	3	.001	1	0	1	0	1	0	1	-.005	3
723	2	max	.865	8	.007	5	0	12	0	12	0	12	.005	8
724		min	-.715	3	0	1	0	1	0	1	0	1	-.006	3
725	3	max	.865	8	.006	5	0	12	0	12	0	12	.003	8
726		min	-.716	3	0	1	0	1	0	1	0	1	-.006	3
727	4	max	.865	8	.006	8	0	12	0	12	0	12	.001	12
728		min	-.716	3	0	1	0	1	0	1	0	1	-.007	3
729	5	max	.864	8	.005	8	0	12	0	12	0	12	0	12
730		min	-.716	3	0	1	0	1	0	1	0	1	-.007	3
731	M75	1	max	.847	3	.01	8	0	12	0	12	0	.017	8
732		min	-1.218	8	-.004	3	0	1	0	1	0	1	-.01	3
733	2	max	.846	3	.01	8	0	12	0	12	0	12	.012	8
734		min	-1.218	8	-.004	3	0	1	0	1	0	1	-.008	3
735	3	max	.846	3	.01	8	0	12	0	12	0	12	.007	8
736		min	-1.218	8	-.003	3	0	1	0	1	0	1	-.006	3
737	4	max	.845	3	.01	8	0	12	0	12	0	12	.002	12
738		min	-1.219	8	-.003	3	0	1	0	1	0	1	-.005	3
739	5	max	.845	3	.011	5	0	12	0	12	0	12	0	12
740		min	-1.219	8	-.002	3	0	1	0	1	0	1	-.004	6
741	M76	1	max	.632	8	.001	9	0	12	0	12	0	.011	8
742		min	-.249	3	0	3	0	1	0	1	0	1	-.011	3
743	2	max	.632	8	.001	9	0	12	0	12	0	12	.01	8
744		min	-.249	3	0	3	0	1	0	1	0	1	-.011	3
745	3	max	.631	8	0	12	0	12	0	12	0	12	.01	8
746		min	-.25	3	0	3	0	1	0	1	0	1	-.011	3
747	4	max	.631	8	0	12	0	12	0	12	0	12	.01	8
748		min	-.251	3	-.001	3	0	1	0	1	0	1	-.01	3
749	5	max	.631	8	0	12	0	12	0	12	0	12	.01	8
750		min	-.251	3	-.001	3	0	1	0	1	0	1	-.009	3
751	M77	1	max	-.018	2	.002	8	0	12	0	12	0	.012	8
752		min	-.321	5	-.001	1	0	1	0	1	0	1	-.009	3
753	2	max	-.018	2	.003	8	0	12	0	12	0	12	.011	8
754		min	-.321	5	0	1	0	1	0	1	0	1	-.009	3
755	3	max	-.019	2	.003	8	0	12	0	12	0	12	.01	8
756		min	-.322	5	0	1	0	1	0	1	0	1	-.009	3
757	4	max	-.019	2	.004	5	0	12	0	12	0	12	.008	8
758		min	-.322	5	0	1	0	1	0	1	0	1	-.009	3
759	5	max	-.019	2	.004	5	0	12	0	12	0	12	.006	8
760		min	-.322	5	.001	1	0	1	0	1	0	1	-.01	3
761	M78	1	max	.612	3	0	9	0	12	0	12	0	.007	8
762		min	-.318	8	0	8	0	1	0	1	0	1	-.007	3
763	2	max	.612	3	0	9	0	12	0	12	0	12	.007	8
764		min	-.319	8	0	8	0	1	0	1	0	1	-.007	3
765	3	max	.611	3	0	12	0	12	0	12	0	12	.008	8
766		min	-.319	8	0	5	0	1	0	1	0	1	-.007	3
767	4	max	.61	3	0	12	0	12	0	12	0	12	.008	8
768		min	-.32	8	-.001	5	0	1	0	1	0	1	-.007	3
769	5	max	.609	3	0	12	0	12	0	12	0	12	.009	8
770		min	-.32	8	-.001	5	0	1	0	1	0	1	-.007	3
771	M79	1	max	-.012	2	.004	3	0	12	0	12	0	.006	8
772		min	-.234	9	-.005	5	0	1	0	1	0	1	-.004	3



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
773	2	max	-.012	2	.005	3	0	12	0	12	0	12	.009	8
774		min	-.234	9	-.004	8	0	1	0	1	0	1	-.006	3
775	3	max	-.012	2	.005	3	0	12	0	12	0	12	.011	8
776		min	-.234	9	-.004	8	0	1	0	1	0	1	-.009	3
777	4	max	-.012	2	.006	3	0	12	0	12	0	12	.012	8
778		min	-.234	9	-.003	8	0	1	0	1	0	1	-.012	3
779	5	max	-.012	2	.007	3	0	12	0	12	0	12	.014	8
780		min	-.234	9	-.003	8	0	1	0	1	0	1	-.015	3
781	M80	1	max	1.471	3	0	12	0	12	0	12	0	.01	8
782		min	-1.644	8	-.002	6	0	1	0	1	0	1	-.011	3
783	2	max	1.47	3	0	12	0	12	0	12	0	12	.011	8
784		min	-1.644	8	-.002	6	0	1	0	1	0	1	-.01	3
785	3	max	1.47	3	0	12	0	12	0	12	0	12	.012	8
786		min	-1.644	8	-.001	6	0	1	0	1	0	1	-.009	3
787	4	max	1.469	3	.001	9	0	12	0	12	0	12	.012	8
788		min	-1.645	8	0	8	0	1	0	1	0	1	-.009	3
789	5	max	1.468	3	.002	9	0	12	0	12	0	12	.013	8
790		min	-1.645	8	0	8	0	1	0	1	0	1	-.009	3
791	M81	1	max	1.472	8	0	12	0	12	0	12	0	.005	12
792		min	-1.254	3	-.002	5	0	1	0	1	0	1	-.003	3
793	2	max	1.472	8	0	10	0	12	0	12	0	12	.005	12
794		min	-1.254	3	0	5	0	1	0	1	0	1	-.003	3
795	3	max	1.472	8	.001	10	0	12	0	12	0	12	.005	8
796		min	-1.253	3	0	8	0	1	0	1	0	1	-.003	3
797	4	max	1.472	8	.002	10	0	12	0	12	0	12	.004	8
798		min	-1.253	3	0	8	0	1	0	1	0	1	-.004	3
799	5	max	1.472	8	.003	10	0	12	0	12	0	12	.004	8
800		min	-1.253	3	.001	8	0	1	0	1	0	1	-.005	3
801	M82	1	max	1.117	3	.003	3	0	12	0	12	0	.004	3
802		min	-1.364	8	-.007	8	0	1	0	1	0	1	-.008	8
803	2	max	1.117	3	.003	3	0	12	0	12	0	12	.003	3
804		min	-1.364	8	-.007	8	0	1	0	1	0	1	-.005	8
805	3	max	1.116	3	.004	3	0	12	0	12	0	12	0	10
806		min	-1.365	8	-.006	8	0	1	0	1	0	1	-.002	8
807	4	max	1.115	3	.004	3	0	12	0	12	0	12	.002	12
808		min	-1.365	8	-.006	8	0	1	0	1	0	1	-.001	3
809	5	max	1.115	3	.004	3	0	12	0	12	0	12	.005	8
810		min	-1.366	8	-.006	8	0	1	0	1	0	1	-.004	3
811	M83	1	max	1.061	8	.007	8	0	12	0	12	0	.01	8
812		min	-.845	3	-.005	3	0	1	0	1	0	1	-.005	3
813	2	max	1.061	8	.008	8	0	12	0	12	0	12	.006	8
814		min	-.845	3	-.004	3	0	1	0	1	0	1	-.003	3
815	3	max	1.062	8	.008	8	0	12	0	12	0	12	.002	5
816		min	-.844	3	-.003	3	0	1	0	1	0	1	0	3
817	4	max	1.062	8	.008	8	0	12	0	12	0	12	0	3
818		min	-.844	3	-.002	3	0	1	0	1	0	1	-.003	8
819	5	max	1.062	8	.009	5	0	12	0	12	0	12	.002	3
820		min	-.844	3	-.002	3	0	1	0	1	0	1	-.007	8
821	M84	1	max	.869	3	.004	3	0	12	0	12	0	.005	3
822		min	-1.157	8	-.013	8	0	1	0	1	0	1	-.012	8
823	2	max	.868	3	.004	3	0	12	0	12	0	12	.003	3
824		min	-1.158	8	-.013	8	0	1	0	1	0	1	-.006	8
825	3	max	.868	3	.004	3	0	12	0	12	0	12	.002	9
826		min	-1.158	8	-.013	8	0	1	0	1	0	1	0	1
827	4	max	.867	3	.005	3	0	12	0	12	0	12	.008	8
828		min	-1.158	8	-.013	8	0	1	0	1	0	1	-.002	3
829	5	max	.866	3	.005	3	0	12	0	12	0	12	.014	8



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
830		min	-1.159	8	-0.12	8	0	1	0	1	0	1	-0.04	3
831	M85	1	max	.979	8	0	3	0	12	0	12	0	.003	3
832		min	-.745	3	-.006	9	0	1	0	1	0	1	-.01	8
833		2	max	.979	8	0	3	0	12	0	12	0	.003	3
834		min	-.745	3	-.005	9	0	1	0	1	0	1	-.008	8
835		3	max	.979	8	0	3	0	12	0	12	0	.003	3
836		min	-.745	3	-.005	12	0	1	0	1	0	1	-.005	8
837		4	max	.979	8	.002	3	0	12	0	12	0	.002	3
838		min	-.745	3	-.004	12	0	1	0	1	0	1	-.003	8
839		5	max	.979	8	.002	3	0	12	0	12	0	.002	10
840		min	-.744	3	-.004	12	0	1	0	1	0	1	-.002	5
841	M86	1	max	.631	3	.002	8	0	12	0	12	0	.004	3
842		min	-.873	8	-.002	3	0	1	0	1	0	1	-.006	8
843		2	max	.63	3	.003	8	0	12	0	12	0	.005	3
844		min	-.873	8	-.002	3	0	1	0	1	0	1	-.007	8
845		3	max	.629	3	.003	8	0	12	0	12	0	.006	3
846		min	-.874	8	-.002	3	0	1	0	1	0	1	-.009	8
847		4	max	.629	3	.003	5	0	12	0	12	0	.007	3
848		min	-.874	8	-.001	3	0	1	0	1	0	1	-.01	8
849		5	max	.628	3	.004	5	0	12	0	12	0	.007	3
850		min	-.874	8	0	3	0	1	0	1	0	1	-.012	8
851	M87	1	max	.783	8	.014	8	0	12	0	12	0	.013	8
852		min	-.62	3	-.009	3	0	1	0	1	0	1	-.006	3
853		2	max	.784	8	.015	8	0	12	0	12	0	.006	8
854		min	-.62	3	-.008	3	0	1	0	1	0	1	-.002	3
855		3	max	.784	8	.015	8	0	12	0	12	0	.002	3
856		min	-.619	3	-.008	3	0	1	0	1	0	1	-.002	8
857		4	max	.784	8	.015	8	0	12	0	12	0	.006	3
858		min	-.619	3	-.007	3	0	1	0	1	0	1	-.01	8
859		5	max	.784	8	.016	8	0	12	0	12	0	.01	3
860		min	-.618	3	-.006	3	0	1	0	1	0	1	-.018	8
861	M88	1	max	.4	3	.009	3	0	12	0	12	0	.013	3
862		min	-.546	8	-.017	8	0	1	0	1	0	1	-.022	8
863		2	max	.399	3	.009	3	0	12	0	12	0	.008	3
864		min	-.547	8	-.017	8	0	1	0	1	0	1	-.013	8
865		3	max	.399	3	.01	3	0	12	0	12	0	.003	3
866		min	-.547	8	-.017	8	0	1	0	1	0	1	-.004	8
867		4	max	.398	3	.01	3	0	12	0	12	0	.005	8
868		min	-.547	8	-.017	8	0	1	0	1	0	1	-.002	3
869		5	max	.398	3	.011	3	0	12	0	12	0	.013	8
870		min	-.548	8	-.016	8	0	1	0	1	0	1	-.007	3
871	M89	1	max	.584	8	.001	3	0	12	0	12	0	.01	3
872		min	-.465	3	-.003	5	0	1	0	1	0	1	-.014	8
873		2	max	.584	8	.002	3	0	12	0	12	0	.009	3
874		min	-.465	3	-.003	8	0	1	0	1	0	1	-.013	8
875		3	max	.584	8	.003	3	0	12	0	12	0	.008	3
876		min	-.464	3	-.002	8	0	1	0	1	0	1	-.011	8
877		4	max	.585	8	.003	3	0	12	0	12	0	.007	3
878		min	-.464	3	-.002	8	0	1	0	1	0	1	-.01	8
879		5	max	.585	8	.004	3	0	12	0	12	0	.005	3
880		min	-.463	3	-.002	8	0	1	0	1	0	1	-.009	8
881	M90	1	max	.23	3	.005	3	0	12	0	12	0	.011	3
882		min	-.306	8	-.013	8	0	1	0	1	0	1	-.019	8
883		2	max	.229	3	.006	3	0	12	0	12	0	.008	3
884		min	-.307	8	-.013	8	0	1	0	1	0	1	-.012	8
885		3	max	.229	3	.006	3	0	12	0	12	0	.005	3
886		min	-.307	8	-.012	8	0	1	0	1	0	1	-.005	8



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
887	4	max	.228	3	.007	3	0	12	0	12	0	12	.001	6
888		min	-.307	8	-.012	8	0	1	0	1	0	1	0	12
889	5	max	.228	3	.007	3	0	12	0	12	0	12	.007	8
890		min	-.307	8	-.012	8	0	1	0	1	0	1	-.002	3
891	M91	1	max	.429	8	.002	8	0	12	0	12	0	.007	3
892		min	-.356	3	-.002	3	0	1	0	1	0	1	-.01	8
893	2	max	.429	8	.002	8	0	12	0	12	0	12	.008	3
894		min	-.356	3	-.001	3	0	1	0	1	0	1	-.011	8
895	3	max	.429	8	.002	8	0	12	0	12	0	12	.009	3
896		min	-.355	3	0	3	0	1	0	1	0	1	-.013	8
897	4	max	.43	8	.003	5	0	12	0	12	0	12	.009	3
898		min	-.355	3	0	3	0	1	0	1	0	1	-.014	8
899	5	max	.43	8	.003	5	0	12	0	12	0	12	.009	3
900		min	-.355	3	0	3	0	1	0	1	0	1	-.015	8
901	M92	1	max	.058	3	0	3	0	12	0	12	0	.009	3
902		min	-.115	12	-.005	5	0	1	0	1	0	1	-.016	8
903	2	max	.057	3	0	3	0	12	0	12	0	12	.009	3
904		min	-.115	12	-.004	5	0	1	0	1	0	1	-.013	8
905	3	max	.057	3	.002	3	0	12	0	12	0	12	.008	3
906		min	-.115	12	-.004	8	0	1	0	1	0	1	-.01	8
907	4	max	.056	3	.002	3	0	12	0	12	0	12	.007	3
908		min	-.115	12	-.003	8	0	1	0	1	0	1	-.008	8
909	5	max	.056	3	.003	3	0	12	0	12	0	12	.005	3
910		min	-.116	12	-.003	8	0	1	0	1	0	1	-.006	8
911	M93	1	max	.061	3	.003	8	0	12	0	12	0	.005	3
912		min	-.124	8	-.003	3	0	1	0	1	0	1	-.006	8
913	2	max	.061	3	.003	8	0	12	0	12	0	12	.007	3
914		min	-.124	8	-.002	3	0	1	0	1	0	1	-.008	8
915	3	max	.062	3	.004	8	0	12	0	12	0	12	.008	3
916		min	-.123	8	-.002	3	0	1	0	1	0	1	-.01	8
917	4	max	.062	3	.004	5	0	12	0	12	0	12	.009	3
918		min	-.123	8	0	3	0	1	0	1	0	1	-.013	8
919	5	max	.063	3	.005	5	0	12	0	12	0	12	.009	3
920		min	-.123	8	0	3	0	1	0	1	0	1	-.016	8
921	M94	1	max	.42	8	0	3	0	12	0	12	0	.008	3
922		min	-.323	3	-.004	5	0	1	0	1	0	1	-.015	8
923	2	max	.42	8	0	3	0	12	0	12	0	12	.009	3
924		min	-.324	3	-.003	5	0	1	0	1	0	1	-.014	8
925	3	max	.42	8	0	3	0	12	0	12	0	12	.008	3
926		min	-.324	3	-.003	8	0	1	0	1	0	1	-.012	8
927	4	max	.419	8	.001	3	0	12	0	12	0	12	.008	3
928		min	-.325	3	-.002	8	0	1	0	1	0	1	-.011	8
929	5	max	.419	8	.002	3	0	12	0	12	0	12	.007	3
930		min	-.325	3	-.002	8	0	1	0	1	0	1	-.01	8
931	M95	1	max	.207	3	.011	8	0	12	0	12	0	.006	8
932		min	-.318	8	-.007	3	0	1	0	1	0	1	-.002	3
933	2	max	.207	3	.012	8	0	12	0	12	0	12	.002	3
934		min	-.318	8	-.006	3	0	1	0	1	0	1	0	12
935	3	max	.208	3	.012	8	0	12	0	12	0	12	.005	3
936		min	-.318	8	-.006	3	0	1	0	1	0	1	-.006	8
937	4	max	.208	3	.012	8	0	12	0	12	0	12	.008	3
938		min	-.317	8	-.005	3	0	1	0	1	0	1	-.012	8
939	5	max	.209	3	.013	8	0	12	0	12	0	12	.011	3
940		min	-.317	8	-.005	3	0	1	0	1	0	1	-.019	8
941	M96	1	max	.644	8	.001	8	0	12	0	12	0	.005	3
942		min	-.491	3	-.004	3	0	1	0	1	0	1	-.01	8
943	2	max	.643	8	.002	8	0	12	0	12	0	12	.007	3



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
944		min	-.492	3	-.003	3	0	1	0	1	0	1	-.011	8
945	3	max	.643	8	.002	8	0	12	0	12	0	12	.008	3
946		min	-.492	3	-.003	3	0	1	0	1	0	1	-.012	8
947	4	max	.643	8	.003	8	0	12	0	12	0	12	.01	3
948		min	-.492	3	-.002	3	0	1	0	1	0	1	-.013	8
949	5	max	.643	8	.003	5	0	12	0	12	0	12	.011	3
950		min	-.493	3	-.002	3	0	1	0	1	0	1	-.014	8
951	M97	1	max	.421	3	.016	8	0	12	0	12	0	.013	8
952		min	-.617	8	-.011	3	0	1	0	1	0	1	-.008	3
953	2	max	.422	3	.016	8	0	12	0	12	0	12	.005	8
954		min	-.617	8	-.01	3	0	1	0	1	0	1	-.002	3
955	3	max	.422	3	.016	8	0	12	0	12	0	12	.003	3
956		min	-.616	8	-.01	3	0	1	0	1	0	1	-.004	8
957	4	max	.423	3	.017	8	0	12	0	12	0	12	.008	3
958		min	-.616	8	-.009	3	0	1	0	1	0	1	-.012	8
959	5	max	.423	3	.017	8	0	12	0	12	0	12	.013	3
960		min	-.616	8	-.009	3	0	1	0	1	0	1	-.021	8
961	M98	1	max	.808	8	.007	3	0	12	0	12	0	.01	3
962		min	-.616	3	-.015	8	0	1	0	1	0	1	-.017	8
963	2	max	.808	8	.007	3	0	12	0	12	0	12	.006	3
964		min	-.616	3	-.014	8	0	1	0	1	0	1	-.009	8
965	3	max	.808	8	.008	3	0	12	0	12	0	12	.002	3
966		min	-.617	3	-.014	8	0	1	0	1	0	1	-.002	8
967	4	max	.808	8	.009	3	0	12	0	12	0	12	.005	8
968		min	-.617	3	-.014	8	0	1	0	1	0	1	-.002	3
969	5	max	.807	8	.009	3	0	12	0	12	0	12	.012	8
970		min	-.617	3	-.013	8	0	1	0	1	0	1	-.007	3
971	M99	1	max	.627	3	.001	3	0	12	0	12	0	.008	3
972		min	-.923	8	-.002	9	0	1	0	1	0	1	-.01	8
973	2	max	.627	3	.001	3	0	12	0	12	0	12	.007	3
974		min	-.922	8	-.002	12	0	1	0	1	0	1	-.009	8
975	3	max	.628	3	.002	3	0	12	0	12	0	12	.006	3
976		min	-.922	8	-.002	12	0	1	0	1	0	1	-.008	8
977	4	max	.629	3	.002	3	0	12	0	12	0	12	.005	3
978		min	-.922	8	-.002	12	0	1	0	1	0	1	-.008	8
979	5	max	.629	3	.003	3	0	12	0	12	0	12	.004	3
980		min	-.921	8	-.001	12	0	1	0	1	0	1	-.007	8
981	M100	1	max	1.009	8	-.001	12	0	12	0	12	0	.001	3
982		min	-.75	3	-.002	6	0	1	0	1	0	1	-.004	5
983	2	max	1.009	8	0	12	0	12	0	12	0	12	.002	3
984		min	-.751	3	-.002	6	0	1	0	1	0	1	-.003	8
985	3	max	1.008	8	0	2	0	12	0	12	0	12	.003	3
986		min	-.751	3	-.001	6	0	1	0	1	0	1	-.003	8
987	4	max	1.008	8	0	2	0	12	0	12	0	12	.003	3
988		min	-.751	3	0	6	0	1	0	1	0	1	-.003	8
989	5	max	1.008	8	.001	2	0	12	0	12	0	12	.003	3
990		min	-.752	3	0	6	0	1	0	1	0	1	-.003	8
991	M101	1	max	.868	3	.008	8	0	12	0	12	0	.008	8
992		min	-1.3	8	-.005	3	0	1	0	1	0	1	-.005	3
993	2	max	.869	3	.008	8	0	12	0	12	0	12	.004	8
994		min	-1.299	8	-.005	3	0	1	0	1	0	1	-.002	3
995	3	max	.869	3	.008	8	0	12	0	12	0	12	0	3
996		min	-1.299	8	-.005	3	0	1	0	1	0	1	-.001	12
997	4	max	.87	3	.008	8	0	12	0	12	0	12	.003	3
998		min	-1.298	8	-.004	3	0	1	0	1	0	1	-.005	8
999	5	max	.871	3	.009	8	0	12	0	12	0	12	.005	3
1000		min	-1.298	8	-.004	3	0	1	0	1	0	1	-.009	8



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
1001	M102	1	max	1.158	8	.003	3	0	12	0	12	0	.002	3
1002			min	-836	3	-.012	5	0	1	0	1	0	-.007	8
1003		2	max	1.157	8	.004	3	0	12	0	12	0	0	3
1004			min	-836	3	-.011	8	0	1	0	1	0	-.002	12
1005		3	max	1.157	8	.004	3	0	12	0	12	0	.004	8
1006			min	-836	3	-.011	8	0	1	0	1	0	-.001	3
1007		4	max	1.157	8	.005	3	0	12	0	12	0	.01	8
1008			min	-837	3	-.01	8	0	1	0	1	0	-.004	3
1009		5	max	1.157	8	.006	3	0	12	0	12	0	.015	8
1010			min	-837	3	-.01	8	0	1	0	1	0	-.006	3
1011	M103	1	max	1.13	3	.003	8	0	12	0	12	0	0	8
1012			min	-1.763	8	-.005	3	0	1	0	1	0	-.003	3
1013		2	max	1.131	3	.004	8	0	12	0	12	0	0	2
1014			min	-1.762	8	-.004	3	0	1	0	1	0	-.002	9
1015		3	max	1.132	3	.004	8	0	12	0	12	0	.002	3
1016			min	-1.762	8	-.004	3	0	1	0	1	0	-.003	8
1017		4	max	1.132	3	.004	8	0	12	0	12	0	.004	3
1018			min	-1.762	8	-.004	3	0	1	0	1	0	-.005	8
1019		5	max	1.133	3	.004	8	0	12	0	12	0	.005	3
1020			min	-1.761	8	-.003	3	0	1	0	1	0	-.008	8
1021	M104	1	max	1.915	8	.001	8	0	12	0	12	0	.009	8
1022			min	-1.28	3	-.002	3	0	1	0	1	0	-.006	3
1023		2	max	1.915	8	.002	8	0	12	0	12	0	.008	8
1024			min	-1.28	3	-.001	3	0	1	0	1	0	-.004	3
1025		3	max	1.915	8	.003	5	0	12	0	12	0	.006	8
1026			min	-1.28	3	0	3	0	1	0	1	0	-.004	3
1027		4	max	1.915	8	.004	5	0	12	0	12	0	.004	8
1028			min	-1.28	3	0	3	0	1	0	1	0	-.004	3
1029		5	max	1.915	8	.004	5	0	12	0	12	0	.002	8
1030			min	-1.28	3	.001	3	0	1	0	1	0	-.004	3
1031	M105	1	max	1.373	3	.01	8	0	12	0	12	0	.027	8
1032			min	-2.198	8	-.004	3	0	1	0	1	0	-.013	3
1033		2	max	1.374	3	.01	8	0	12	0	12	0	.021	8
1034			min	-2.197	8	-.004	3	0	1	0	1	0	-.011	3
1035		3	max	1.374	3	.01	8	0	12	0	12	0	.016	8
1036			min	-2.197	8	-.004	3	0	1	0	1	0	-.009	3
1037		4	max	1.375	3	.01	8	0	12	0	12	0	.01	8
1038			min	-2.197	8	-.004	3	0	1	0	1	0	-.007	3
1039		5	max	1.376	3	.01	8	0	12	0	12	0	.005	8
1040			min	-2.196	8	-.003	3	0	1	0	1	0	-.005	3
1041	M106	1	max	.835	8	0	8	0	12	0	12	0	.014	8
1042			min	-.545	3	-.002	3	0	1	0	1	0	-.01	3
1043		2	max	.835	8	0	8	0	12	0	12	0	.014	8
1044			min	-.545	3	-.001	3	0	1	0	1	0	-.009	3
1045		3	max	.835	8	0	8	0	12	0	12	0	.014	8
1046			min	-.545	3	0	3	0	1	0	1	0	-.008	3
1047		4	max	.835	8	.001	5	0	12	0	12	0	.014	8
1048			min	-.545	3	0	3	0	1	0	1	0	-.008	3
1049		5	max	.835	8	.002	5	0	12	0	12	0	.013	8
1050			min	-.545	3	0	12	0	1	0	1	0	-.009	3
1051	M107	1	max	.754	3	0	3	0	12	0	12	0	.013	8
1052			min	-1.29	8	-.002	8	0	1	0	1	0	-.008	3
1053		2	max	.754	3	0	3	0	12	0	12	0	.014	8
1054			min	-1.289	8	-.002	8	0	1	0	1	0	-.009	3
1055		3	max	.755	3	0	3	0	12	0	12	0	.015	8
1056			min	-1.289	8	-.002	8	0	1	0	1	0	-.009	3
1057		4	max	.756	3	0	3	0	12	0	12	0	.015	8



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
1058		min	-1.288	8	-.002	8	0	1	0	1	0	1	-.01	3
1059	5	max	.757	3	0	3	0	12	0	12	0	12	.016	8
1060		min	-1.288	8	-.002	8	0	1	0	1	0	1	-.01	3
1061	M108	1	max	.246	3	.01	8	0	12	0	12	0	.024	8
1062		min	-.204	8	-.005	3	0	1	0	1	0	1	-.013	3
1063	2	max	.246	3	.01	8	0	12	0	12	0	12	.019	8
1064		min	-.204	8	-.004	3	0	1	0	1	0	1	-.011	3
1065	3	max	.247	3	.01	8	0	12	0	12	0	12	.014	8
1066		min	-.203	8	-.004	3	0	1	0	1	0	1	-.009	3
1067	4	max	.247	3	.011	8	0	12	0	12	0	12	.009	8
1068		min	-.203	8	-.003	3	0	1	0	1	0	1	-.007	3
1069	5	max	.247	3	.011	5	0	12	0	12	0	12	.006	12
1070		min	-.203	8	-.003	3	0	1	0	1	0	1	-.006	3
1071	M109	1	max	.099	8	.002	5	0	12	0	12	0	.019	8
1072		min	-.389	10	-.003	12	0	1	0	1	0	1	-.009	3
1073	2	max	.099	8	.002	5	0	12	0	12	0	12	.018	8
1074		min	-.389	10	-.003	12	0	1	0	1	0	1	-.009	3
1075	3	max	.099	8	.002	8	0	12	0	12	0	12	.017	8
1076		min	-.388	10	-.003	12	0	1	0	1	0	1	-.009	3
1077	4	max	.1	8	.001	8	0	12	0	12	0	12	.016	8
1078		min	-.387	10	-.004	9	0	1	0	1	0	1	-.009	3
1079	5	max	.1	8	.001	8	0	12	0	12	0	12	.015	8
1080		min	-.387	10	-.004	9	0	1	0	1	0	1	-.009	3
1081	M110	1	max	.838	3	.004	10	0	12	0	12	0	.009	8
1082		min	-1.174	8	-.002	8	0	1	0	1	0	1	-.003	3
1083	2	max	.838	3	.004	10	0	12	0	12	0	12	.01	8
1084		min	-1.174	8	-.002	8	0	1	0	1	0	1	-.005	3
1085	3	max	.839	3	.005	10	0	12	0	12	0	12	.011	8
1086		min	-1.174	8	-.002	8	0	1	0	1	0	1	-.007	3
1087	4	max	.839	3	.005	10	0	12	0	12	0	12	.012	8
1088		min	-1.173	8	-.001	8	0	1	0	1	0	1	-.009	3
1089	5	max	.84	3	.006	10	0	12	0	12	0	12	.012	8
1090		min	-1.173	8	0	8	0	1	0	1	0	1	-.011	3
1091	M111	1	max	1.22	8	.012	9	0	12	0	12	0	.02	12
1092		min	-.747	3	0	3	0	1	0	1	0	1	-.007	3
1093	2	max	1.22	8	.011	12	0	12	0	12	0	12	.016	8
1094		min	-.746	3	0	3	0	1	0	1	0	1	-.007	3
1095	3	max	1.22	8	.011	12	0	12	0	12	0	12	.013	8
1096		min	-.746	3	-.001	3	0	1	0	1	0	1	-.006	3
1097	4	max	1.22	8	.011	12	0	12	0	12	0	12	.01	8
1098		min	-.746	3	-.002	3	0	1	0	1	0	1	-.006	3
1099	5	max	1.221	8	.01	12	0	12	0	12	0	12	.007	8
1100		min	-.745	3	-.002	3	0	1	0	1	0	1	-.005	3
1101	M112	1	max	.902	3	.003	3	0	12	0	12	0	.001	8
1102		min	-1.442	8	-.009	8	0	1	0	1	0	1	-.001	3
1103	2	max	.903	3	.004	3	0	12	0	12	0	12	.006	8
1104		min	-1.441	8	-.009	8	0	1	0	1	0	1	-.003	3
1105	3	max	.903	3	.004	3	0	12	0	12	0	12	.01	8
1106		min	-1.441	8	-.009	8	0	1	0	1	0	1	-.005	3
1107	4	max	.904	3	.004	3	0	12	0	12	0	12	.015	8
1108		min	-1.441	8	-.008	8	0	1	0	1	0	1	-.007	3
1109	5	max	.905	3	.005	3	0	12	0	12	0	12	.019	8
1110		min	-1.44	8	-.008	8	0	1	0	1	0	1	-.009	3
1111	M113	1	max	1.403	8	0	3	0	12	0	12	0	.003	8
1112		min	-.753	3	-.004	12	0	1	0	1	0	1	-.003	3
1113	2	max	1.404	8	0	3	0	12	0	12	0	12	.005	8
1114		min	-.752	3	-.004	12	0	1	0	1	0	1	-.004	3



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
1115	3	max	1.404	8	0	3	0	12	0	12	0	12	.006	8
1116		min	-.752	3	-.005	9	0	1	0	1	0	1	-.004	3
1117	4	max	1.404	8	0	3	0	12	0	12	0	12	.008	8
1118		min	-.751	3	-.005	9	0	1	0	1	0	1	-.003	3
1119	5	max	1.404	8	-.001	3	0	12	0	12	0	12	.009	8
1120		min	-.751	3	-.006	9	0	1	0	1	0	1	-.003	3
1121	M114	1	max	.838	3	.006	3	0	12	0	12	0	.004	10
1122		min	-1.535	8	-.009	8	0	1	0	1	0	1	-.003	8
1123	2	max	.838	3	.007	3	0	12	0	12	0	12	.003	9
1124		min	-1.535	8	-.008	8	0	1	0	1	0	1	0	1
1125	3	max	.839	3	.007	3	0	12	0	12	0	12	.005	8
1126		min	-1.535	8	-.008	8	0	1	0	1	0	1	-.003	3
1127	4	max	.839	3	.008	3	0	12	0	12	0	12	.009	8
1128		min	-1.534	8	-.008	8	0	1	0	1	0	1	-.006	3
1129	5	max	.84	3	.008	3	0	12	0	12	0	12	.013	8
1130		min	-1.534	8	-.008	8	0	1	0	1	0	1	-.01	3
1131	M115	1	max	2.059	8	.011	12	0	12	0	12	0	.018	12
1132		min	-.973	3	-.003	3	0	1	0	1	0	1	-.006	3
1133	2	max	2.059	8	.011	12	0	12	0	12	0	12	.012	12
1134		min	-.972	3	-.004	3	0	1	0	1	0	1	-.004	3
1135	3	max	2.06	8	.01	12	0	12	0	12	0	12	.006	12
1136		min	-.972	3	-.004	3	0	1	0	1	0	1	-.002	3
1137	4	max	2.06	8	.01	12	0	12	0	12	0	12	0	3
1138		min	-.971	3	-.005	3	0	1	0	1	0	1	0	8
1139	5	max	2.061	8	.01	12	0	12	0	12	0	12	.003	3
1140		min	-.97	3	-.005	3	0	1	0	1	0	1	-.006	8
1141	M120	1	max	.657	3	.019	8	0	12	0	12	0	.011	8
1142		min	-.656	8	-.016	3	0	1	0	1	0	1	-.01	3
1143	2	max	.657	3	.02	8	0	12	0	12	0	12	.005	8
1144		min	-.656	8	-.016	3	0	1	0	1	0	1	-.004	3
1145	3	max	.657	3	.02	8	0	12	0	12	0	12	0	3
1146		min	-.656	8	-.015	3	0	1	0	1	0	1	-.002	8
1147	4	max	.657	3	.02	8	0	12	0	12	0	12	.006	3
1148		min	-.656	8	-.015	3	0	1	0	1	0	1	-.009	8
1149	5	max	.657	3	.02	8	0	12	0	12	0	12	.011	3
1150		min	-.656	8	-.014	3	0	1	0	1	0	1	-.015	8
1151	M122	1	max	.53	3	.006	8	0	12	0	12	0	.004	8
1152		min	-.576	8	-.014	3	0	1	0	1	0	1	-.009	3
1153	2	max	.53	3	.006	8	0	12	0	12	0	12	.002	8
1154		min	-.577	8	-.013	3	0	1	0	1	0	1	-.005	3
1155	3	max	.53	3	.006	8	0	12	0	12	0	12	0	9
1156		min	-.577	8	-.013	3	0	1	0	1	0	1	0	3
1157	4	max	.53	3	.007	8	0	12	0	12	0	12	.004	3
1158		min	-.577	8	-.012	3	0	1	0	1	0	1	-.002	8
1159	5	max	.53	3	.007	8	0	12	0	12	0	12	.008	3
1160		min	-.577	8	-.012	3	0	1	0	1	0	1	-.004	8
1161	M124	1	max	.651	3	.018	3	0	12	0	12	0	.01	3
1162		min	-.71	8	-.015	8	0	1	0	1	0	1	-.009	8
1163	2	max	.651	3	.018	3	0	12	0	12	0	12	.005	3
1164		min	-.71	8	-.015	8	0	1	0	1	0	1	-.004	8
1165	3	max	.65	3	.018	3	0	12	0	12	0	12	.001	8
1166		min	-.711	8	-.016	8	0	1	0	1	0	1	-.001	3
1167	4	max	.65	3	.018	3	0	12	0	12	0	12	.006	8
1168		min	-.711	8	-.016	8	0	1	0	1	0	1	-.007	3
1169	5	max	.649	3	.017	3	0	12	0	12	0	12	.011	8
1170		min	-.711	8	-.016	8	0	1	0	1	0	1	-.012	3
1171	M127	1	max	.951	3	.019	8	0	12	0	12	0	.014	8



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC	
1172		min	-1.661	8	-.011	3	0	1	0	1	0	1	-.008	3	
1173	2	max	.951	3	.019	8	0	12	0	12	0	12	.008	8	
1174		min	-1.662	8	-.011	3	0	1	0	1	0	1	-.004	3	
1175	3	max	.951	3	.019	8	0	12	0	12	0	12	.001	8	
1176		min	-1.662	8	-.01	3	0	1	0	1	0	1	0	3	
1177	4	max	.951	3	.02	8	0	12	0	12	0	12	.003	3	
1178		min	-1.662	8	-.01	3	0	1	0	1	0	1	-.006	8	
1179	5	max	.95	3	.02	8	0	12	0	12	0	12	.006	3	
1180		min	-1.662	8	-.009	3	0	1	0	1	0	1	-.012	8	
1181	M129	1	max	.371	3	.013	3	0	12	0	12	0	.01	3	
1182		min	-.57	8	-.023	8	0	1	0	1	0	1	-.015	8	
1183	2	max	.371	3	.014	3	0	12	0	12	0	12	.005	3	
1184		min	-.57	8	-.023	8	0	1	0	1	0	1	-.007	8	
1185	3	max	.371	3	.014	3	0	12	0	12	0	12	0	6	
1186		min	-.57	8	-.022	8	0	1	0	1	0	1	-.003	12	
1187	4	max	.371	3	.015	3	0	12	0	12	0	12	.008	8	
1188		min	-.57	8	-.022	8	0	1	0	1	0	1	-.006	10	
1189	5	max	.371	3	.015	3	0	12	0	12	0	12	.015	8	
1190		min	-.57	8	-.022	8	0	1	0	1	0	1	-.011	10	
1191	M135	1	max	.221	8	0	12	.001	8	0	12	0	10	0	12
1192		min	-.173	3	0	1	0	9	0	1	0	8	0	1	
1193	2	max	.222	8	0	12	.001	8	0	12	0	10	0	12	
1194		min	-.173	3	0	1	0	9	0	1	0	8	0	1	
1195	3	max	.222	8	0	12	.001	8	0	12	0	3	0	12	
1196		min	-.172	3	0	1	0	9	0	1	0	12	0	1	
1197	4	max	.222	8	0	12	.001	8	0	12	0	5	0	12	
1198		min	-.172	3	0	1	0	9	0	1	0	9	0	1	
1199	5	max	.222	8	0	12	.001	8	0	12	0	8	0	12	
1200		min	-.171	3	0	1	0	9	0	1	0	9	0	1	
1201	M112A	1	max	.104	3	.041	3	0	12	0	12	0	.026	3	
1202		min	-.165	8	-.07	8	0	1	0	1	0	1	-.042	8	
1203	2	max	.104	3	.041	3	0	12	0	12	0	12	.012	3	
1204		min	-.165	8	-.07	8	0	1	0	1	0	1	-.019	8	
1205	3	max	.104	3	.041	3	0	12	0	12	0	12	.005	8	
1206		min	-.165	8	-.071	8	0	1	0	1	0	1	-.002	3	
1207	4	max	.103	3	.04	3	0	12	0	12	0	12	.029	8	
1208		min	-.165	8	-.071	8	0	1	0	1	0	1	-.016	3	
1209	5	max	.103	3	.04	3	0	12	0	12	0	12	.053	8	
1210		min	-.166	8	-.071	8	0	1	0	1	0	1	-.029	3	
1211	M113A	1	max	.278	3	.045	3	0	12	0	12	0	.026	3	
1212		min	-.353	8	-.051	8	0	1	0	1	0	1	-.03	8	
1213	2	max	.278	3	.044	3	0	12	0	12	0	12	.012	3	
1214		min	-.353	8	-.051	8	0	1	0	1	0	1	-.013	8	
1215	3	max	.277	3	.044	3	0	12	0	12	0	12	.004	8	
1216		min	-.353	8	-.052	8	0	1	0	1	0	1	-.003	3	
1217	4	max	.277	3	.044	3	0	12	0	12	0	12	.021	8	
1218		min	-.353	8	-.052	8	0	1	0	1	0	1	-.018	3	
1219	5	max	.276	3	.044	3	0	12	0	12	0	12	.038	8	
1220		min	-.354	8	-.052	8	0	1	0	1	0	1	-.032	3	
1221	M115B	1	max	.673	3	.021	3	0	12	0	12	0	.014	3	
1222		min	-1.106	8	-.028	8	0	1	0	1	0	1	-.02	8	
1223	2	max	.672	3	.02	3	0	12	0	12	0	12	.008	3	
1224		min	-1.106	8	-.028	8	0	1	0	1	0	1	-.011	8	
1225	3	max	.672	3	.02	3	0	12	0	12	0	12	0	3	
1226		min	-1.106	8	-.028	8	0	1	0	1	0	1	-.002	8	
1227	4	max	.671	3	.02	3	0	12	0	12	0	12	.007	8	
1228		min	-1.106	8	-.028	8	0	1	0	1	0	1	-.005	3	



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	y Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
1229	5	max	.671	3	.02	3	0	12	0	12	0	12	.016	8
1230		min	-1.107	8	-.028	8	0	1	0	1	0	1	-.012	3
1231	M118	1	max	.934	3	0	3	0	12	0	12	0	0	2
1232		min	-1.525	8	-.013	5	0	1	0	1	0	1	-.008	5
1233		2	max	.934	3	0	3	0	12	0	12	0	0	12
1234		min	-1.525	8	-.012	5	0	1	0	1	0	1	-.003	5
1235		3	max	.934	3	0	3	0	12	0	12	0	.003	12
1236		min	-1.525	8	-.012	8	0	1	0	1	0	1	-.001	3
1237		4	max	.934	3	0	3	0	12	0	12	0	.005	8
1238		min	-1.525	8	-.011	8	0	1	0	1	0	1	-.001	3
1239		5	max	.934	3	.001	3	0	12	0	12	0	.009	8
1240		min	-1.524	8	-.011	8	0	1	0	1	0	1	-.002	3
1241	M119	1	max	.741	3	.021	8	0	12	0	12	0	.014	8
1242		min	-1.186	8	-.012	3	0	1	0	1	0	1	-.009	3
1243		2	max	.741	3	.02	8	0	12	0	12	0	.007	8
1244		min	-1.186	8	-.012	3	0	1	0	1	0	1	-.005	3
1245		3	max	.742	3	.02	8	0	12	0	12	0	0	8
1246		min	-1.186	8	-.013	3	0	1	0	1	0	1	0	10
1247		4	max	.742	3	.02	8	0	12	0	12	0	.004	3
1248		min	-1.185	8	-.013	3	0	1	0	1	0	1	-.007	8
1249		5	max	.742	3	.02	8	0	12	0	12	0	.009	3
1250		min	-1.185	8	-.013	3	0	1	0	1	0	1	-.014	8
1251	M120A	1	max	.678	3	0	2	0	12	0	12	0	0	2
1252		min	-.784	8	-.004	10	0	1	0	1	0	1	-.003	10
1253		2	max	.679	3	0	2	0	12	0	12	0	0	2
1254		min	-.784	8	-.004	10	0	1	0	1	0	1	-.002	10
1255		3	max	.679	3	0	2	0	12	0	12	0	0	12
1256		min	-.784	8	-.005	10	0	1	0	1	0	1	0	3
1257		4	max	.679	3	-.001	2	0	12	0	12	0	.002	10
1258		min	-.783	8	-.005	10	0	1	0	1	0	1	0	1
1259		5	max	.68	3	-.002	2	0	12	0	12	0	.004	10
1260		min	-.783	8	-.006	10	0	1	0	1	0	1	0	1
1261	M121	1	max	.986	3	.013	8	0	12	0	12	0	.008	8
1262		min	-1.012	8	-.003	3	0	1	0	1	0	1	0	3
1263		2	max	.986	3	.013	8	0	12	0	12	0	.003	5
1264		min	-1.012	8	-.003	3	0	1	0	1	0	1	0	1
1265		3	max	.986	3	.013	8	0	12	0	12	0	.001	3
1266		min	-1.012	8	-.002	3	0	1	0	1	0	1	-.001	8
1267		4	max	.986	3	.013	8	0	12	0	12	0	.002	3
1268		min	-1.011	8	-.002	3	0	1	0	1	0	1	-.006	8
1269		5	max	.986	3	.014	5	0	12	0	12	0	.003	3
1270		min	-1.011	8	-.001	3	0	1	0	1	0	1	-.01	8
1271	M129A	1	max	.833	3	.011	3	0	12	0	12	0	.01	3
1272		min	-1.767	8	-.028	8	0	1	0	1	0	1	-.023	8
1273		2	max	.834	3	.011	3	0	12	0	12	0	.005	3
1274		min	-1.767	8	-.028	8	0	1	0	1	0	1	-.01	8
1275		3	max	.834	3	.012	3	0	12	0	12	0	.006	9
1276		min	-1.767	8	-.028	8	0	1	0	1	0	1	0	3
1277		4	max	.835	3	.012	3	0	12	0	12	0	.018	12
1278		min	-1.766	8	-.027	8	0	1	0	1	0	1	-.006	3
1279		5	max	.835	3	.013	3	0	12	0	12	0	.031	12
1280		min	-1.766	8	-.027	8	0	1	0	1	0	1	-.012	3
1281	M130	1	max	1.88	8	0	2	0	12	0	12	0	0	3
1282		min	-.789	3	-.007	9	0	1	0	1	0	1	-.016	12
1283		2	max	1.88	8	0	2	0	12	0	12	0	.002	3
1284		min	-.788	3	-.007	9	0	1	0	1	0	1	-.013	12
1285		3	max	1.881	8	-.001	2	0	12	0	12	0	.003	3



Envelope Member Section Forces (Continued)

Member	Sec		Axial[k]	LC	v Shear[k]	LC	z Shear[k]	LC	Torque[k-...	LC	y-y Mome...	LC	z-z Mome...	LC
1287	4	max	1.881	8	-.002	2	0	12	0	12	0	12	.005	3
1289	5	max	1.881	8	-.002	2	0	12	0	12	0	12	.007	3
1291	M131	1	max	.833	3	.011	3	0	12	0	12	0	.01	3
1293		2	max	.834	3	.011	3	0	12	0	12	0	.005	3
1295		3	max	.834	3	.012	3	0	12	0	12	0	0	2
1297		4	max	.835	3	.012	3	0	12	0	12	0	0	12
1299		5	max	.835	3	.013	3	0	12	0	12	0	0	12
1301	M132	1	max	.264	12	.011	8	0	12	0	12	0	.011	5
1303		2	max	.264	12	.01	8	0	12	0	12	0	.006	5
1305		3	max	.264	12	.01	8	0	12	0	12	0	.003	3
1307		4	max	.265	12	.01	8	0	12	0	12	0	.005	3
1309		5	max	.265	12	.009	8	0	12	0	12	0	.007	3

Envelope Member Section Deflections Service

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y' Ratio	LC	(n) L/z' Ratio	LC	
1	M43	1	max	.728	8	.186	3	0	12	0	12	NC	12	NC	12
2			min	-.291	3	-.133	12	0	1	0	1	NC	1	NC	1
3		2	max	.73	8	.228	3	0	12	0	12	NC	12	NC	12
4			min	-.292	3	-.17	12	0	1	0	1	NC	1	NC	1
5		3	max	.731	8	.269	3	0	12	0	12	NC	12	NC	12
6			min	-.292	3	-.21	8	0	1	0	1	NC	1	NC	1
7		4	max	.733	8	.311	3	0	12	0	12	NC	12	NC	12
8			min	-.293	3	-.267	8	0	1	0	1	NC	1	NC	1
9		5	max	.734	8	.352	3	0	12	0	12	NC	12	NC	12
10			min	-.294	3	-.324	8	0	1	0	1	NC	1	NC	1
11	M44	1	max	.708	8	.372	3	0	12	0	12	NC	12	NC	12
12			min	-.267	3	-.377	8	0	1	0	1	NC	1	NC	1
13		2	max	.708	8	.414	3	0	12	0	12	NC	12	NC	12
14			min	-.267	3	-.435	8	0	1	0	1	NC	1	NC	1
15		3	max	.708	8	.456	3	0	12	0	12	NC	12	NC	12
16			min	-.267	3	-.493	8	0	1	0	1	NC	1	NC	1
17		4	max	.708	8	.497	3	0	12	0	12	NC	12	NC	12
18			min	-.267	3	-.55	8	0	1	0	1	NC	1	NC	1
19		5	max	.708	8	.536	3	0	12	0	12	NC	12	NC	12
20			min	-.266	3	-.605	8	0	1	0	1	NC	1	NC	1
21	M45	1	max	.662	8	.554	3	0	12	0	12	NC	12	NC	12
22			min	-.226	3	-.655	8	0	1	0	1	NC	1	NC	1
23		2	max	.661	8	.592	3	0	12	0	12	NC	12	NC	12
24			min	-.225	3	-.708	8	0	1	0	1	NC	1	NC	1
25		3	max	.66	8	.628	3	0	12	0	12	NC	12	NC	12
26			min	-.224	3	-.759	8	0	1	0	1	7890.906	8	NC	1
27		4	max	.659	8	.663	3	0	12	0	12	NC	12	NC	12



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...]	LC	(n) L/y' Ratio	LC	(n) L/z' Ratio	LC
28		min	-.223	3	-.807	8	0	1	0	1	9918.555	8	NC	1
29	5	max	.658	8	.695	3	0	12	0	12	NC	12	NC	12
30		min	-.222	3	-.853	8	0	1	0	1	NC	1	NC	1
31	M46	1	max	.594	.709	3	0	12	0	12	NC	12	NC	12
32		min	-.171	3	-.899	8	0	1	0	1	NC	1	NC	1
33	2	max	.592	8	.74	3	0	12	0	12	NC	12	NC	12
34		min	-.169	3	-.942	8	0	1	0	1	7605.545	8	NC	1
35	3	max	.59	8	.768	3	0	12	0	12	NC	11	NC	12
36		min	-.167	3	-.982	8	0	1	0	1	5386.808	8	NC	1
37	4	max	.588	8	.794	3	0	12	0	12	NC	12	NC	12
38		min	-.166	3	-1.019	8	0	1	0	1	6762.894	8	NC	1
39	5	max	.586	8	.817	3	0	12	0	12	NC	12	NC	12
40		min	-.164	3	-1.051	8	0	1	0	1	NC	1	NC	1
41	M47	1	max	.508	.827	3	0	12	0	12	NC	12	NC	12
42		min	-.104	3	-1.091	8	0	1	0	1	NC	1	NC	1
43	2	max	.505	8	.847	3	0	12	0	12	NC	11	NC	12
44		min	-.102	3	-1.12	8	0	1	0	1	6411.823	8	NC	1
45	3	max	.503	8	.864	3	0	12	0	12	NC	11	NC	12
46		min	-.1	3	-1.145	8	0	1	0	1	4547.372	8	NC	1
47	4	max	.5	8	.878	3	0	12	0	12	NC	11	NC	12
48		min	-.098	3	-1.166	8	0	1	0	1	5721.563	8	NC	1
49	5	max	.498	8	.889	3	0	12	0	12	NC	12	NC	12
50		min	-.095	3	-1.182	8	0	1	0	1	NC	1	NC	1
51	M48	1	max	.422	.894	3	0	12	0	12	NC	12	NC	12
52		min	-.039	3	-1.212	8	0	1	0	1	NC	1	NC	1
53	2	max	.419	8	.9	3	0	12	0	12	NC	12	NC	12
54		min	-.037	3	-1.221	8	0	1	0	1	7510.741	8	NC	1
55	3	max	.417	8	.904	3	0	12	0	12	NC	11	NC	12
56		min	-.035	3	-1.227	8	0	1	0	1	5941.491	8	NC	1
57	4	max	.415	8	.906	3	0	12	0	12	NC	12	NC	12
58		min	-.033	3	-1.23	8	0	1	0	1	8354.037	8	NC	1
59	5	max	.413	8	.907	3	0	12	0	12	NC	12	NC	12
60		min	-.031	3	-1.232	8	0	1	0	1	NC	1	NC	1
61	M49	1	max	.348	.907	3	0	12	0	12	NC	12	NC	12
62		min	.004	1	-1.253	8	0	1	0	1	NC	1	NC	1
63	2	max	.346	5	.906	3	0	12	0	12	NC	12	NC	12
64		min	.005	1	-1.253	8	0	1	0	1	8472.045	8	NC	1
65	3	max	.344	5	.904	3	0	12	0	12	NC	11	NC	12
66		min	.005	1	-1.251	8	0	1	0	1	5983.567	8	NC	1
67	4	max	.342	5	.899	3	0	12	0	12	NC	12	NC	12
68		min	.006	1	-1.247	8	0	1	0	1	7518.102	8	NC	1
69	5	max	.34	5	.893	3	0	12	0	12	NC	12	NC	12
70		min	.006	1	-1.24	8	0	1	0	1	NC	1	NC	1
71	M50	1	max	.259	.889	3	0	12	0	12	NC	12	NC	12
72		min	.022	1	-1.26	8	0	1	0	1	NC	1	NC	1
73	2	max	.257	5	.878	3	0	12	0	12	NC	11	NC	12
74		min	.023	1	-1.246	8	0	1	0	1	5618.088	8	NC	1
75	3	max	.255	6	.863	3	0	12	0	12	NC	11	NC	12
76		min	.023	1	-1.227	8	0	1	0	1	4503.024	8	NC	1
77	4	max	.254	6	.845	3	0	12	0	12	NC	12	NC	12
78		min	.024	1	-1.204	8	0	1	0	1	6409.314	8	NC	1
79	5	max	.254	6	.825	3	0	12	0	12	NC	12	NC	12
80		min	.024	1	-1.177	8	0	1	0	1	NC	1	NC	1
81	M51	1	max	.233	.817	3	0	12	0	12	NC	12	NC	12
82		min	-.006	12	-1.189	8	0	1	0	1	NC	1	NC	1
83	2	max	.233	6	.794	3	0	12	0	12	NC	12	NC	12
84		min	-.007	12	-1.159	8	0	1	0	1	6731.12	8	NC	1



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...]	LC	(n) L/y' Ratio	LC	(n) L/z' Ratio	LC
85	3	max	.232	6	.769	3	0	12	0	12	NC	11	NC	12
86		min	-.008	12	-1.124	8	0	1	0	1	5298.205	8	NC	1
87	4	max	.232	6	.74	3	0	12	0	12	NC	12	NC	12
88		min	-.009	12	-1.087	8	0	1	0	1	7383.388	8	NC	1
89	5	max	.232	6	.71	3	0	12	0	12	NC	12	NC	12
90		min	-.011	12	-1.046	8	0	1	0	1	NC	1	NC	1
91	M52	1	max	.208	.695	3	0	12	0	12	NC	12	NC	12
92		min	-.058	12	-1.055	8	0	1	0	1	NC	1	NC	1
93	2	max	.209	3	.663	3	0	12	0	12	NC	12	NC	12
94		min	-.058	12	-1.011	8	0	1	0	1	9423.611	8	NC	1
95	3	max	.21	3	.628	3	0	12	0	12	NC	12	NC	12
96		min	-.059	12	-.964	8	0	1	0	1	7513.408	8	NC	1
97	4	max	.212	3	.592	3	0	12	0	12	NC	12	NC	12
98		min	-.06	12	-.915	8	0	1	0	1	NC	1	NC	1
99	5	max	.213	3	.553	3	0	12	0	12	NC	12	NC	12
100		min	-.061	12	-.863	8	0	1	0	1	NC	1	NC	1
101	M53	1	max	.252	.536	3	0	12	0	12	NC	12	NC	12
102		min	-.095	12	-.866	8	0	1	0	1	NC	1	NC	1
103	2	max	.253	3	.497	3	0	12	0	12	NC	12	NC	12
104		min	-.094	12	-.812	8	0	1	0	1	NC	1	NC	1
105	3	max	.253	3	.457	3	0	12	0	12	NC	12	NC	12
106		min	-.094	12	-.757	8	0	1	0	1	NC	1	NC	1
107	4	max	.253	3	.415	3	0	12	0	12	NC	12	NC	12
108		min	-.094	12	-.701	8	0	1	0	1	NC	1	NC	1
109	5	max	.254	3	.374	3	0	12	0	12	NC	12	NC	12
110		min	-.094	12	-.644	8	0	1	0	1	NC	1	NC	1
111	M54	1	max	.28	.354	3	0	12	0	12	NC	12	NC	12
112		min	-.118	12	-.643	8	0	1	0	1	NC	1	NC	1
113	2	max	.279	3	.312	3	0	12	0	12	NC	12	NC	12
114		min	-.117	12	-.586	8	0	1	0	1	NC	1	NC	1
115	3	max	.279	3	.27	3	0	12	0	12	NC	12	NC	12
116		min	-.116	12	-.528	8	0	1	0	1	NC	1	NC	1
117	4	max	.278	3	.228	3	0	12	0	12	NC	12	NC	12
118		min	-.115	12	-.471	8	0	1	0	1	NC	1	NC	1
119	5	max	.277	3	.187	3	0	12	0	12	NC	12	NC	12
120		min	-.114	12	-.414	8	0	1	0	1	NC	1	NC	1
121	M104A	1	max	.285	.175	3	0	12	0	12	NC	12	NC	12
122		min	-.121	12	-.412	8	0	1	0	1	NC	1	NC	1
123	2	max	.283	3	.147	3	0	12	0	12	NC	12	NC	12
124		min	-.12	12	-.372	8	0	1	0	1	NC	1	NC	1
125	3	max	.282	3	.118	3	0	12	0	12	NC	12	NC	12
126		min	-.118	12	-.333	8	0	1	0	1	NC	1	NC	1
127	4	max	.28	3	.091	3	0	12	0	12	NC	12	NC	12
128		min	-.117	12	-.295	8	0	1	0	1	NC	1	NC	1
129	5	max	.278	3	.065	3	0	12	0	12	NC	12	NC	12
130		min	-.116	12	-.259	8	0	1	0	1	NC	1	NC	1
131	M110A	1	max	.722	.118	6	0	12	0	12	NC	12	NC	12
132		min	-.295	3	-.015	12	0	1	0	1	NC	1	NC	1
133	2	max	.725	8	.11	6	0	12	0	12	NC	12	NC	12
134		min	-.296	3	-.037	12	0	1	0	1	7610.803	8	NC	1
135	3	max	.727	8	.114	3	0	12	0	12	NC	12	NC	12
136		min	-.298	3	-.062	12	0	1	0	1	7499.362	8	NC	1
137	4	max	.73	8	.142	3	0	12	0	12	NC	12	NC	12
138		min	-.3	3	-.087	12	0	1	0	1	NC	1	NC	1
139	5	max	.733	8	.17	3	0	12	0	12	NC	12	NC	12
140		min	-.301	3	-.113	12	0	1	0	1	NC	1	NC	1
141	M34	1	max	-.004	.488	8	0	12	0	12	NC	12	NC	12



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...]	LC (n)	L/y' Ratio	LC (n)	L/z' Ratio	LC	
142		min	-.012	6	-.215	3	0	1	0	1	NC	1	NC	1	
143	2	max	0	12	.534	8	0	12	0	12	NC	11	NC	12	
144		min	-.01	6	-.235	3	0	1	0	1	7348.196	8	NC	1	
145	3	max	.002	12	.578	8	0	12	0	12	NC	10	NC	12	
146		min	-.011	3	-.253	3	0	1	0	1	5177.021	8	NC	1	
147	4	max	.005	12	.618	8	0	12	0	12	NC	11	NC	12	
148		min	-.013	3	-.271	3	0	1	0	1	6508.123	8	NC	1	
149	5	max	.007	12	.655	8	0	12	0	12	NC	12	NC	12	
150		min	-.015	3	-.286	3	0	1	0	1	NC	1	NC	1	
151	M63	1	max	.016	3	.127	12	0	12	0	12	NC	12	NC	12
152		min	-.029	8	-.282	3	0	1	0	1	NC	1	NC	1	
153	2	max	.014	3	.12	12	0	12	0	12	NC	12	NC	12	
154		min	-.027	8	-.267	3	0	1	0	1	NC	1	NC	1	
155	3	max	.012	3	.112	12	0	12	0	12	NC	12	NC	12	
156		min	-.025	8	-.25	3	0	1	0	1	9594.515	3	NC	1	
157	4	max	.009	3	.103	12	0	12	0	12	NC	12	NC	12	
158		min	-.024	8	-.231	3	0	1	0	1	NC	1	NC	1	
159	5	max	.007	3	.094	12	0	12	0	12	NC	12	NC	12	
160		min	-.022	8	-.211	3	0	1	0	1	NC	1	NC	1	
161	M64	1	max	.007	3	.094	12	0	12	0	12	NC	12	NC	12
162		min	-.022	8	-.211	3	0	1	0	1	NC	1	NC	1	
163	2	max	.006	3	.082	12	0	12	0	12	NC	12	NC	12	
164		min	-.021	8	-.186	3	0	1	0	1	NC	1	NC	1	
165	3	max	.004	3	.07	12	0	12	0	12	NC	12	NC	12	
166		min	-.02	8	-.159	3	0	1	0	1	NC	1	NC	1	
167	4	max	.003	4	.057	12	0	12	0	12	NC	12	NC	12	
168		min	-.018	8	-.131	3	0	1	0	1	NC	1	NC	1	
169	5	max	.002	2	.044	12	0	12	0	12	NC	12	NC	12	
170		min	-.017	8	-.102	3	0	1	0	1	NC	1	NC	1	
171	M121A	1	max	.507	8	.597	8	0	12	0	12	NC	12	NC	12
172		min	-.227	3	-.231	3	0	1	0	1	NC	1	NC	1	
173	2	max	.51	8	.593	8	0	12	0	12	NC	12	NC	12	
174		min	-.228	3	-.226	3	0	1	0	1	7483.714	8	NC	1	
175	3	max	.513	8	.588	8	0	12	0	12	NC	12	NC	12	
176		min	-.23	3	-.22	3	0	1	0	1	5536.282	8	NC	1	
177	4	max	.516	8	.581	8	0	12	0	12	NC	12	NC	12	
178		min	-.232	3	-.213	3	0	1	0	1	7285.18	8	NC	1	
179	5	max	.518	8	.572	8	0	12	0	12	NC	12	NC	12	
180		min	-.234	3	-.205	3	0	1	0	1	NC	1	NC	1	
181	M119A	1	max	.708	8	.227	8	0	12	0	12	NC	12	NC	12
182		min	-.291	3	-.03	3	0	1	0	1	NC	1	NC	1	
183	2	max	.711	8	.204	5	0	12	0	12	NC	12	NC	12	
184		min	-.293	3	-.012	3	0	1	0	1	7364.866	8	NC	1	
185	3	max	.713	8	.181	5	0	12	0	12	NC	12	NC	12	
186		min	-.294	3	.004	1	0	1	0	1	6141.015	8	NC	1	
187	4	max	.715	8	.156	5	0	12	0	12	NC	12	NC	12	
188		min	-.296	3	.009	1	0	1	0	1	9233.951	8	NC	1	
189	5	max	.718	8	.132	6	0	12	0	12	NC	12	NC	12	
190		min	-.297	3	0	12	0	1	0	1	NC	1	NC	1	
191	M117	1	max	.143	8	.741	8	0	12	0	12	NC	12	NC	12
192		min	-.076	3	-.315	3	0	1	0	1	NC	1	NC	1	
193	2	max	.147	8	.75	8	0	12	0	12	NC	12	NC	12	
194		min	-.078	3	-.318	3	0	1	0	1	6799.397	8	NC	1	
195	3	max	.15	8	.759	8	0	12	0	12	NC	11	NC	12	
196		min	-.08	3	-.32	3	0	1	0	1	4560.009	8	NC	1	
197	4	max	.153	8	.765	8	0	12	0	12	NC	11	NC	12	
198		min	-.082	3	-.321	3	0	1	0	1	5498.849	8	NC	1	



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y' Ratio	LC	(n) L/z' Ratio	LC	
199	5	max	.157	8	.769	8	0	12	0	12	NC	12	NC	12	
200		min	-.084	3	-.32	3	0	1	0	1	NC	1	NC	1	
201	M105A	1	max	.249	3	.026	12	0	12	0	12	NC	12	NC	12
202		min	-.116	12	-.176	6	0	1	0	1	NC	1	NC	1	
203		2	max	.247	3	.035	12	0	12	0	12	NC	12	NC	12
204		min	-.114	12	-.171	6	0	1	0	1	NC	1	NC	1	
205		3	max	.246	3	.043	12	0	12	0	12	NC	12	NC	12
206		min	-.113	12	-.167	6	0	1	0	1	8014.667	8	NC	1	
207		4	max	.244	3	.05	12	0	12	0	12	NC	12	NC	12
208		min	-.112	12	-.162	6	0	1	0	1	NC	1	NC	1	
209		5	max	.243	3	.056	12	0	12	0	12	NC	12	NC	12
210		min	-.111	12	-.17	3	0	1	0	1	NC	1	NC	1	
211	M106A	1	max	.165	3	.108	12	0	12	0	12	NC	12	NC	12
212		min	-.087	8	-.264	3	0	1	0	1	NC	1	NC	1	
213		2	max	.164	3	.112	12	0	12	0	12	NC	12	NC	12
214		min	-.085	8	-.269	3	0	1	0	1	NC	1	NC	1	
215		3	max	.162	3	.116	12	0	12	0	12	NC	12	NC	12
216		min	-.083	8	-.274	3	0	1	0	1	8385.85	8	NC	1	
217		4	max	.16	3	.119	12	0	12	0	12	NC	12	NC	12
218		min	-.081	8	-.278	3	0	1	0	1	9618.709	8	NC	1	
219		5	max	.158	3	.122	12	0	12	0	12	NC	12	NC	12
220		min	-.079	8	-.28	3	0	1	0	1	NC	1	NC	1	
221	M107A	1	max	.026	3	.141	12	0	12	0	12	NC	12	NC	12
222		min	-.038	8	-.315	3	0	1	0	1	NC	1	NC	1	
223		2	max	.024	3	.139	12	0	12	0	12	NC	12	NC	12
224		min	-.036	8	-.31	3	0	1	0	1	9572.738	3	NC	1	
225		3	max	.021	3	.136	12	0	12	0	12	NC	12	NC	12
226		min	-.034	8	-.302	3	0	1	0	1	7463.61	3	NC	1	
227		4	max	.018	3	.132	12	0	12	0	12	NC	12	NC	12
228		min	-.031	8	-.293	3	0	1	0	1	NC	1	NC	1	
229		5	max	.016	3	.127	12	0	12	0	12	NC	12	NC	12
230		min	-.029	8	-.282	3	0	1	0	1	NC	1	NC	1	
231	M111A	1	max	.283	3	.039	3	0	12	0	12	NC	12	NC	12
232		min	-.123	12	-.254	8	0	1	0	1	NC	1	NC	1	
233		2	max	.282	3	.016	3	0	12	0	12	NC	12	NC	12
234		min	-.122	12	-.221	8	0	1	0	1	NC	1	NC	1	
235		3	max	.28	3	0	2	0	12	0	12	NC	11	NC	12
236		min	-.121	12	-.19	5	0	1	0	1	6851.311	8	NC	1	
237		4	max	.279	3	-.005	2	0	12	0	12	NC	12	NC	12
238		min	-.119	12	-.162	5	0	1	0	1	8059.22	8	NC	1	
239		5	max	.277	3	-.01	2	0	12	0	12	NC	12	NC	12
240		min	-.118	12	-.137	5	0	1	0	1	NC	1	NC	1	
241	M115C	1	max	.603	8	.482	8	0	12	0	12	NC	12	NC	12
242		min	-.263	3	-.165	3	0	1	0	1	NC	1	NC	1	
243		2	max	.606	8	.469	8	0	12	0	12	NC	12	NC	12
244		min	-.265	3	-.153	3	0	1	0	1	6206.455	8	NC	1	
245		3	max	.61	8	.453	8	0	12	0	12	NC	11	NC	12
246		min	-.267	3	-.14	3	0	1	0	1	5203.116	8	NC	1	
247		4	max	.613	8	.435	8	0	12	0	12	NC	12	NC	12
248		min	-.269	3	-.126	3	0	1	0	1	7870.76	8	NC	1	
249		5	max	.617	8	.416	8	0	12	0	12	NC	12	NC	12
250		min	-.271	3	-.11	3	0	1	0	1	NC	1	NC	1	
251	M116A	1	max	.214	3	.072	12	0	12	0	12	NC	12	NC	12
252		min	-.101	12	-.205	3	0	1	0	1	NC	1	NC	1	
253		2	max	.213	3	.078	12	0	12	0	12	NC	12	NC	12
254		min	-.1	12	-.213	3	0	1	0	1	NC	1	NC	1	
255		3	max	.211	3	.084	12	0	12	0	12	NC	12	NC	12



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC (n)	L/y' Ratio	LC (n)	L/z' Ratio	LC	
256		min	-.099	12	-.22	3	0	1	0	1	NC	1	NC	1	
257	4	max	.209	3	.089	12	0	12	0	12	NC	12	NC	12	
258		min	-.098	12	-.226	3	0	1	0	1	NC	1	NC	1	
259	5	max	.208	3	.093	12	0	12	0	12	NC	12	NC	12	
260		min	-.096	12	-.232	3	0	1	0	1	NC	1	NC	1	
261	M117A	1	max	.098	3	.134	12	0	12	0	12	NC	12	NC	12
262		min	-.065	8	-.306	3	0	1	0	1	NC	1	NC	1	
263	2	max	.096	3	.135	12	0	12	0	12	NC	12	NC	12	
264		min	-.063	8	-.307	3	0	1	0	1	9810.691	8	NC	1	
265	3	max	.095	3	.135	12	0	12	0	12	NC	12	NC	12	
266		min	-.062	8	-.306	3	0	1	0	1	8814.566	3	NC	1	
267	4	max	.093	3	.135	12	0	12	0	12	NC	12	NC	12	
268		min	-.06	8	-.304	3	0	1	0	1	NC	1	NC	1	
269	5	max	.091	3	.135	12	0	12	0	12	NC	12	NC	12	
270		min	-.058	8	-.302	3	0	1	0	1	NC	1	NC	1	
271	M122A	1	max	0	.018	8	0	12	0	12	NC	12	NC	12	
272		min	-.022	5	-.007	3	0	1	0	1	NC	1	NC	1	
273	2	max	0	3	.071	8	0	12	0	12	NC	12	NC	12	
274		min	-.022	5	-.03	3	0	1	0	1	NC	1	NC	1	
275	3	max	0	3	.126	8	0	12	0	12	NC	12	NC	12	
276		min	-.022	5	-.055	3	0	1	0	1	NC	1	NC	1	
277	4	max	0	3	.182	8	0	12	0	12	NC	12	NC	12	
278		min	-.021	5	-.079	3	0	1	0	1	NC	1	NC	1	
279	5	max	0	3	.238	8	0	12	0	12	NC	12	NC	12	
280		min	-.021	5	-.104	3	0	1	0	1	NC	1	NC	1	
281	M125D	1	max	0	.238	8	0	12	0	12	NC	12	NC	12	
282		min	-.021	5	-.104	3	0	1	0	1	NC	1	NC	1	
283	2	max	-.002	3	.303	8	0	12	0	12	NC	12	NC	12	
284		min	-.018	5	-.133	3	0	1	0	1	NC	1	NC	1	
285	3	max	-.003	2	.368	8	0	12	0	12	NC	11	NC	12	
286		min	-.016	5	-.162	3	0	1	0	1	8134.577	8	NC	1	
287	4	max	-.003	2	.43	8	0	12	0	12	NC	11	NC	12	
288		min	-.013	5	-.189	3	0	1	0	1	8796.009	8	NC	1	
289	5	max	-.004	12	.488	8	0	12	0	12	NC	12	NC	12	
290		min	-.012	6	-.215	3	0	1	0	1	NC	1	NC	1	
291	M127A	1	max	.002	.044	12	0	12	0	12	NC	12	NC	12	
292		min	-.017	8	-.102	3	0	1	0	1	NC	1	NC	1	
293	2	max	.002	2	.034	12	0	12	0	12	NC	12	NC	12	
294		min	-.017	8	-.078	3	0	1	0	1	NC	1	NC	1	
295	3	max	.002	2	.023	12	0	12	0	12	NC	12	NC	12	
296		min	-.016	8	-.054	3	0	1	0	1	NC	1	NC	1	
297	4	max	.002	2	.012	12	0	12	0	12	NC	12	NC	12	
298		min	-.016	8	-.03	3	0	1	0	1	NC	1	NC	1	
299	5	max	.002	2	.002	12	0	12	0	12	NC	12	NC	12	
300		min	-.015	8	-.007	3	0	1	0	1	NC	1	NC	1	
301	M133A	1	max	.007	.655	8	0	12	0	12	NC	12	NC	12	
302		min	-.015	3	-.286	3	0	1	0	1	NC	1	NC	1	
303	2	max	.011	8	.685	8	0	12	0	12	NC	11	NC	12	
304		min	-.018	3	-.298	3	0	1	0	1	5368.515	8	NC	1	
305	3	max	.016	8	.712	8	0	12	0	12	NC	10	NC	12	
306		min	-.02	3	-.309	3	0	1	0	1	3856.795	8	NC	1	
307	4	max	.021	8	.735	8	0	12	0	12	NC	11	NC	12	
308		min	-.023	3	-.317	3	0	1	0	1	4934.552	8	NC	1	
309	5	max	.025	8	.754	8	0	12	0	12	NC	12	NC	12	
310		min	-.026	3	-.323	3	0	1	0	1	NC	1	NC	1	
311	M137	1	max	.3	.725	8	0	12	0	12	NC	12	NC	12	
312		min	-.143	3	-.298	3	0	1	0	1	NC	1	NC	1	



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...]	LC	(n) L/y' Ratio	LC	(n) L/z' Ratio	LC	
313	2	max	.302	8	.725	8	0	12	0	12	NC	12	NC	12	
314		min	-.145	3	-.296	3	0	1	0	1	8063.768	8	NC	1	
315	3	max	.304	8	.724	8	0	12	0	12	NC	12	NC	12	
316		min	-.146	3	-.294	3	0	1	0	1	6794.778	8	NC	1	
317	4	max	.307	8	.723	8	0	12	0	12	NC	12	NC	12	
318		min	-.147	3	-.291	3	0	1	0	1	NC	1	NC	1	
319	5	max	.309	8	.72	8	0	12	0	12	NC	12	NC	12	
320		min	-.149	3	-.288	3	0	1	0	1	NC	1	NC	1	
321	M124A	1	max	.007	3	0	3	0	12	0	12	NC	12	NC	12
322		min	-.018	8	-.022	5	0	1	0	1	NC	1	NC	1	
323	2	max	.007	3	.003	8	0	12	0	12	NC	12	NC	12	
324		min	-.018	8	-.01	3	0	1	0	1	NC	1	NC	1	
325	3	max	.007	3	.028	8	0	12	0	12	NC	12	NC	12	
326		min	-.018	8	-.021	3	0	1	0	1	NC	1	NC	1	
327	4	max	.007	3	.053	8	0	12	0	12	NC	12	NC	12	
328		min	-.018	8	-.032	3	0	1	0	1	NC	1	NC	1	
329	5	max	.007	3	.078	8	0	12	0	12	NC	12	NC	12	
330		min	-.018	8	-.043	3	0	1	0	1	NC	1	NC	1	
331	M125	1	max	.007	3	.015	8	0	12	0	12	NC	12	NC	12
332		min	-.002	12	-.002	1	0	1	0	1	NC	1	NC	1	
333	2	max	.007	3	.019	8	0	12	0	12	NC	12	NC	12	
334		min	-.002	12	-.01	3	0	1	0	1	NC	1	NC	1	
335	3	max	.007	3	.023	8	0	12	0	12	NC	12	NC	12	
336		min	-.002	12	-.021	3	0	1	0	1	NC	1	NC	1	
337	4	max	.007	3	.026	8	0	12	0	12	NC	12	NC	12	
338		min	-.002	12	-.031	3	0	1	0	1	NC	1	NC	1	
339	5	max	.007	3	.03	8	0	12	0	12	NC	12	NC	12	
340		min	-.002	12	-.042	3	0	1	0	1	NC	1	NC	1	
341	M2	1	max	.03	8	.002	12	0	12	0	12	NC	12	NC	12
342		min	-.042	3	-.007	3	0	1	0	1	NC	1	NC	1	
343	2	max	.031	8	.007	12	0	12	0	12	NC	12	NC	12	
344		min	-.043	3	-.019	3	0	1	0	1	NC	1	NC	1	
345	3	max	.031	8	.013	12	0	12	0	12	NC	12	NC	12	
346		min	-.043	3	-.031	3	0	1	0	1	NC	1	NC	1	
347	4	max	.031	8	.018	12	0	12	0	12	NC	12	NC	12	
348		min	-.044	3	-.043	3	0	1	0	1	NC	1	NC	1	
349	5	max	.032	8	.023	12	0	12	0	12	NC	12	NC	12	
350		min	-.044	3	-.056	3	0	1	0	1	NC	1	NC	1	
351	M3	1	max	.034	8	.074	12	0	12	0	12	NC	12	NC	12
352		min	-.046	3	-.168	3	0	1	0	1	NC	1	NC	1	
353	2	max	.034	8	.083	12	0	12	0	12	NC	12	NC	12	
354		min	-.045	3	-.188	3	0	1	0	1	NC	1	NC	1	
355	3	max	.034	8	.092	12	0	12	0	12	NC	12	NC	12	
356		min	-.045	3	-.208	3	0	1	0	1	NC	1	NC	1	
357	4	max	.034	8	.101	12	0	12	0	12	NC	12	NC	12	
358		min	-.044	3	-.226	3	0	1	0	1	NC	1	NC	1	
359	5	max	.034	8	.109	12	0	12	0	12	NC	12	NC	12	
360		min	-.043	3	-.243	3	0	1	0	1	NC	1	NC	1	
361	M4	1	max	.034	8	.109	12	0	12	0	12	NC	12	NC	12
362		min	-.043	3	-.243	3	0	1	0	1	NC	1	NC	1	
363	2	max	.033	8	.116	12	0	12	0	12	NC	12	NC	12	
364		min	-.042	3	-.26	3	0	1	0	1	NC	1	NC	1	
365	3	max	.032	8	.123	12	0	12	0	12	NC	12	NC	12	
366		min	-.04	3	-.276	3	0	1	0	1	7773.621	3	NC	1	
367	4	max	.031	8	.129	12	0	12	0	12	NC	12	NC	12	
368		min	-.039	3	-.289	3	0	1	0	1	9457.515	3	NC	1	
369	5	max	.03	8	.135	12	0	12	0	12	NC	12	NC	12	



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...]	LC (n)	L/y' Ratio	LC (n)	L/z' Ratio	LC
370		min	-.037	3	-.3	3	0	1	0	1	NC	1	NC	1
371	M5	max	.03	8	.135	12	0	12	0	12	NC	12	NC	12
372		min	-.037	3	-.3	3	0	1	0	1	NC	1	NC	1
373		max	.029	8	.137	12	0	12	0	12	NC	12	NC	12
374		min	-.036	3	-.304	3	0	1	0	1	NC	1	NC	1
375		max	.028	8	.139	12	0	12	0	12	NC	12	NC	12
376		min	-.035	3	-.308	3	0	1	0	1	NC	1	NC	1
377		max	.027	8	.139	12	0	12	0	12	NC	12	NC	12
378		min	-.034	3	-.311	3	0	1	0	1	NC	1	NC	1
379		max	.026	8	.14	12	0	12	0	12	NC	12	NC	12
380		min	-.033	3	-.314	3	0	1	0	1	NC	1	NC	1
381	M6	max	.045	8	.134	12	0	12	0	12	NC	12	NC	12
382		min	-.095	3	-.301	3	0	1	0	1	NC	1	NC	1
383		max	.043	8	.134	12	0	12	0	12	NC	12	NC	12
384		min	-.093	3	-.303	3	0	1	0	1	NC	1	NC	1
385		max	.042	8	.134	12	0	12	0	12	NC	12	NC	12
386		min	-.092	3	-.305	3	0	1	0	1	8474.236	3	NC	1
387		max	.041	8	.134	12	0	12	0	12	NC	12	NC	12
388		min	-.09	3	-.306	3	0	1	0	1	9916.61	3	NC	1
389		max	.04	8	.132	12	0	12	0	12	NC	12	NC	12
390		min	-.088	3	-.304	3	0	1	0	1	NC	1	NC	1
391	M7	max	.065	12	.121	12	0	12	0	12	NC	12	NC	12
392		min	-.149	3	-.28	3	0	1	0	1	NC	1	NC	1
393		max	.064	12	.119	12	0	12	0	12	NC	12	NC	12
394		min	-.147	3	-.277	3	0	1	0	1	NC	1	NC	1
395		max	.063	12	.116	12	0	12	0	12	NC	12	NC	12
396		min	-.146	3	-.274	3	0	1	0	1	NC	1	NC	1
397		max	.063	12	.112	12	0	12	0	12	NC	12	NC	12
398		min	-.145	3	-.269	3	0	1	0	1	NC	1	NC	1
399		max	.062	12	.108	12	0	12	0	12	NC	12	NC	12
400		min	-.144	3	-.264	3	0	1	0	1	NC	1	NC	1
401	M8	max	.077	12	.098	12	0	12	0	12	NC	12	NC	12
402		min	-.18	3	-.241	3	0	1	0	1	NC	1	NC	1
403		max	.076	12	.092	12	0	12	0	12	NC	12	NC	12
404		min	-.179	3	-.233	3	0	1	0	1	NC	1	NC	1
405		max	.074	12	.086	12	0	12	0	12	NC	12	NC	12
406		min	-.177	3	-.225	3	0	1	0	1	NC	1	NC	1
407		max	.073	12	.079	12	0	12	0	12	NC	12	NC	12
408		min	-.175	3	-.217	3	0	1	0	1	NC	1	NC	1
409		max	.072	12	.071	12	0	12	0	12	NC	12	NC	12
410		min	-.174	3	-.207	3	0	1	0	1	NC	1	NC	1
411	M9	max	.091	12	.046	12	0	12	0	12	NC	12	NC	12
412		min	-.229	3	-.144	3	0	1	0	1	NC	1	NC	1
413		max	.089	12	.036	12	0	12	0	12	NC	12	NC	12
414		min	-.227	3	-.147	6	0	1	0	1	NC	1	NC	1
415		max	.088	12	.026	12	0	12	0	12	NC	12	NC	12
416		min	-.226	3	-.154	6	0	1	0	1	NC	1	NC	1
417		max	.087	12	.015	12	0	12	0	12	NC	12	NC	12
418		min	-.224	3	-.161	6	0	1	0	1	NC	1	NC	1
419		max	.086	12	.003	12	0	12	0	12	NC	12	NC	12
420		min	-.223	3	-.167	6	0	1	0	1	NC	1	NC	1
421	M12	max	.049	12	.276	3	0	12	0	12	NC	12	NC	12
422		min	-.201	6	-.523	8	0	1	0	1	NC	1	NC	1
423		max	.049	12	.322	3	0	12	0	12	NC	12	NC	12
424		min	-.201	6	-.585	8	0	1	0	1	NC	1	NC	1
425		max	.049	12	.367	3	0	12	0	12	NC	12	NC	12
426		min	-.2	6	-.646	8	0	1	0	1	7681.776	8	NC	1



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y' Ratio	LC	(n) L/z' Ratio	LC	
427	4	max	.05	12	.409	3	0	12	0	12	NC	12	NC	12	
428		min	-.2	3	-.703	8	0	1	0	1	NC	1	NC	1	
429	5	max	.05	12	.449	3	0	12	0	12	NC	12	NC	12	
430		min	-.2	3	-.76	8	0	1	0	1	NC	1	NC	1	
431	M13	1	max	.021	12	.463	3	0	12	0	12	NC	12	NC	12
432		min	-.219	6	-.752	8	0	1	0	1	NC	1	NC	1	
433		2	max	.022	12	.507	3	0	12	0	12	NC	11	NC	12
434		min	-.218	6	-.816	8	0	1	0	1	3892.019	8	NC	1	
435		3	max	.023	12	.551	3	0	12	0	12	NC	10	NC	12
436		min	-.217	6	-.876	8	0	1	0	1	2368.563	8	NC	1	
437		4	max	.024	12	.588	3	0	12	0	12	NC	10	NC	12
438		min	-.216	6	-.925	8	0	1	0	1	3511.675	8	NC	1	
439		5	max	.025	12	.621	3	0	12	0	12	NC	12	NC	12
440		min	-.215	6	-.968	8	0	1	0	1	NC	1	NC	1	
441	M18	1	max	.103	3	.861	3	0	12	0	12	NC	12	NC	12
442		min	-.504	8	-1.127	8	0	1	0	1	NC	1	NC	1	
443		2	max	.101	3	.846	3	0	12	0	12	NC	10	NC	12
444		min	-.5	8	-1.106	8	0	1	0	1	3519.863	8	NC	1	
445		3	max	.098	3	.828	3	0	12	0	12	NC	10	NC	12
446		min	-.496	8	-1.082	8	0	1	0	1	2127.065	8	NC	1	
447		4	max	.095	3	.802	3	0	12	0	12	NC	10	NC	12
448		min	-.492	8	-1.044	8	0	1	0	1	3062.424	8	NC	1	
449		5	max	.093	3	.772	3	0	12	0	12	NC	12	NC	12
450		min	-.488	8	-.999	8	0	1	0	1	NC	1	NC	1	
451	M19	1	max	.137	3	.765	3	0	12	0	12	NC	12	NC	12
452		min	-.545	8	-.969	8	0	1	0	1	NC	1	NC	1	
453		2	max	.136	3	.75	3	0	12	0	12	NC	12	NC	12
454		min	-.543	8	-.949	8	0	1	0	1	NC	1	NC	1	
455		3	max	.135	3	.735	3	0	12	0	12	NC	12	NC	12
456		min	-.542	8	-.928	8	0	1	0	1	NC	1	NC	1	
457		4	max	.134	3	.719	3	0	12	0	12	NC	12	NC	12
458		min	-.54	8	-.906	8	0	1	0	1	NC	1	NC	1	
459		5	max	.133	3	.703	3	0	12	0	12	NC	12	NC	12
460		min	-.539	8	-.883	8	0	1	0	1	NC	1	NC	1	
461	M20	1	max	.186	3	.621	3	0	12	0	12	NC	12	NC	12
462		min	-.602	8	-.736	8	0	1	0	1	NC	1	NC	1	
463		2	max	.185	3	.588	3	0	12	0	12	NC	10	NC	12
464		min	-.6	8	-.691	8	0	1	0	1	3741.552	8	NC	1	
465		3	max	.184	3	.55	3	0	12	0	12	NC	10	NC	12
466		min	-.598	8	-.64	8	0	1	0	1	2562.926	8	NC	1	
467		4	max	.182	3	.507	3	0	12	0	12	NC	11	NC	12
468		min	-.596	8	-.578	8	0	1	0	1	4439.985	8	NC	1	
469		5	max	.181	3	.462	3	0	12	0	12	NC	12	NC	12
470		min	-.594	8	-.514	8	0	1	0	1	NC	1	NC	1	
471	M21	1	max	.214	3	.448	3	0	12	0	12	NC	12	NC	12
472		min	-.63	8	-.469	8	0	1	0	1	NC	1	NC	1	
473		2	max	.214	3	.407	3	0	12	0	12	NC	12	NC	12
474		min	-.629	8	-.415	8	0	1	0	1	7406.52	8	NC	1	
475		3	max	.213	3	.366	3	0	12	0	12	NC	11	NC	12
476		min	-.628	8	-.358	8	0	1	0	1	4670.54	8	NC	1	
477		4	max	.213	3	.321	3	0	12	0	12	NC	12	NC	12
478		min	-.627	8	-.294	8	0	1	0	1	NC	1	NC	1	
479		5	max	.212	3	.276	3	0	12	0	12	NC	12	NC	12
480		min	-.627	8	-.231	8	0	1	0	1	NC	1	NC	1	
481	M22	1	max	.234	3	.258	3	0	12	0	12	NC	12	NC	12
482		min	-.643	8	-.192	12	0	1	0	1	NC	1	NC	1	
483		2	max	.235	3	.212	3	0	12	0	12	NC	10	NC	12



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...]	LC	(n) L/y' Ratio	LC	(n) L/z' Ratio	LC	
484		min	-.645	8	-.155	12	0	1	0	1	3798.705	8	NC	1	
485	3	max	.236	3	.164	3	0	12	0	12	NC	8	NC	12	
486		min	-.646	8	-.114	12	0	1	0	1	2304.276	8	NC	1	
487	4	max	.237	3	.108	3	0	12	0	12	NC	10	NC	12	
488		min	-.647	8	-.061	12	0	1	0	1	4834.653	8	NC	1	
489	5	max	.238	3	.117	6	0	12	0	12	NC	12	NC	12	
490		min	-.649	8	-.009	12	0	1	0	1	NC	1	NC	1	
491	M23	1	max	.195	3	.581	8	0	12	0	12	NC	12	NC	12
492		min	-.466	8	-.206	3	0	1	0	1	NC	1	NC	1	
493	2	max	.197	3	.591	8	0	12	0	12	NC	12	NC	12	
494		min	-.469	8	-.216	3	0	1	0	1	8257.596	8	NC	1	
495	3	max	.199	3	.6	8	0	12	0	12	NC	12	NC	12	
496		min	-.472	8	-.225	3	0	1	0	1	7176.445	8	NC	1	
497	4	max	.201	3	.607	8	0	12	0	12	NC	12	NC	12	
498		min	-.475	8	-.233	3	0	1	0	1	9369.186	8	NC	1	
499	5	max	.203	3	.612	8	0	12	0	12	NC	12	NC	12	
500		min	-.478	8	-.239	3	0	1	0	1	NC	1	NC	1	
501	M24	1	max	.139	3	.709	8	0	12	0	12	NC	12	NC	12
502		min	-.317	8	-.281	3	0	1	0	1	NC	1	NC	1	
503	2	max	.14	3	.711	8	0	12	0	12	NC	12	NC	12	
504		min	-.319	8	-.285	3	0	1	0	1	NC	1	NC	1	
505	3	max	.142	3	.713	8	0	12	0	12	NC	12	NC	12	
506		min	-.322	8	-.289	3	0	1	0	1	8044.07	8	NC	1	
507	4	max	.143	3	.713	8	0	12	0	12	NC	12	NC	12	
508		min	-.324	8	-.292	3	0	1	0	1	9673.296	8	NC	1	
509	5	max	.145	3	.712	8	0	12	0	12	NC	12	NC	12	
510		min	-.326	8	-.294	3	0	1	0	1	NC	1	NC	1	
511	M25	1	max	.064	3	.772	8	0	12	0	12	NC	12	NC	12
512		min	-.133	8	-.321	3	0	1	0	1	NC	1	NC	1	
513	2	max	.066	3	.768	8	0	12	0	12	NC	12	NC	12	
514		min	-.135	8	-.322	3	0	1	0	1	5391.796	8	NC	1	
515	3	max	.067	3	.762	8	0	12	0	12	NC	12	NC	12	
516		min	-.138	8	-.321	3	0	1	0	1	4205.51	8	NC	1	
517	4	max	.069	3	.753	8	0	12	0	12	NC	12	NC	12	
518		min	-.141	8	-.319	3	0	1	0	1	6168.519	8	NC	1	
519	5	max	.07	3	.742	8	0	12	0	12	NC	12	NC	12	
520		min	-.143	8	-.317	3	0	1	0	1	NC	1	NC	1	
521	M26	1	max	.034	3	.753	8	0	12	0	12	NC	12	NC	12
522		min	-.058	8	-.322	3	0	1	0	1	NC	1	NC	1	
523	2	max	.035	3	.744	8	0	12	0	12	NC	12	NC	12	
524		min	-.06	8	-.32	3	0	1	0	1	9797.578	8	NC	1	
525	3	max	.036	3	.733	8	0	12	0	12	NC	11	NC	12	
526		min	-.062	8	-.316	3	0	1	0	1	7364.641	8	NC	1	
527	4	max	.037	3	.721	8	0	12	0	12	NC	12	NC	12	
528		min	-.064	8	-.312	3	0	1	0	1	NC	1	NC	1	
529	5	max	.038	3	.708	8	0	12	0	12	NC	12	NC	12	
530		min	-.066	8	-.307	3	0	1	0	1	NC	1	NC	1	
531	M27	1	max	.038	3	.708	8	0	12	0	12	NC	12	NC	12
532		min	-.066	8	-.307	3	0	1	0	1	NC	1	NC	1	
533	2	max	.04	3	.681	8	0	12	0	12	NC	4	NC	12	
534		min	-.069	8	-.296	3	0	1	0	1	3803.608	8	NC	1	
535	3	max	.041	3	.648	8	0	12	0	12	NC	2	NC	12	
536		min	-.072	8	-.282	3	0	1	0	1	2747.742	12	NC	1	
537	4	max	.043	3	.608	8	0	12	0	12	NC	4	NC	12	
538		min	-.075	8	-.265	3	0	1	0	1	4277.522	12	NC	1	
539	5	max	.044	3	.564	8	0	12	0	12	NC	12	NC	12	
540		min	-.078	8	-.248	3	0	1	0	1	NC	1	NC	1	



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y' Ratio	LC	(n) L/z' Ratio	LC	
541	M28	1	max	.044	3	.564	8	0	12	0	12	NC	12	NC	12
542			min	-.078	8	-.248	3	0	1	0	1	NC	1	NC	1
543		2	max	.045	3	.524	8	0	12	0	12	NC	11	NC	12
544			min	-.079	8	-.23	3	0	1	0	1	7172.068	8	NC	1
545		3	max	.045	3	.482	8	0	12	0	12	NC	6	NC	12
546			min	-.081	8	-.211	3	0	1	0	1	5049.279	12	NC	1
547		4	max	.046	3	.436	8	0	12	0	12	NC	11	NC	12
548			min	-.082	8	-.192	3	0	1	0	1	8505.83	8	NC	1
549		5	max	.046	3	.388	8	0	12	0	12	NC	12	NC	12
550			min	-.083	8	-.171	3	0	1	0	1	NC	1	NC	1
551	M29	1	max	.046	3	.388	8	0	12	0	12	NC	12	NC	12
552			min	-.083	8	-.171	3	0	1	0	1	NC	1	NC	1
553		2	max	.046	3	.33	8	0	12	0	12	NC	4	NC	12
554			min	-.083	8	-.143	3	0	1	0	1	3939.687	12	NC	1
555		3	max	.046	3	.268	8	0	12	0	12	NC	4	NC	12
556			min	-.083	8	-.115	3	0	1	0	1	2559.787	12	NC	1
557		4	max	.045	3	.2	8	0	12	0	12	NC	4	NC	12
558			min	-.082	8	-.086	3	0	1	0	1	4144.775	12	NC	1
559		5	max	.045	3	.129	8	0	12	0	12	NC	12	NC	12
560			min	-.082	8	-.056	3	0	1	0	1	NC	1	NC	1
561	M133	1	max	.593	8	.451	8	0	12	0	12	NC	12	NC	12
562			min	-.239	3	-.152	3	0	1	0	1	NC	1	NC	1
563		2	max	.591	8	.435	8	0	12	0	12	NC	12	NC	12
564			min	-.238	3	-.139	3	0	1	0	1	8664.325	8	NC	1
565		3	max	.589	8	.416	8	0	12	0	12	NC	12	NC	12
566			min	-.236	3	-.123	3	0	1	0	1	8986.721	8	NC	1
567		4	max	.586	8	.396	8	0	12	0	12	NC	12	NC	12
568			min	-.235	3	-.107	3	0	1	0	1	NC	1	NC	1
569		5	max	.584	8	.376	8	0	12	0	12	NC	12	NC	12
570			min	-.233	3	-.09	3	0	1	0	1	NC	1	NC	1
571	M114A	1	max	.647	8	.251	8	0	12	0	12	NC	12	NC	12
572			min	-.247	3	-.042	3	0	1	0	1	NC	1	NC	1
573		2	max	.645	8	.229	8	0	12	0	12	NC	12	NC	12
574			min	-.245	3	-.024	3	0	1	0	1	7836.355	8	NC	1
575		3	max	.643	8	.206	5	0	12	0	12	NC	12	NC	12
576			min	-.244	3	-.006	3	0	1	0	1	5879.854	8	NC	1
577		4	max	.641	8	.183	5	0	12	0	12	NC	12	NC	12
578			min	-.243	3	.005	1	0	1	0	1	6804.895	8	NC	1
579		5	max	.639	8	.157	5	0	12	0	12	NC	12	NC	12
580			min	-.241	3	.011	1	0	1	0	1	NC	1	NC	1
581	M112B	1	max	.41	8	.866	3	0	12	0	12	NC	12	NC	12
582			min	-.033	3	-1.165	8	0	1	0	1	NC	1	NC	1
583		2	max	.416	8	.89	3	0	12	0	12	NC	10	NC	12
584			min	-.037	3	-1.203	8	0	1	0	1	1994.238	8	NC	1
585		3	max	.421	8	.908	3	0	12	0	12	NC	10	NC	12
586			min	-.04	3	-1.231	8	0	1	0	1	1304.891	8	NC	1
587		4	max	.426	8	.91	3	0	12	0	12	NC	10	NC	12
588			min	-.044	3	-1.232	8	0	1	0	1	2088.795	8	NC	1
589		5	max	.432	8	.906	3	0	12	0	12	NC	12	NC	12
590			min	-.047	3	-1.225	8	0	1	0	1	NC	1	NC	1
591	M125A	1	max	.325	5	.906	3	0	12	0	12	NC	12	NC	12
592			min	.009	1	-1.258	8	0	1	0	1	NC	1	NC	1
593		2	max	.33	5	.91	3	0	12	0	12	NC	10	NC	12
594			min	.008	1	-1.269	8	0	1	0	1	2039.117	8	NC	1
595		3	max	.335	5	.907	3	0	12	0	12	NC	10	NC	12
596			min	.007	1	-1.271	8	0	1	0	1	1275.633	8	NC	1
597		4	max	.341	5	.889	3	0	12	0	12	NC	10	NC	12



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...]	LC	(n) L/y' Ratio	LC	(n) L/z' Ratio	LC
598		min	.006	1	-1.246	8	0	1	0	1	1949.467	8	NC	1
599	5	max	.346	5	.864	3	0	12	0	12	NC	12	NC	12
600		min	.005	1	-1.209	8	0	1	0	1	NC	1	NC	1
601	M125B	1	max	.07	.067	3	0	12	0	12	NC	12	NC	12
602		min	-.222	3	-.259	8	0	1	0	1	NC	1	NC	1
603	2	max	.069	12	.118	3	0	12	0	12	NC	12	NC	12
604		min	-.221	3	-.33	8	0	1	0	1	NC	1	NC	1
605	3	max	.069	12	.17	3	0	12	0	12	NC	12	NC	12
606		min	-.22	3	-.403	8	0	1	0	1	4718.261	8	NC	1
607	4	max	.068	12	.216	3	0	12	0	12	NC	12	NC	12
608		min	-.219	3	-.466	8	0	1	0	1	7659.395	8	NC	1
609	5	max	.067	12	.261	3	0	12	0	12	NC	12	NC	12
610		min	-.218	3	-.528	8	0	1	0	1	NC	1	NC	1
611	M125C	1	max	.085	-.01	2	0	12	0	12	NC	12	NC	12
612		min	-.234	3	-.142	5	0	1	0	1	NC	1	NC	1
613	2	max	.084	12	-.005	2	0	12	0	12	NC	12	NC	12
614		min	-.233	3	-.168	5	0	1	0	1	9847.897	8	NC	1
615	3	max	.083	12	0	2	0	12	0	12	NC	12	NC	12
616		min	-.231	3	-.197	5	0	1	0	1	8300.361	8	NC	1
617	4	max	.081	12	.016	3	0	12	0	12	NC	12	NC	12
618		min	-.23	3	-.228	8	0	1	0	1	NC	1	NC	1
619	5	max	.08	12	.04	3	0	12	0	12	NC	12	NC	12
620		min	-.228	3	-.262	8	0	1	0	1	NC	1	NC	1
621	M126	1	max	.045	.129	8	0	12	0	12	NC	12	NC	12
622		min	-.082	8	-.056	3	0	1	0	1	NC	1	NC	1
623	2	max	.044	3	.1	8	0	12	0	12	NC	12	NC	12
624		min	-.081	8	-.044	3	0	1	0	1	NC	1	NC	1
625	3	max	.044	3	.072	8	0	12	0	12	NC	12	NC	12
626		min	-.08	8	-.031	3	0	1	0	1	NC	1	NC	1
627	4	max	.043	3	.044	8	0	12	0	12	NC	12	NC	12
628		min	-.079	8	-.019	3	0	1	0	1	NC	1	NC	1
629	5	max	.043	3	.018	8	0	12	0	12	NC	12	NC	12
630		min	-.078	8	-.007	3	0	1	0	1	NC	1	NC	1
631	M128	1	max	.032	.023	12	0	12	0	12	NC	12	NC	12
632		min	-.044	3	-.056	3	0	1	0	1	NC	1	NC	1
633	2	max	.032	8	.034	12	0	12	0	12	NC	12	NC	12
634		min	-.045	3	-.084	3	0	1	0	1	7390.752	5	NC	1
635	3	max	.033	8	.046	12	0	12	0	12	NC	12	NC	12
636		min	-.045	3	-.113	3	0	1	0	1	4677.706	5	NC	1
637	4	max	.034	8	.06	12	0	12	0	12	NC	12	NC	12
638		min	-.046	3	-.141	3	0	1	0	1	8214.629	5	NC	1
639	5	max	.034	8	.074	12	0	12	0	12	NC	12	NC	12
640		min	-.046	3	-.168	3	0	1	0	1	NC	1	NC	1
641	M139	1	max	-.02	.77	3	0	12	0	12	NC	12	NC	12
642		min	-.268	5	-1.115	8	0	1	0	1	NC	1	NC	1
643	2	max	-.021	2	.8	3	0	12	0	12	NC	10	NC	12
644		min	-.264	5	-1.157	8	0	1	0	1	3136.871	8	NC	1
645	3	max	-.021	2	.826	3	0	12	0	12	NC	10	NC	12
646		min	-.261	5	-1.191	8	0	1	0	1	2191.426	8	NC	1
647	4	max	-.022	2	.844	3	0	12	0	12	NC	11	NC	12
648		min	-.257	5	-1.214	8	0	1	0	1	3651.101	8	NC	1
649	5	max	-.023	2	.86	3	0	12	0	12	NC	12	NC	12
650		min	-.253	5	-1.233	8	0	1	0	1	NC	1	NC	1
651	M140	1	max	-.006	.63	3	0	12	0	12	NC	12	NC	12
652		min	-.233	6	-.959	8	0	1	0	1	NC	1	NC	1
653	2	max	-.005	12	.648	3	0	12	0	12	NC	12	NC	12
654		min	-.233	6	-.983	8	0	1	0	1	NC	1	NC	1



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC (n)	L/y' Ratio	LC (n)	L/z' Ratio	LC
655	3	max	-.004	12	.665	3	0	12	0	12	NC	12	NC	12
656		min	-.232	6	-1.006	8	0	1	0	1	NC	1	NC	1
657	4	max	-.003	12	.682	3	0	12	0	12	NC	12	NC	12
658		min	-.232	6	-1.029	8	0	1	0	1	NC	1	NC	1
659	5	max	-.002	12	.698	3	0	12	0	12	NC	12	NC	12
660		min	-.231	6	-1.052	8	0	1	0	1	NC	1	NC	1
661	M137A	1	max	.154	3	.698	3	0	12	0	12	NC	12	12
662		min	-.565	8	-.867	8	0	1	0	1	NC	1	NC	1
663	2	max	.153	3	.682	3	0	12	0	12	NC	12	NC	12
664		min	-.563	8	-.843	8	0	1	0	1	NC	1	NC	1
665	3	max	.152	3	.665	3	0	12	0	12	NC	12	NC	12
666		min	-.562	8	-.819	8	0	1	0	1	NC	1	NC	1
667	4	max	.151	3	.648	3	0	12	0	12	NC	12	NC	12
668		min	-.56	8	-.795	8	0	1	0	1	NC	1	NC	1
669	5	max	.15	3	.631	3	0	12	0	12	NC	12	NC	12
670		min	-.559	8	-.77	8	0	1	0	1	NC	1	NC	1
671	M138	1	max	-.02	12	.702	3	0	12	0	12	NC	12	12
672		min	-.24	6	-1.046	8	0	1	0	1	NC	1	NC	1
673	2	max	-.019	12	.718	3	0	12	0	12	NC	12	NC	12
674		min	-.24	6	-1.068	8	0	1	0	1	NC	1	NC	1
675	3	max	-.018	12	.734	3	0	12	0	12	NC	12	NC	12
676		min	-.239	6	-1.089	8	0	1	0	1	NC	1	NC	1
677	4	max	-.017	12	.75	3	0	12	0	12	NC	12	NC	12
678		min	-.239	6	-1.109	8	0	1	0	1	NC	1	NC	1
679	5	max	-.016	12	.764	3	0	12	0	12	NC	12	NC	12
680		min	-.238	6	-1.128	8	0	1	0	1	NC	1	NC	1
681	M70	1	max	.06	3	.039	8	0	12	0	12	NC	12	12
682		min	-.025	12	-.083	3	0	1	0	1	NC	1	NC	1
683	2	max	.06	3	.046	8	0	12	0	12	NC	12	NC	12
684		min	-.025	12	-.103	3	0	1	0	1	NC	1	NC	1
685	3	max	.061	3	.055	12	0	12	0	12	NC	12	NC	12
686		min	-.025	12	-.123	3	0	1	0	1	NC	1	NC	1
687	4	max	.062	3	.064	12	0	12	0	12	NC	12	NC	12
688		min	-.026	12	-.143	3	0	1	0	1	NC	1	NC	1
689	5	max	.063	3	.073	12	0	12	0	12	NC	12	NC	12
690		min	-.026	12	-.162	3	0	1	0	1	NC	1	NC	1
691	M71	1	max	.067	12	.038	12	0	12	0	12	NC	12	12
692		min	-.149	3	-.089	3	0	1	0	1	NC	1	NC	1
693	2	max	.068	8	.045	12	0	12	0	12	NC	12	NC	12
694		min	-.15	3	-.104	3	0	1	0	1	NC	1	NC	1
695	3	max	.068	8	.052	12	0	12	0	12	NC	12	NC	12
696		min	-.15	3	-.119	3	0	1	0	1	NC	1	NC	1
697	4	max	.069	8	.058	12	0	12	0	12	NC	12	NC	12
698		min	-.151	3	-.133	3	0	1	0	1	NC	1	NC	1
699	5	max	.069	8	.064	12	0	12	0	12	NC	12	NC	12
700		min	-.151	3	-.147	3	0	1	0	1	NC	1	NC	1
701	M72	1	max	.157	3	.066	8	0	12	0	12	NC	12	12
702		min	-.069	12	-.141	3	0	1	0	1	NC	1	NC	1
703	2	max	.157	3	.071	8	0	12	0	12	NC	12	NC	12
704		min	-.069	12	-.154	3	0	1	0	1	NC	1	NC	1
705	3	max	.158	3	.075	12	0	12	0	12	NC	12	NC	12
706		min	-.069	12	-.166	3	0	1	0	1	NC	1	NC	1
707	4	max	.158	3	.081	12	0	12	0	12	NC	12	NC	12
708		min	-.07	12	-.178	3	0	1	0	1	NC	1	NC	1
709	5	max	.158	3	.086	12	0	12	0	12	NC	12	NC	12
710		min	-.07	12	-.189	3	0	1	0	1	NC	1	NC	1
711	M73	1	max	.084	12	.072	12	0	12	0	12	NC	12	12



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC (n)	L/y' Ratio	LC (n)	L/z' Ratio	LC	
712		min	-.185	3	-.164	3	0	1	0	1	NC	1	NC	1	
713	2	max	.085	12	.079	12	0	12	0	12	NC	12	NC	12	
714		min	-.185	3	-.177	3	0	1	0	1	NC	1	NC	1	
715	3	max	.085	12	.084	12	0	12	0	12	NC	12	NC	12	
716		min	-.186	3	-.189	3	0	1	0	1	NC	1	NC	1	
717	4	max	.085	12	.089	12	0	12	0	12	NC	12	NC	12	
718		min	-.187	3	-.201	3	0	1	0	1	NC	1	NC	1	
719	5	max	.086	12	.094	12	0	12	0	12	NC	12	NC	12	
720		min	-.187	3	-.212	3	0	1	0	1	NC	1	NC	1	
721	M74	1	max	.215	3	.084	12	0	12	0	12	NC	12	NC	12
722		min	-.096	12	-.183	3	0	1	0	1	NC	1	NC	1	
723	2	max	.216	3	.087	12	0	12	0	12	NC	12	NC	12	
724		min	-.096	12	-.191	3	0	1	0	1	NC	1	NC	1	
725	3	max	.216	3	.09	12	0	12	0	12	NC	12	NC	12	
726		min	-.097	12	-.198	3	0	1	0	1	NC	1	NC	1	
727	4	max	.216	3	.093	12	0	12	0	12	NC	12	NC	12	
728		min	-.097	12	-.205	3	0	1	0	1	NC	1	NC	1	
729	5	max	.217	3	.096	12	0	12	0	12	NC	12	NC	12	
730		min	-.097	12	-.211	3	0	1	0	1	NC	1	NC	1	
731	M75	1	max	.107	12	.085	12	0	12	0	12	NC	12	NC	12
732		min	-.235	3	-.191	3	0	1	0	1	NC	1	NC	1	
733	2	max	.107	12	.088	12	0	12	0	12	NC	12	NC	12	
734		min	-.235	3	-.197	3	0	1	0	1	NC	1	NC	1	
735	3	max	.107	12	.089	12	0	12	0	12	NC	12	NC	12	
736		min	-.236	3	-.202	3	0	1	0	1	NC	1	NC	1	
737	4	max	.108	12	.09	12	0	12	0	12	NC	12	NC	12	
738		min	-.236	3	-.206	3	0	1	0	1	NC	1	NC	1	
739	5	max	.108	12	.091	12	0	12	0	12	NC	12	NC	12	
740		min	-.237	3	-.209	3	0	1	0	1	NC	1	NC	1	
741	M76	1	max	.131	3	.13	12	0	12	0	12	NC	12	NC	12
742		min	-.056	12	-.287	3	0	1	0	1	NC	1	NC	1	
743	2	max	.131	3	.13	12	0	12	0	12	NC	12	NC	12	
744		min	-.056	12	-.29	3	0	1	0	1	NC	1	NC	1	
745	3	max	.132	3	.13	12	0	12	0	12	NC	12	NC	12	
746		min	-.056	12	-.291	3	0	1	0	1	7979.233	3	NC	1	
747	4	max	.132	3	.128	12	0	12	0	12	NC	12	NC	12	
748		min	-.057	12	-.29	3	0	1	0	1	NC	1	NC	1	
749	5	max	.132	3	.126	12	0	12	0	12	NC	12	NC	12	
750		min	-.057	12	-.288	3	0	1	0	1	NC	1	NC	1	
751	M77	1	max	.132	12	.04	12	0	12	0	12	NC	12	NC	12
752		min	-.303	3	-.094	3	0	1	0	1	NC	1	NC	1	
753	2	max	.132	12	.037	12	0	12	0	12	NC	12	NC	12	
754		min	-.303	3	-.09	3	0	1	0	1	NC	1	NC	1	
755	3	max	.132	12	.033	12	0	12	0	12	NC	12	NC	12	
756		min	-.303	3	-.086	3	0	1	0	1	9035.262	8	NC	1	
757	4	max	.132	12	.028	12	0	12	0	12	NC	12	NC	12	
758		min	-.303	3	-.081	3	0	1	0	1	NC	1	NC	1	
759	5	max	.132	12	.022	12	0	12	0	12	NC	12	NC	12	
760		min	-.303	3	-.084	6	0	1	0	1	NC	1	NC	1	
761	M78	1	max	.058	8	.134	12	0	12	0	12	NC	12	NC	12
762		min	-.002	1	-.311	3	0	1	0	1	NC	1	NC	1	
763	2	max	.059	8	.127	12	0	12	0	12	NC	12	NC	12	
764		min	-.002	1	-.303	3	0	1	0	1	NC	1	NC	1	
765	3	max	.059	8	.119	12	0	12	0	12	NC	12	NC	12	
766		min	-.002	1	-.293	3	0	1	0	1	NC	1	NC	1	
767	4	max	.059	8	.11	12	0	12	0	12	NC	12	NC	12	
768		min	-.002	1	-.282	3	0	1	0	1	NC	1	NC	1	



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...]	LC (n)	L/y' Ratio	LC (n)	L/z' Ratio	LC
769	5	max	.059	8	.101	12	0	12	0	12	NC	12	NC	12
770		min	-.002	1	-.27	3	0	1	0	1	NC	1	NC	1
771	M79	1	max	.1	.029	3	0	12	0	12	NC	12	NC	12
772		min	-.269	3	-.059	8	0	1	0	1	NC	1	NC	1
773		2	max	.1	.041	3	0	12	0	12	NC	12	NC	12
774		min	-.269	3	-.078	8	0	1	0	1	NC	1	NC	1
775		3	max	.1	.054	3	0	12	0	12	NC	12	NC	12
776		min	-.269	3	-.099	8	0	1	0	1	8025.941	8	NC	1
777		4	max	.1	.068	3	0	12	0	12	NC	12	NC	12
778		min	-.268	3	-.121	8	0	1	0	1	NC	1	NC	1
779		5	max	.1	.084	3	0	12	0	12	NC	12	NC	12
780		min	-.268	3	-.145	8	0	1	0	1	NC	1	NC	1
781	M80	1	max	.12	.052	12	0	12	0	12	NC	12	NC	12
782		min	-.213	3	-.194	6	0	1	0	1	NC	1	NC	1
783		2	max	.122	.034	12	0	12	0	12	NC	12	NC	12
784		min	-.214	3	-.203	6	0	1	0	1	7736.412	8	NC	1
785		3	max	.123	.015	12	0	12	0	12	NC	11	NC	12
786		min	-.215	3	-.213	6	0	1	0	1	5679.55	8	NC	1
787		4	max	.124	-.006	12	0	12	0	12	NC	12	NC	12
788		min	-.216	3	-.224	6	0	1	0	1	7433.646	8	NC	1
789		5	max	.126	-.019	2	0	12	0	12	NC	12	NC	12
790		min	-.217	3	-.238	5	0	1	0	1	NC	1	NC	1
791	M81	1	max	.014	.172	3	0	12	0	12	NC	12	NC	12
792		min	-.239	6	-.202	8	0	1	0	1	NC	1	NC	1
793		2	max	.013	.203	3	0	12	0	12	NC	12	NC	12
794		min	-.239	6	-.245	8	0	1	0	1	NC	1	NC	1
795		3	max	.012	.234	3	0	12	0	12	NC	12	NC	12
796		min	-.239	6	-.288	8	0	1	0	1	NC	1	NC	1
797		4	max	.012	.266	3	0	12	0	12	NC	12	NC	12
798		min	-.239	6	-.333	8	0	1	0	1	NC	1	NC	1
799		5	max	.011	.299	3	0	12	0	12	NC	12	NC	12
800		min	-.24	6	-.378	8	0	1	0	1	NC	1	NC	1
801	M82	1	max	.301	-.01	2	0	12	0	12	NC	12	NC	12
802		min	-.331	3	-.291	5	0	1	0	1	NC	1	NC	1
803		2	max	.301	-.003	2	0	12	0	12	NC	12	NC	12
804		min	-.332	3	-.326	5	0	1	0	1	NC	1	NC	1
805		3	max	.302	.01	3	0	12	0	12	NC	12	NC	12
806		min	-.333	3	-.36	8	0	1	0	1	NC	1	NC	1
807		4	max	.303	.037	3	0	12	0	12	NC	12	NC	12
808		min	-.334	3	-.396	8	0	1	0	1	NC	1	NC	1
809		5	max	.304	.064	3	0	12	0	12	NC	12	NC	12
810		min	-.334	3	-.433	8	0	1	0	1	NC	1	NC	1
811	M83	1	max	.021	.34	3	0	12	0	12	NC	12	NC	12
812		min	-.39	8	-.357	8	0	1	0	1	NC	1	NC	1
813		2	max	.021	.367	3	0	12	0	12	NC	12	NC	12
814		min	-.391	8	-.394	8	0	1	0	1	NC	1	NC	1
815		3	max	.022	.395	3	0	12	0	12	NC	12	NC	12
816		min	-.392	8	-.433	8	0	1	0	1	NC	1	NC	1
817		4	max	.022	.423	3	0	12	0	12	NC	12	NC	12
818		min	-.393	8	-.472	8	0	1	0	1	NC	1	NC	1
819		5	max	.023	.451	3	0	12	0	12	NC	12	NC	12
820		min	-.393	8	-.51	8	0	1	0	1	NC	1	NC	1
821	M84	1	max	.421	.113	3	0	12	0	12	NC	12	NC	12
822		min	-.437	3	-.488	8	0	1	0	1	NC	1	NC	1
823		2	max	.422	.14	3	0	12	0	12	NC	12	NC	12
824		min	-.438	3	-.525	8	0	1	0	1	NC	1	NC	1
825		3	max	.422	.167	3	0	12	0	12	NC	12	NC	12



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC (n)	L/y' Ratio	LC (n)	L/z' Ratio	LC
826		min	-.438	3	-.561	8	0	1	0	1	NC	1	NC	1
827	4	max	.423	8	.194	3	0	12	0	12	NC	12	NC	12
828		min	-.439	3	-.597	8	0	1	0	1	NC	1	NC	1
829	5	max	.424	8	.221	3	0	12	0	12	NC	12	NC	12
830		min	-.439	3	-.635	8	0	1	0	1	NC	1	NC	1
831	M85	1	max	.166	.463	3	0	12	0	12	NC	12	NC	12
832		min	-.578	8	-.498	8	0	1	0	1	NC	1	NC	1
833	2	max	.166	3	.49	3	0	12	0	12	NC	12	NC	12
834		min	-.579	8	-.536	8	0	1	0	1	NC	1	NC	1
835	3	max	.167	3	.517	3	0	12	0	12	NC	12	NC	12
836		min	-.579	8	-.572	8	0	1	0	1	NC	1	NC	1
837	4	max	.167	3	.543	3	0	12	0	12	NC	12	NC	12
838		min	-.58	8	-.608	8	0	1	0	1	NC	1	NC	1
839	5	max	.168	3	.569	3	0	12	0	12	NC	12	NC	12
840		min	-.581	8	-.643	8	0	1	0	1	NC	1	NC	1
841	M86	1	max	.518	.275	3	0	12	0	12	NC	12	NC	12
842		min	-.525	3	-.694	8	0	1	0	1	NC	1	NC	1
843	2	max	.518	8	.3	3	0	12	0	12	NC	12	NC	12
844		min	-.526	3	-.729	8	0	1	0	1	NC	1	NC	1
845	3	max	.519	8	.325	3	0	12	0	12	NC	12	NC	12
846		min	-.526	3	-.762	8	0	1	0	1	9162.132	8	NC	1
847	4	max	.519	8	.349	3	0	12	0	12	NC	12	NC	12
848		min	-.527	3	-.794	8	0	1	0	1	NC	1	NC	1
849	5	max	.52	8	.372	3	0	12	0	12	NC	12	NC	12
850		min	-.527	3	-.825	8	0	1	0	1	NC	1	NC	1
851	M87	1	max	.304	.569	3	0	12	0	12	NC	12	NC	12
852		min	-.754	8	-.618	8	0	1	0	1	NC	1	NC	1
853	2	max	.304	3	.591	3	0	12	0	12	NC	12	NC	12
854		min	-.755	8	-.648	8	0	1	0	1	NC	1	NC	1
855	3	max	.305	3	.614	3	0	12	0	12	NC	12	NC	12
856		min	-.755	8	-.679	8	0	1	0	1	NC	1	NC	1
857	4	max	.305	3	.637	3	0	12	0	12	NC	12	NC	12
858		min	-.756	8	-.71	8	0	1	0	1	NC	1	NC	1
859	5	max	.306	3	.659	3	0	12	0	12	NC	12	NC	12
860		min	-.756	8	-.74	8	0	1	0	1	NC	1	NC	1
861	M88	1	max	.576	.429	3	0	12	0	12	NC	12	NC	12
862		min	-.585	3	-.887	8	0	1	0	1	NC	1	NC	1
863	2	max	.576	8	.45	3	0	12	0	12	NC	12	NC	12
864		min	-.586	3	-.914	8	0	1	0	1	NC	1	NC	1
865	3	max	.577	8	.469	3	0	12	0	12	NC	12	NC	12
866		min	-.586	3	-.939	8	0	1	0	1	NC	1	NC	1
867	4	max	.577	8	.487	3	0	12	0	12	NC	12	NC	12
868		min	-.586	3	-.963	8	0	1	0	1	NC	1	NC	1
869	5	max	.577	8	.506	3	0	12	0	12	NC	12	NC	12
870		min	-.586	3	-.988	8	0	1	0	1	NC	1	NC	1
871	M89	1	max	.435	.64	3	0	12	0	12	NC	12	NC	12
872		min	-.916	8	-.687	8	0	1	0	1	NC	1	NC	1
873	2	max	.436	3	.659	3	0	12	0	12	NC	12	NC	12
874		min	-.916	8	-.711	8	0	1	0	1	9121.269	8	NC	1
875	3	max	.436	3	.676	3	0	12	0	12	NC	12	NC	12
876		min	-.917	8	-.734	8	0	1	0	1	7084.461	8	NC	1
877	4	max	.436	3	.691	3	0	12	0	12	NC	12	NC	12
878		min	-.917	8	-.755	8	0	1	0	1	9766.13	8	NC	1
879	5	max	.437	3	.706	3	0	12	0	12	NC	12	NC	12
880		min	-.917	8	-.775	8	0	1	0	1	NC	1	NC	1
881	M90	1	max	.596	.557	3	0	12	0	12	NC	12	NC	12
882		min	-.615	3	-1.043	8	0	1	0	1	NC	1	NC	1



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC	(n) L/y' Ratio	LC	(n) L/z' Ratio	LC	
883	2	max	.596	8	.571	3	0	12	0	12	NC	12	NC	12	
884		min	-.615	3	-1.06	8	0	1	0	1	NC	1	NC	1	
885	3	max	.596	8	.583	3	0	12	0	12	NC	12	NC	12	
886		min	-.616	3	-1.076	8	0	1	0	1	NC	1	NC	1	
887	4	max	.596	8	.595	3	0	12	0	12	NC	12	NC	12	
888		min	-.616	3	-1.091	8	0	1	0	1	NC	1	NC	1	
889	5	max	.597	8	.607	3	0	12	0	12	NC	12	NC	12	
890		min	-.616	3	-1.106	8	0	1	0	1	NC	1	NC	1	
891	M91	1	max	.529	3	.684	3	0	12	0	12	NC	12	NC	12
892		min	-1.026	8	-.725	8	0	1	0	1	NC	1	NC	1	
893	2	max	.529	3	.695	3	0	12	0	12	NC	12	NC	12	
894		min	-1.027	8	-.739	8	0	1	0	1	8936.454	8	NC	1	
895	3	max	.529	3	.705	3	0	12	0	12	NC	12	NC	12	
896		min	-1.027	8	-.752	8	0	1	0	1	6485.703	8	NC	1	
897	4	max	.529	3	.713	3	0	12	0	12	NC	12	NC	12	
898		min	-1.027	8	-.763	8	0	1	0	1	8357.002	8	NC	1	
899	5	max	.529	3	.72	3	0	12	0	12	NC	12	NC	12	
900		min	-1.028	8	-.771	8	0	1	0	1	NC	1	NC	1	
901	M92	1	max	.329	8	.761	3	0	12	0	12	NC	12	NC	12
902		min	-.469	3	-1.242	8	0	1	0	1	NC	1	NC	1	
903	2	max	.329	8	.768	3	0	12	0	12	NC	12	NC	12	
904		min	-.469	3	-1.25	8	0	1	0	1	7383.416	8	NC	1	
905	3	max	.33	8	.773	3	0	12	0	12	NC	11	NC	12	
906		min	-.469	3	-1.254	8	0	1	0	1	5981.281	8	NC	1	
907	4	max	.33	8	.775	3	0	12	0	12	NC	12	NC	12	
908		min	-.469	3	-1.256	8	0	1	0	1	8620.754	8	NC	1	
909	5	max	.33	8	.776	3	0	12	0	12	NC	12	NC	12	
910		min	-.469	3	-1.256	8	0	1	0	1	NC	1	NC	1	
911	M93	1	max	.474	3	.773	3	0	12	0	12	NC	12	NC	12
912		min	-.964	8	-.869	8	0	1	0	1	NC	1	NC	1	
913	2	max	.474	3	.772	3	0	12	0	12	NC	12	NC	12	
914		min	-.964	8	-.867	8	0	1	0	1	8658.489	8	NC	1	
915	3	max	.474	3	.77	3	0	12	0	12	NC	11	NC	12	
916		min	-.964	8	-.863	8	0	1	0	1	6000.84	8	NC	1	
917	4	max	.474	3	.765	3	0	12	0	12	NC	12	NC	12	
918		min	-.964	8	-.857	8	0	1	0	1	7398.603	8	NC	1	
919	5	max	.474	3	.758	3	0	12	0	12	NC	12	NC	12	
920		min	-.964	8	-.846	8	0	1	0	1	NC	1	NC	1	
921	M94	1	max	.441	8	.716	3	0	12	0	12	NC	12	NC	12
922		min	-.536	3	-1.205	8	0	1	0	1	NC	1	NC	1	
923	2	max	.44	8	.71	3	0	12	0	12	NC	12	NC	12	
924		min	-.535	3	-1.195	8	0	1	0	1	8824.552	8	NC	1	
925	3	max	.44	8	.702	3	0	12	0	12	NC	12	NC	12	
926		min	-.535	3	-1.183	8	0	1	0	1	6866.794	8	NC	1	
927	4	max	.44	8	.693	3	0	12	0	12	NC	12	NC	12	
928		min	-.535	3	-1.169	8	0	1	0	1	9489.481	8	NC	1	
929	5	max	.44	8	.682	3	0	12	0	12	NC	12	NC	12	
930		min	-.535	3	-1.154	8	0	1	0	1	NC	1	NC	1	
931	M95	1	max	.617	3	.609	3	0	12	0	12	NC	12	NC	12
932		min	-1.096	8	-.569	8	0	1	0	1	NC	1	NC	1	
933	2	max	.617	3	.598	3	0	12	0	12	NC	12	NC	12	
934		min	-1.096	8	-.552	8	0	1	0	1	NC	1	NC	1	
935	3	max	.616	3	.587	3	0	12	0	12	NC	12	NC	12	
936		min	-1.095	8	-.536	8	0	1	0	1	NC	1	NC	1	
937	4	max	.616	3	.574	3	0	12	0	12	NC	12	NC	12	
938		min	-1.095	8	-.519	8	0	1	0	1	NC	1	NC	1	
939	5	max	.616	3	.561	3	0	12	0	12	NC	12	NC	12	



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...]	LC (n)	L/y' Ratio	LC (n)	L/z' Ratio	LC
940		min	-1.095	8	-.499	8	0	1	0	1	NC	1	NC	1
941	M96	max	.27	12	.718	3	0	12	0	12	NC	12	NC	12
942		min	-.422	3	-1.174	8	0	1	0	1	NC	1	NC	1
943		max	.269	12	.704	3	0	12	0	12	NC	12	NC	12
944		min	-.422	3	-1.153	8	0	1	0	1	9733.946	8	NC	1
945		max	.269	12	.688	3	0	12	0	12	NC	12	NC	12
946		min	-.422	3	-1.131	8	0	1	0	1	7078.892	8	NC	1
947		max	.269	12	.671	3	0	12	0	12	NC	12	NC	12
948		min	-.422	3	-1.107	8	0	1	0	1	9135.996	8	NC	1
949		max	.269	12	.653	3	0	12	0	12	NC	12	NC	12
950		min	-.421	3	-1.081	8	0	1	0	1	NC	1	NC	1
951	M97	max	.596	3	.498	3	0	12	0	12	NC	12	NC	12
952		min	-1.04	8	-.393	8	0	1	0	1	NC	1	NC	1
953		max	.596	3	.479	3	0	12	0	12	NC	12	NC	12
954		min	-1.04	8	-.367	8	0	1	0	1	NC	1	NC	1
955		max	.596	3	.461	3	0	12	0	12	NC	12	NC	12
956		min	-1.039	8	-.341	8	0	1	0	1	NC	1	NC	1
957		max	.596	3	.442	3	0	12	0	12	NC	12	NC	12
958		min	-1.039	8	-.314	8	0	1	0	1	NC	1	NC	1
959		max	.595	3	.422	3	0	12	0	12	NC	12	NC	12
960		min	-1.039	8	-.286	8	0	1	0	1	NC	1	NC	1
961	M98	max	.162	12	.666	3	0	12	0	12	NC	12	NC	12
962		min	-.298	3	-1.074	8	0	1	0	1	NC	1	NC	1
963		max	.162	12	.645	3	0	12	0	12	NC	12	NC	12
964		min	-.297	3	-1.044	8	0	1	0	1	NC	1	NC	1
965		max	.162	12	.622	3	0	12	0	12	NC	12	NC	12
966		min	-.297	3	-1.012	8	0	1	0	1	NC	1	NC	1
967		max	.162	12	.6	3	0	12	0	12	NC	12	NC	12
968		min	-.296	3	-.98	8	0	1	0	1	NC	1	NC	1
969		max	.161	12	.577	3	0	12	0	12	NC	12	NC	12
970		min	-.296	3	-.948	8	0	1	0	1	NC	1	NC	1
971	M99	max	.538	3	.362	3	0	12	0	12	NC	12	NC	12
972		min	-.933	8	-.226	12	0	1	0	1	NC	1	NC	1
973		max	.538	3	.339	3	0	12	0	12	NC	12	NC	12
974		min	-.932	8	-.208	12	0	1	0	1	NC	1	NC	1
975		max	.538	3	.315	3	0	12	0	12	NC	12	NC	12
976		min	-.932	8	-.188	12	0	1	0	1	9743.653	8	NC	1
977		max	.537	3	.291	3	0	12	0	12	NC	12	NC	12
978		min	-.931	8	-.168	12	0	1	0	1	NC	1	NC	1
979		max	.537	3	.265	3	0	12	0	12	NC	12	NC	12
980		min	-.93	8	-.147	12	0	1	0	1	NC	1	NC	1
981	M100	max	.036	12	.579	3	0	12	0	12	NC	12	NC	12
982		min	-.214	6	-.922	8	0	1	0	1	NC	1	NC	1
983		max	.036	12	.553	3	0	12	0	12	NC	12	NC	12
984		min	-.214	6	-.886	8	0	1	0	1	NC	1	NC	1
985		max	.036	12	.526	3	0	12	0	12	NC	12	NC	12
986		min	-.214	6	-.849	8	0	1	0	1	NC	1	NC	1
987		max	.035	12	.5	3	0	12	0	12	NC	12	NC	12
988		min	-.215	6	-.811	8	0	1	0	1	NC	1	NC	1
989		max	.035	12	.473	3	0	12	0	12	NC	12	NC	12
990		min	-.215	6	-.773	8	0	1	0	1	NC	1	NC	1
991	M101	max	.449	3	.212	3	0	12	0	12	NC	12	NC	12
992		min	-.784	8	-.096	12	0	1	0	1	NC	1	NC	1
993		max	.448	3	.189	6	0	12	0	12	NC	12	NC	12
994		min	-.784	8	-.073	12	0	1	0	1	NC	1	NC	1
995		max	.448	3	.198	6	0	12	0	12	NC	12	NC	12
996		min	-.783	8	-.05	12	0	1	0	1	NC	1	NC	1



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...]	LC (n)	L/y' Ratio	LC (n)	L/z' Ratio	LC	
997	4	max	.447	3	.208	6	0	12	0	12	NC	12	NC	12	
998		min	-.782	8	-.027	12	0	1	0	1	NC	1	NC	1	
999	5	max	.447	3	.218	6	0	12	0	12	NC	12	NC	12	
1000		min	-.781	8	-.003	12	0	1	0	1	NC	1	NC	1	
1001	M102	1	max	-.004	2	.458	3	0	12	0	12	NC	12	NC	12
1002		min	-.336	5	-.73	8	0	1	0	1	NC	1	NC	1	
1003	2	max	-.004	2	.431	3	0	12	0	12	NC	12	NC	12	
1004		min	-.337	5	-.692	8	0	1	0	1	NC	1	NC	1	
1005	3	max	-.004	2	.403	3	0	12	0	12	NC	12	NC	12	
1006		min	-.337	5	-.653	8	0	1	0	1	NC	1	NC	1	
1007	4	max	-.004	2	.375	3	0	12	0	12	NC	12	NC	12	
1008		min	-.338	5	-.614	8	0	1	0	1	NC	1	NC	1	
1009	5	max	-.004	2	.348	3	0	12	0	12	NC	12	NC	12	
1010		min	-.339	5	-.578	8	0	1	0	1	NC	1	NC	1	
1011	M103	1	max	.344	3	.272	5	0	12	0	12	NC	12	NC	12
1012		min	-.613	8	.014	1	0	1	0	1	NC	1	NC	1	
1013	2	max	.344	3	.305	5	0	12	0	12	NC	12	NC	12	
1014		min	-.612	8	.008	1	0	1	0	1	NC	1	NC	1	
1015	3	max	.343	3	.339	5	0	12	0	12	NC	12	NC	12	
1016		min	-.611	8	0	3	0	1	0	1	NC	1	NC	1	
1017	4	max	.342	3	.374	8	0	12	0	12	NC	12	NC	12	
1018		min	-.61	8	-.026	3	0	1	0	1	NC	1	NC	1	
1019	5	max	.341	3	.411	8	0	12	0	12	NC	12	NC	12	
1020		min	-.609	8	-.053	3	0	1	0	1	NC	1	NC	1	
1021	M104	1	max	.177	3	.297	3	0	12	0	12	NC	12	NC	12
1022		min	-.609	8	-.41	8	0	1	0	1	NC	1	NC	1	
1023	2	max	.178	3	.261	3	0	12	0	12	NC	12	NC	12	
1024		min	-.611	8	-.362	8	0	1	0	1	NC	1	NC	1	
1025	3	max	.18	3	.227	3	0	12	0	12	NC	12	NC	12	
1026		min	-.612	8	-.316	8	0	1	0	1	NC	1	NC	1	
1027	4	max	.181	3	.194	3	0	12	0	12	NC	12	NC	12	
1028		min	-.614	8	-.271	8	0	1	0	1	NC	1	NC	1	
1029	5	max	.182	3	.162	3	0	12	0	12	NC	12	NC	12	
1030		min	-.616	8	-.227	8	0	1	0	1	NC	1	NC	1	
1031	M105	1	max	.215	3	.501	8	0	12	0	12	NC	12	NC	12
1032		min	-.423	8	-.115	3	0	1	0	1	NC	1	NC	1	
1033	2	max	.214	3	.534	8	0	12	0	12	NC	12	NC	12	
1034		min	-.422	8	-.14	3	0	1	0	1	5856.299	8	NC	1	
1035	3	max	.213	3	.564	8	0	12	0	12	NC	11	NC	12	
1036		min	-.421	8	-.162	3	0	1	0	1	4893.721	8	NC	1	
1037	4	max	.212	3	.59	8	0	12	0	12	NC	12	NC	12	
1038		min	-.419	8	-.183	3	0	1	0	1	7375.132	8	NC	1	
1039	5	max	.211	3	.615	8	0	12	0	12	NC	12	NC	12	
1040		min	-.418	8	-.203	3	0	1	0	1	NC	1	NC	1	
1041	M106	1	max	.282	3	.079	3	0	12	0	12	NC	12	NC	12
1042		min	-.742	8	-.063	12	0	1	0	1	NC	1	NC	1	
1043	2	max	.282	3	.06	3	0	12	0	12	NC	12	NC	12	
1044		min	-.743	8	-.045	12	0	1	0	1	6920.253	8	NC	1	
1045	3	max	.283	3	.042	3	0	12	0	12	NC	11	NC	12	
1046		min	-.743	8	-.028	12	0	1	0	1	5208.912	8	NC	1	
1047	4	max	.283	3	.031	6	0	12	0	12	NC	12	NC	12	
1048		min	-.744	8	-.012	12	0	1	0	1	6992.645	8	NC	1	
1049	5	max	.284	3	.034	5	0	12	0	12	NC	12	NC	12	
1050		min	-.744	8	.002	12	0	1	0	1	NC	1	NC	1	
1051	M107	1	max	.022	3	.745	8	0	12	0	12	NC	12	NC	12
1052		min	-.011	12	-.283	3	0	1	0	1	NC	1	NC	1	
1053	2	max	.021	3	.758	8	0	12	0	12	NC	12	NC	12	



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...]	LC	(n) L/y' Ratio	LC	(n) L/z' Ratio	LC	
1054		min	-.01	12	-.295	3	0	1	0	1	7484.982	8	NC	1	
1055	3	max	.021	6	.769	8	0	12	0	12	NC	12	NC	12	
1056		min	-.01	12	-.306	3	0	1	0	1	5508.024	8	NC	1	
1057	4	max	.021	6	.778	8	0	12	0	12	NC	12	NC	12	
1058		min	-.009	12	-.315	3	0	1	0	1	7207.01	8	NC	1	
1059	5	max	.021	6	.784	8	0	12	0	12	NC	12	NC	12	
1060		min	-.009	12	-.323	3	0	1	0	1	NC	1	NC	1	
1061	M108	1	max	.312	3	.264	8	0	12	0	12	NC	12	NC	12
1062		min	-.738	8	-.087	3	0	1	0	1	NC	1	NC	1	
1063	2	max	.312	3	.267	8	0	12	0	12	NC	12	NC	12	
1064		min	-.738	8	-.093	3	0	1	0	1	7682.011	8	NC	1	
1065	3	max	.312	3	.268	8	0	12	0	12	NC	11	NC	12	
1066		min	-.738	8	-.097	3	0	1	0	1	6429.163	8	NC	1	
1067	4	max	.311	3	.267	8	0	12	0	12	NC	12	NC	12	
1068		min	-.738	8	-.1	3	0	1	0	1	9718.479	8	NC	1	
1069	5	max	.311	3	.265	8	0	12	0	12	NC	12	NC	12	
1070		min	-.737	8	-.102	3	0	1	0	1	NC	1	NC	1	
1071	M109	1	max	.39	8	.679	8	0	12	0	12	NC	12	NC	12
1072		min	-.155	3	-.289	3	0	1	0	1	NC	1	NC	1	
1073	2	max	.39	8	.675	8	0	12	0	12	NC	12	NC	12	
1074		min	-.155	3	-.29	3	0	1	0	1	6212.138	8	NC	1	
1075	3	max	.39	8	.668	8	0	12	0	12	NC	11	NC	12	
1076		min	-.155	3	-.29	3	0	1	0	1	4740.146	8	NC	1	
1077	4	max	.39	8	.658	8	0	12	0	12	NC	12	NC	12	
1078		min	-.155	3	-.288	3	0	1	0	1	6423.852	8	NC	1	
1079	5	max	.39	8	.646	8	0	12	0	12	NC	12	NC	12	
1080		min	-.155	3	-.285	3	0	1	0	1	NC	1	NC	1	
1081	M110	1	max	.243	3	.526	8	0	12	0	12	NC	12	NC	12
1082		min	-.541	8	-.215	3	0	1	0	1	NC	1	NC	1	
1083	2	max	.242	3	.512	8	0	12	0	12	NC	12	NC	12	
1084		min	-.541	8	-.211	3	0	1	0	1	NC	1	NC	1	
1085	3	max	.242	3	.498	8	0	12	0	12	NC	12	NC	12	
1086		min	-.54	8	-.207	3	0	1	0	1	7902.297	8	NC	1	
1087	4	max	.241	3	.482	8	0	12	0	12	NC	12	NC	12	
1088		min	-.539	8	-.201	3	0	1	0	1	NC	1	NC	1	
1089	5	max	.241	3	.464	8	0	12	0	12	NC	12	NC	12	
1090		min	-.539	8	-.195	3	0	1	0	1	NC	1	NC	1	
1091	M111	1	max	.499	8	.506	8	0	12	0	12	NC	12	NC	12
1092		min	-.21	3	-.227	3	0	1	0	1	NC	1	NC	1	
1093	2	max	.499	8	.489	8	0	12	0	12	NC	12	NC	12	
1094		min	-.21	3	-.22	3	0	1	0	1	9265.93	8	NC	1	
1095	3	max	.498	8	.469	8	0	12	0	12	NC	11	NC	12	
1096		min	-.21	3	-.213	3	0	1	0	1	7528.286	8	NC	1	
1097	4	max	.497	8	.448	8	0	12	0	12	NC	12	NC	12	
1098		min	-.209	3	-.204	3	0	1	0	1	NC	1	NC	1	
1099	5	max	.497	8	.427	8	0	12	0	12	NC	12	NC	12	
1100		min	-.209	3	-.196	3	0	1	0	1	NC	1	NC	1	
1101	M112	1	max	.195	3	.497	8	0	12	0	12	NC	12	NC	12
1102		min	-.426	8	-.209	3	0	1	0	1	NC	1	NC	1	
1103	2	max	.195	3	.471	8	0	12	0	12	NC	12	NC	12	
1104		min	-.425	8	-.198	3	0	1	0	1	NC	1	NC	1	
1105	3	max	.194	3	.443	8	0	12	0	12	NC	11	NC	12	
1106		min	-.424	8	-.187	3	0	1	0	1	7759.207	8	NC	1	
1107	4	max	.194	3	.414	8	0	12	0	12	NC	12	NC	12	
1108		min	-.423	8	-.175	3	0	1	0	1	9057.144	8	NC	1	
1109	5	max	.193	3	.382	8	0	12	0	12	NC	12	NC	12	
1110		min	-.422	8	-.161	3	0	1	0	1	NC	1	NC	1	



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC (n)	L/y' Ratio	LC (n)	L/z' Ratio	LC
M113	1	max	.384	8	.421	8	0	12	0	12	NC	12	NC	12
		min	-.162	3	-.192	3	0	1	0	1	NC	1	NC	1
1113	2	max	.383	8	.393	8	0	12	0	12	NC	12	NC	12
1114		min	-.162	3	-.18	3	0	1	0	1	NC	1	NC	1
1115	3	max	.382	8	.365	8	0	12	0	12	NC	12	NC	12
1116		min	-.161	3	-.168	3	0	1	0	1	NC	1	NC	1
1117	4	max	.382	8	.336	8	0	12	0	12	NC	12	NC	12
1118		min	-.161	3	-.156	3	0	1	0	1	NC	1	NC	1
1119	5	max	.381	8	.306	8	0	12	0	12	NC	12	NC	12
1120		min	-.161	3	-.143	3	0	1	0	1	NC	1	NC	1
M114	1	max	.154	3	.356	8	0	12	0	12	NC	12	NC	12
1122		min	-.334	8	-.149	3	0	1	0	1	NC	1	NC	1
1123	2	max	.154	3	.323	8	0	12	0	12	NC	12	NC	12
1124		min	-.333	8	-.135	3	0	1	0	1	NC	1	NC	1
1125	3	max	.153	3	.29	8	0	12	0	12	NC	12	NC	12
1126		min	-.332	8	-.12	3	0	1	0	1	NC	1	NC	1
1127	4	max	.153	3	.256	8	0	12	0	12	NC	12	NC	12
1128		min	-.331	8	-.106	3	0	1	0	1	NC	1	NC	1
1129	5	max	.152	3	.221	8	0	12	0	12	NC	12	NC	12
1130		min	-.331	8	-.09	3	0	1	0	1	NC	1	NC	1
M115	1	max	.163	8	.362	8	0	12	0	12	NC	12	NC	12
1132		min	-.064	3	-.165	3	0	1	0	1	NC	1	NC	1
1133	2	max	.161	8	.319	8	0	12	0	12	NC	12	NC	12
1134		min	-.063	3	-.146	3	0	1	0	1	NC	1	NC	1
1135	3	max	.16	8	.273	8	0	12	0	12	NC	12	NC	12
1136		min	-.062	3	-.125	3	0	1	0	1	NC	1	NC	1
1137	4	max	.159	8	.227	8	0	12	0	12	NC	12	NC	12
1138		min	-.062	3	-.105	3	0	1	0	1	NC	1	NC	1
1139	5	max	.157	8	.18	8	0	12	0	12	NC	12	NC	12
1140		min	-.061	3	-.084	3	0	1	0	1	NC	1	NC	1
M120	1	max	.14	12	.033	3	0	12	0	12	NC	12	NC	12
1142		min	-.314	3	-.026	8	0	1	0	1	NC	1	NC	1
1143	2	max	.14	12	.031	3	0	12	0	12	NC	12	NC	12
1144		min	-.314	3	-.029	8	0	1	0	1	NC	1	NC	1
1145	3	max	.14	12	.03	3	0	12	0	12	NC	12	NC	12
1146		min	-.314	3	-.032	8	0	1	0	1	NC	1	NC	1
1147	4	max	.141	12	.028	3	0	12	0	12	NC	12	NC	12
1148		min	-.314	3	-.036	8	0	1	0	1	NC	1	NC	1
1149	5	max	.141	12	.026	3	0	12	0	12	NC	12	NC	12
1150		min	-.315	3	-.038	8	0	1	0	1	NC	1	NC	1
M122	1	max	.259	3	.173	3	0	12	0	12	NC	12	NC	12
1152		min	-.106	12	-.087	8	0	1	0	1	NC	1	NC	1
1153	2	max	.258	3	.169	3	0	12	0	12	NC	12	NC	12
1154		min	-.106	12	-.078	12	0	1	0	1	NC	1	NC	1
1155	3	max	.258	3	.164	3	0	12	0	12	NC	12	NC	12
1156		min	-.105	12	-.074	12	0	1	0	1	NC	1	NC	1
1157	4	max	.258	3	.159	3	0	12	0	12	NC	12	NC	12
1158		min	-.105	12	-.07	12	0	1	0	1	NC	1	NC	1
1159	5	max	.258	3	.154	3	0	12	0	12	NC	12	NC	12
1160		min	-.105	12	-.066	12	0	1	0	1	NC	1	NC	1
M124	1	max	.138	5	.117	12	0	12	0	12	NC	12	NC	12
1162		min	.006	1	-.28	3	0	1	0	1	NC	1	NC	1
1163	2	max	.139	5	.109	12	0	12	0	12	NC	12	NC	12
1164		min	.006	1	-.269	3	0	1	0	1	NC	1	NC	1
1165	3	max	.139	5	.101	12	0	12	0	12	NC	12	NC	12
1166		min	.006	1	-.259	3	0	1	0	1	NC	1	NC	1
1167	4	max	.139	5	.092	12	0	12	0	12	NC	12	NC	12



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC (n)	L/y' Ratio	LC (n)	L/z' Ratio	LC	
1168		min	.006	1	-.248	3	0	1	0	1	NC	1	NC	1	
1169	5	max	.139	5	.084	12	0	12	0	12	NC	12	NC	12	
1170		min	.006	1	-.238	3	0	1	0	1	NC	1	NC	1	
1171	M127	1	max	.271	3	.177	3	0	12	0	12	NC	12	NC	12
1172		min	-.685	8	-.38	8	0	1	0	1	NC	1	NC	1	
1173	2	max	.271	3	.173	3	0	12	0	12	NC	12	NC	12	
1174		min	-.685	8	-.378	8	0	1	0	1	NC	1	NC	1	
1175	3	max	.27	3	.169	3	0	12	0	12	NC	12	NC	12	
1176		min	-.684	8	-.375	8	0	1	0	1	NC	1	NC	1	
1177	4	max	.27	3	.165	3	0	12	0	12	NC	12	NC	12	
1178		min	-.683	8	-.373	8	0	1	0	1	NC	1	NC	1	
1179	5	max	.27	3	.16	3	0	12	0	12	NC	12	NC	12	
1180		min	-.682	8	-.371	8	0	1	0	1	NC	1	NC	1	
1181	M129	1	max	.323	3	.026	3	0	12	0	12	NC	12	NC	12
1182		min	-.754	8	-.025	8	0	1	0	1	NC	1	NC	1	
1183	2	max	.323	3	.028	3	0	12	0	12	NC	12	NC	12	
1184		min	-.754	8	-.034	8	0	1	0	1	NC	1	NC	1	
1185	3	max	.323	3	.03	3	0	12	0	12	NC	12	NC	12	
1186		min	-.754	8	-.041	8	0	1	0	1	NC	1	NC	1	
1187	4	max	.323	3	.032	3	0	12	0	12	NC	12	NC	12	
1188		min	-.753	8	-.049	8	0	1	0	1	NC	1	NC	1	
1189	5	max	.322	3	.034	3	0	12	0	12	NC	12	NC	12	
1190		min	-.753	8	-.058	8	0	1	0	1	NC	1	NC	1	
1191	M135	1	max	.907	3	0	12	.377	5	0	12	NC	12	NC	12
1192		min	-1.243	8	0	1	-.007	3	0	1	NC	1	NC	1	
1193	2	max	.907	3	0	12	.378	5	0	12	NC	12	NC	12	
1194		min	-1.243	8	0	1	-.007	3	0	1	NC	1	NC	1	
1195	3	max	.907	3	0	12	.378	5	0	12	NC	12	NC	12	
1196		min	-1.243	8	0	1	-.007	3	0	1	NC	1	NC	1	
1197	4	max	.907	3	0	12	.379	5	0	12	NC	12	NC	12	
1198		min	-1.243	8	0	1	-.007	3	0	1	NC	1	NC	1	
1199	5	max	.907	3	0	12	.379	5	0	12	NC	12	NC	12	
1200		min	-1.243	8	0	1	-.007	3	0	1	NC	1	NC	1	
1201	M112A	1	max	-.003	2	.693	8	0	12	0	12	NC	12	NC	12
1202		min	-.227	5	-.301	3	0	1	0	1	NC	1	NC	1	
1203	2	max	-.004	2	.674	8	0	12	0	12	NC	12	NC	12	
1204		min	-.226	5	-.286	3	0	1	0	1	NC	1	NC	1	
1205	3	max	-.004	2	.656	8	0	12	0	12	NC	12	NC	12	
1206		min	-.226	5	-.273	3	0	1	0	1	NC	1	NC	1	
1207	4	max	-.004	2	.637	8	0	12	0	12	NC	12	NC	12	
1208		min	-.226	5	-.259	3	0	1	0	1	NC	1	NC	1	
1209	5	max	-.004	2	.617	8	0	12	0	12	NC	12	NC	12	
1210		min	-.226	5	-.244	3	0	1	0	1	NC	1	NC	1	
1211	M113A	1	max	.259	8	.116	12	0	12	0	12	NC	12	NC	12
1212		min	-.064	3	-.279	3	0	1	0	1	NC	1	NC	1	
1213	2	max	.259	8	.105	12	0	12	0	12	NC	12	NC	12	
1214		min	-.065	3	-.264	3	0	1	0	1	NC	1	NC	1	
1215	3	max	.259	8	.094	12	0	12	0	12	NC	12	NC	12	
1216		min	-.065	3	-.251	3	0	1	0	1	NC	1	NC	1	
1217	4	max	.259	8	.083	12	0	12	0	12	NC	12	NC	12	
1218		min	-.065	3	-.237	3	0	1	0	1	NC	1	NC	1	
1219	5	max	.259	8	.071	12	0	12	0	12	NC	12	NC	12	
1220		min	-.065	3	-.222	3	0	1	0	1	NC	1	NC	1	
1221	M115B	1	max	.068	3	.672	8	0	12	0	12	NC	12	NC	12
1222		min	-.319	8	-.285	3	0	1	0	1	NC	1	NC	1	
1223	2	max	.068	3	.658	8	0	12	0	12	NC	12	NC	12	
1224		min	-.318	8	-.274	3	0	1	0	1	NC	1	NC	1	



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...	LC (n)	L/y' Ratio	LC (n)	L/z' Ratio	LC	
1225	3	max	.068	3	.645	8	0	12	0	12	NC	12	NC	12	
1226		min	-.318	8	-.263	3	0	1	0	1	NC	1	NC	1	
1227	4	max	.067	3	.631	8	0	12	0	12	NC	12	NC	12	
1228		min	-.317	8	-.252	3	0	1	0	1	NC	1	NC	1	
1229	5	max	.067	3	.618	8	0	12	0	12	NC	12	NC	12	
1230		min	-.317	8	-.241	3	0	1	0	1	NC	1	NC	1	
1231	M118	1	max	.768	8	.073	3	0	12	0	12	NC	12	NC	12
1232		min	-.319	3	-.152	8	0	1	0	1	NC	1	NC	1	
1233	2	max	.769	8	.074	3	0	12	0	12	NC	12	NC	12	
1234		min	-.32	3	-.15	8	0	1	0	1	NC	1	NC	1	
1235	3	max	.77	8	.075	3	0	12	0	12	NC	12	NC	12	
1236		min	-.32	3	-.148	8	0	1	0	1	NC	1	NC	1	
1237	4	max	.77	8	.077	3	0	12	0	12	NC	12	NC	12	
1238		min	-.321	3	-.146	8	0	1	0	1	NC	1	NC	1	
1239	5	max	.771	8	.079	3	0	12	0	12	NC	12	NC	12	
1240		min	-.321	3	-.144	8	0	1	0	1	NC	1	NC	1	
1241	M119	1	max	.503	8	.55	8	0	12	0	12	NC	12	NC	12
1242		min	-.173	3	-.225	3	0	1	0	1	NC	1	NC	1	
1243	2	max	.503	8	.559	8	0	12	0	12	NC	12	NC	12	
1244		min	-.174	3	-.233	3	0	1	0	1	NC	1	NC	1	
1245	3	max	.504	8	.567	8	0	12	0	12	NC	12	NC	12	
1246		min	-.174	3	-.241	3	0	1	0	1	NC	1	NC	1	
1247	4	max	.504	8	.576	8	0	12	0	12	NC	12	NC	12	
1248		min	-.174	3	-.249	3	0	1	0	1	NC	1	NC	1	
1249	5	max	.505	8	.584	8	0	12	0	12	NC	12	NC	12	
1250		min	-.175	3	-.257	3	0	1	0	1	NC	1	NC	1	
1251	M120A	1	max	.061	12	.081	12	0	12	0	12	NC	12	NC	12
1252		min	-.182	3	-.2	3	0	1	0	1	NC	1	NC	1	
1253	2	max	.061	12	.088	12	0	12	0	12	NC	12	NC	12	
1254		min	-.182	3	-.208	3	0	1	0	1	NC	1	NC	1	
1255	3	max	.061	12	.095	12	0	12	0	12	NC	12	NC	12	
1256		min	-.182	3	-.217	3	0	1	0	1	NC	1	NC	1	
1257	4	max	.062	12	.101	12	0	12	0	12	NC	12	NC	12	
1258		min	-.183	3	-.225	3	0	1	0	1	NC	1	NC	1	
1259	5	max	.062	12	.108	12	0	12	0	12	NC	12	NC	12	
1260		min	-.183	3	-.233	3	0	1	0	1	NC	1	NC	1	
1261	M121	1	max	.123	12	.144	3	0	12	0	12	NC	12	NC	12
1262		min	-.282	3	-.063	12	0	1	0	1	NC	1	NC	1	
1263	2	max	.123	12	.146	3	0	12	0	12	NC	12	NC	12	
1264		min	-.283	3	-.065	12	0	1	0	1	NC	1	NC	1	
1265	3	max	.123	12	.147	3	0	12	0	12	NC	12	NC	12	
1266		min	-.283	3	-.067	12	0	1	0	1	NC	1	NC	1	
1267	4	max	.123	12	.149	3	0	12	0	12	NC	12	NC	12	
1268		min	-.284	3	-.071	8	0	1	0	1	NC	1	NC	1	
1269	5	max	.124	12	.151	3	0	12	0	12	NC	12	NC	12	
1270		min	-.284	3	-.078	8	0	1	0	1	NC	1	NC	1	
1271	M129A	1	max	.074	3	.183	8	0	12	0	12	NC	12	NC	12
1272		min	-.153	8	-.074	3	0	1	0	1	NC	1	NC	1	
1273	2	max	.073	3	.146	8	0	12	0	12	NC	12	NC	12	
1274		min	-.152	8	-.057	3	0	1	0	1	NC	1	NC	1	
1275	3	max	.073	3	.11	8	0	12	0	12	NC	12	NC	12	
1276		min	-.151	8	-.041	3	0	1	0	1	NC	1	NC	1	
1277	4	max	.072	3	.073	8	0	12	0	12	NC	12	NC	12	
1278		min	-.15	8	-.025	3	0	1	0	1	NC	1	NC	1	
1279	5	max	.072	3	.034	8	0	12	0	12	NC	12	NC	12	
1280		min	-.149	8	-.009	3	0	1	0	1	NC	1	NC	1	
1281	M130	1	max	.032	8	.149	8	0	12	0	12	NC	12	NC	12



Envelope Member Section Deflections Service (Continued)

Member	Sec		x [in]	LC	y [in]	LC	z [in]	LC	x Rotate [r...]	LC (n)	L/y' Ratio	LC (n)	L/z' Ratio	LC	
1282		min	-.008	3	-.072	3	0	1	0	1	NC	1	NC	1	
1283	2	max	.031	8	.11	8	0	12	0	12	NC	12	NC	12	
1284		min	-.007	3	-.054	3	0	1	0	1	NC	1	NC	1	
1285	3	max	.03	8	.071	8	0	12	0	12	NC	11	NC	12	
1286		min	-.007	3	-.037	3	0	1	0	1	8978.056	8	NC	1	
1287	4	max	.029	8	.034	8	0	12	0	12	NC	12	NC	12	
1288		min	-.006	3	-.021	3	0	1	0	1	NC	1	NC	1	
1289	5	max	.028	5	0	12	0	12	0	12	NC	12	NC	12	
1290		min	-.006	3	-.005	6	0	1	0	1	NC	1	NC	1	
1291	M131	1	max	.073	3	.03	12	0	12	0	12	NC	12	NC	12
1292		min	-.037	8	-.072	3	0	1	0	1	NC	1	NC	1	
1293	2	max	.072	3	.023	12	0	12	0	12	NC	12	NC	12	
1294		min	-.037	8	-.056	3	0	1	0	1	NC	1	NC	1	
1295	3	max	.072	3	.016	12	0	12	0	12	NC	12	NC	12	
1296		min	-.037	8	-.04	3	0	1	0	1	NC	1	NC	1	
1297	4	max	.071	3	.009	12	0	12	0	12	NC	12	NC	12	
1298		min	-.036	8	-.025	3	0	1	0	1	NC	1	NC	1	
1299	5	max	.071	3	.002	12	0	12	0	12	NC	12	NC	12	
1300		min	-.036	8	-.013	6	0	1	0	1	NC	1	NC	1	
1301	M132	1	max	.002	12	.036	8	0	12	0	12	NC	12	NC	12
1302		min	-.012	6	-.071	3	0	1	0	1	NC	1	NC	1	
1303	2	max	.001	12	.03	8	0	12	0	12	NC	12	NC	12	
1304		min	-.012	6	-.054	3	0	1	0	1	NC	1	NC	1	
1305	3	max	.001	12	.024	8	0	12	0	12	NC	12	NC	12	
1306		min	-.012	6	-.037	3	0	1	0	1	NC	1	NC	1	
1307	4	max	.001	12	.018	8	0	12	0	12	NC	12	NC	12	
1308		min	-.011	6	-.021	3	0	1	0	1	NC	1	NC	1	
1309	5	max	0	12	.012	8	0	12	0	12	NC	12	NC	12	
1310		min	-.011	6	-.005	3	0	1	0	1	NC	1	NC	1	

Envelope AISC 15th(360-16): ASD Steel Code Checks

Member	Shape	Code C...	Loc[ft]	LC	Shear ...	Loc[ft]	Dir	LC	Pnc/om [k]	Pnt/om [k]	Mnyy/om ...	Mnzz/om ...	Cb	Eqn
1	M43	1.9x0.09	.162	0	3	.001	0	3	5.777	16.862	.81	.81	1	H1-1b*
2	M44	1.9x0.09	.125	0	12	.001	3.129	5	3.765	16.862	.81	.81	1	H1-1b*
3	M45	1.9x0.09	.422	3.087	8	.001	3.087	5	3.765	16.862	.81	.81	1	H1-1a
4	M46	1.9x0.09	.722	3.104	8	.001	3.104	5	3.765	16.862	.81	.81	1	H1-1a
5	M47	1.9x0.09	.301	3.081	8	.001	3.081	5	12.422	16.862	.81	.81	1	H1-1a
6	M48	1.9x0.09	.335	0	8	.001	0	5	12.422	16.862	.81	.81	1	H1-1a
7	M49	1.9x0.09	.336	2.287	8	.002	2.287	5	12.422	16.862	.81	.81	1	H1-1a
8	M50	1.9x0.09	.305	0	8	.001	0	5	12.422	16.862	.81	.81	1	H1-1a
9	M51	1.9x0.09	.745	0	8	.001	0	5	3.765	16.862	.81	.81	1	H1-1a
10	M52	1.9x0.09	.466	0	8	.001	0	5	3.765	16.862	.81	.81	1	H1-1a
11	M53	1.9x0.09	.067	3.102	8	.001	0	5	3.765	16.862	.81	.81	1	H1-1b*
12	M54	1.9x0.09	.162	3.12	3	.001	0	5	5.777	16.862	.81	.81	1	H1-1b*
13	M104A	1.9x0.09	.525	2.144	3	.004	0	8	5.777	16.862	.81	.81	1	H1-1a
14	M110A	1.9x0.09	.543	0	3	.006	2.083	8	5.777	16.862	.81	.81	1	H1-1a
15	M34	1.9x0.09	.428	2.72	3	.001	0	8	7.266	16.862	.81	.81	1	H1-1a
16	M63	1.9x0.09	.432	0	3	.001	0	8	7.266	16.862	.81	.81	1	H1-1a
17	M64	1.9x0.09	.279	0	3	.001	0	3	7.266	16.862	.81	.81	1	H1-1a
18	M121A	1.9x0.09	.548	1.414	3	.001	0	5	9.061	16.862	.81	.81	1	H1-1a
19	M119A	1.9x0.09	.540	0	3	.003	1.899	8	5.777	16.862	.81	.81	1	H1-1a
20	M117	1.9x0.09	.601	1.579	3	.006	0	8	9.061	16.862	.81	.81	1	H1-1a
21	M105A	1.9x0.09	.525	1.333	3	.001	0	5	9.061	16.862	.81	.81	1	H1-1a
22	M106A	1.9x0.09	.610	1.351	3	.007	0	8	9.061	16.862	.81	.81	1	H1-1a
23	M107A	1.9x0.09	.482	0	3	.001	0	8	9.061	16.862	.81	.81	1	H1-1a



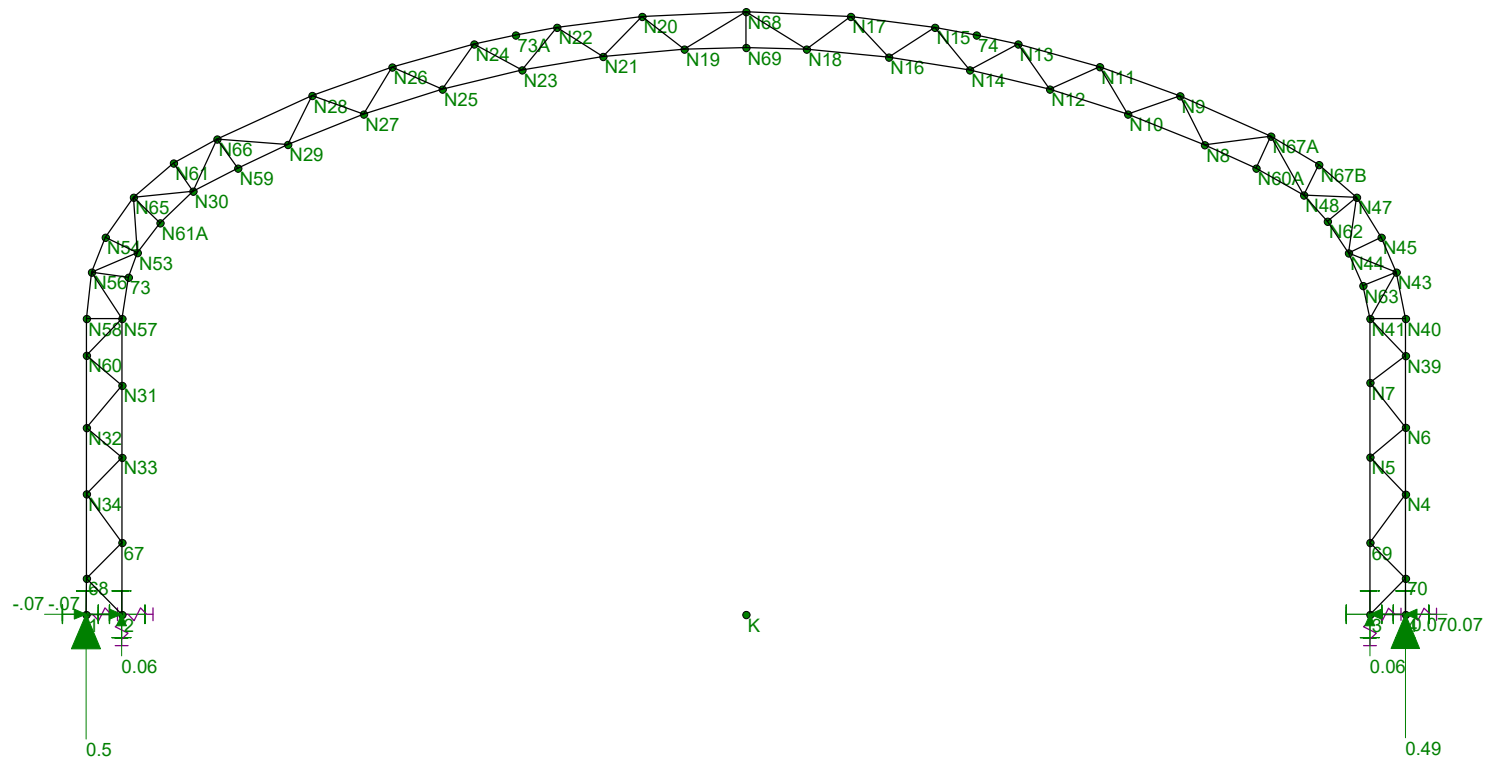
Envelope AISC 15th(360-16): ASD Steel Code Checks (Continued)

Member	Shape	Code C...	Loc[ft]	LC	Shear ...	Loc[ft]	Dir	LC	Pnc/om [k]	Pnt/om [k]	Mnvy/om ...	Mnzz/om ...	Cb	Eqn	
24	M111A	1.9x0.09	.545	2.065	3	.004	2.065	3	5.777	16.862	.81	.81	1	H1-1a	
25	M115C	1.9x0.09	.552	0	3	.005	1.734	8	9.061	16.862	.81	.81	1	H1-1a	
26	M116A	1.9x0.09	.524	0	3	.004	1.438	8	9.061	16.862	.81	.81	1	H1-1a	
27	M117A	1.9x0.09	.621	0	3	.011	1.271	8	9.061	16.862	.81	.81	1	H1-1a	
28	M122A	1.9x0.09	.076	0	3	.003	0	8	7.266	16.862	.81	.81	1	H1-1b*	
29	M125D	1.9x0.09	.278	3.212	3	.002	0	8	7.266	16.862	.81	.81	1	H1-1a	
30	M127A	1.9x0.09	.078	2.72	3	.001	0	3	7.266	16.862	.81	.81	1	H1-1b*	
31	M133A	1.9x0.09	.482	2.527	3	.001	0	8	9.061	16.862	.81	.81	1	H1-1a	
32	M137	1.9x0.09	.614	0	3	.012	.985	8	9.061	16.862	.81	.81	1	H1-1a	
33	M124A	2" x 3" x 0.08...	.037	1.344	8	.008	0	y	8	24.244	24.581	1.425	2.086	2....	H1-1b
34	M125	2" x 3" x 0.08...	.017	1.343	3	.004	1.343	y	3	24.245	24.581	1.425	2.086	2....	H1-1b
35	M2	1.9x0.09	.254	0	3	.016	1.36	8	7.266	16.862	.81	.81	1	H1-1a	
36	M3	1.9x0.09	.067	0	8	.017	0	5	7.266	16.862	.81	.81	1	H1-1b	
37	M4	1.9x0.09	.160	0	8	.019	2.716	8	9.061	16.862	.81	.81	1	H1-1b*	
38	M5	1.9x0.09	.352	0	8	.011	0	8	9.061	16.862	.81	.81	1	H1-1a	
39	M6	1.9x0.09	.380	1.791	8	.016	1.791	8	9.061	16.862	.81	.81	1	H1-1a	
40	M7	1.9x0.09	.431	0	8	.013	0	8	9.061	16.862	.81	.81	1	H1-1a	
41	M8	1.9x0.09	.426	1.768	8	.013	1.768	8	9.061	16.862	.81	.81	1	H1-1a	
42	M9	1.9x0.09	.636	0	8	.012	0	8	5.777	16.862	.81	.81	1	H1-1a	
43	M12	1.9x0.09	.150	0	3	.021	0	8	3.765	16.862	.81	.81	1	H1-1b*	
44	M13	1.9x0.09	.503	0	3	.032	0	8	3.765	16.862	.81	.81	1	H1-1a	
45	M18	1.9x0.09	.378	0	8	.033	0	8	12.422	16.862	.81	.81	1	H1-1a	
46	M19	1.9x0.09	.698	.815	3	.018	0	8	3.765	16.862	.81	.81	1	H1-1a	
47	M20	1.9x0.09	.503	3.214	3	.032	3.214	8	3.765	16.862	.81	.81	1	H1-1a	
48	M21	1.9x0.09	.156	3.203	8	.034	3.203	8	3.765	16.862	.81	.81	1	H1-1b	
49	M22	1.9x0.09	.391	3.954	8	.041	3.954	8	5.777	16.862	.81	.81	1	H1-1a	
50	M23	1.9x0.09	.770	0	8	.021	0	8	9.061	16.862	.81	.81	1	H1-1a	
51	M24	1.9x0.09	.753	1.412	8	.017	1.412	8	9.061	16.862	.81	.81	1	H1-1a	
52	M25	1.9x0.09	.702	.607	8	.013	0	12	9.061	16.862	.81	.81	1	H1-1a	
53	M26	1.9x0.09	.683	.611	8	.018	1.396	12	9.061	16.862	.81	.81	1	H1-1a	
54	M27	1.9x0.09	.521	1.196	8	.027	2.733	12	9.061	16.862	.81	.81	1	H1-1a	
55	M28	1.9x0.09	.360	2.502	12	.025	2.502	12	7.266	16.862	.81	.81	1	H1-1a	
56	M29	1.9x0.09	.120	3.189	9	.031	3.189	12	7.266	16.862	.81	.81	1	H1-1b	
57	M133	1.9x0.09	.907	0	8	.024	0	8	5.777	16.862	.81	.81	1	H1-1a	
58	M114A	1.9x0.09	.894	1.879	8	.021	1.879	8	5.777	16.862	.81	.81	1	H1-1a	
59	M112B	1.9x0.09	.442	3.931	8	.038	3.931	8	12.422	16.862	.81	.81	1	H1-1a	
60	M125A	1.9x0.09	.446	0	8	.038	0	8	12.422	16.862	.81	.81	1	H1-1a	
61	M125B	1.9x0.09	.163	0	8	.025	0	8	5.777	16.862	.81	.81	1	H1-1b	
62	M125C	1.9x0.09	.620	0	8	.014	0	8	5.777	16.862	.81	.81	1	H1-1a	
63	M126	1.9x0.09	.257	1.36	3	.015	1.36	12	7.266	16.862	.81	.81	1	H1-1a	
64	M128	1.9x0.09	.097	3.184	8	.022	3.184	8	7.266	16.862	.81	.81	1	H1-1b	
65	M139	1.9x0.09	.380	3.205	8	.032	3.205	8	12.422	16.862	.81	.81	1	H1-1a	
66	M140	1.9x0.09	.703	0	3	.019	0	8	3.765	16.862	.81	.81	1	H1-1a	
67	M137A	1.9x0.09	.702	1.607	3	.020	1.607	8	3.765	16.862	.81	.81	1	H1-1a	
68	M138	1.9x0.09	.700	.767	3	.018	1.601	8	3.765	16.862	.81	.81	1	H1-1a	
69	M70	1.66" x 0.085"	.046	2.265	3	.001	0	3	12.614	13.851	.579	.579	2....	H1-1b	
70	M71	1.66" x 0.085"	.065	0	3	.003	1.935	8	12.937	13.851	.579	.579	2....	H1-1b*	
71	M72	1.66" x 0.085"	.050	0	8	.001	1.752	5	13.097	13.851	.579	.579	1....	H1-1b*	
72	M73	1.66" x 0.085"	.074	0	3	.001	0	3	12.714	13.851	.579	.579	1....	H1-1b*	
73	M74	1.66" x 0.085"	.066	0	8	.002	0	5	13.153	13.851	.579	.579	2....	H1-1b*	
74	M75	1.66" x 0.085"	.073	0	8	.003	1.94	5	12.932	13.851	.579	.579	1....	H1-1b	
75	M76	1.66" x 0.085"	.049	0	8	.000	2.014	3	12.864	13.851	.579	.579	1....	H1-1b*	
76	M77	1.66" x 0.085"	.033	0	8	.001	1.938	5	12.934	13.851	.579	.579	1....	H1-1b	
77	M78	1.66" x 0.085"	.048	0	3	.000	2.122	5	12.759	13.851	.579	.579	1....	H1-1b*	
78	M79	1.66" x 0.085"	.032	2.003	8	.002	2.003	3	12.874	13.851	.579	.579	1....	H1-1b	
79	M80	1.66" x 0.085"	.120	0	3	.001	0	6	12.3	13.851	.579	.579	1....	H1-1b*	
80	M81	1.66" x 0.085"	.119	2.524	8	.001	2.524	10	12.331	13.851	.579	.579	1....	H1-1b*	



Envelope AISC 15th(360-16): ASD Steel Code Checks (Continued)

Member	Shape	Code C...	Loc[ft]	LC	Shear ...	Loc[ft]	Dir	LC	Pnc/om [k]	Pnt/om [k]	Mnyy/om ...	Mnzz/om ...	Cb	Eqn
81	M82	1.66" x 0.085"	.087	0	3	.002	0	8	12.806	13.851	.579	.579	2...	H1-1b*
82	M83	1.66" x 0.085"	.083	2.082	8	.002	2.082	5	12.798	13.851	.579	.579	2...	H1-1b*
83	M84	1.66" x 0.085"	.068	0	3	.003	0	8	12.804	13.851	.579	.579	2...	H1-1b*
84	M85	1.66" x 0.085"	.076	2.066	8	.001	0	9	12.814	13.851	.579	.579	1...	H1-1b*
85	M86	1.66" x 0.085"	.052	2.077	8	.001	2.077	5	12.803	13.851	.579	.579	1...	H1-1b
86	M87	1.66" x 0.085"	.062	2.069	8	.004	2.069	8	12.811	13.851	.579	.579	2...	H1-1b
87	M88	1.66" x 0.085"	.057	0	8	.004	0	8	12.799	13.851	.579	.579	2...	H1-1b
88	M89	1.66" x 0.085"	.047	0	8	.001	2.072	3	12.807	13.851	.579	.579	1...	H1-1b
89	M90	1.66" x 0.085"	.044	0	8	.003	0	8	12.782	13.851	.579	.579	2...	H1-1b
90	M91	1.66" x 0.085"	.043	2.068	8	.001	2.068	5	12.811	13.851	.579	.579	1...	H1-1b
91	M92	1.66" x 0.085"	.030	0	8	.001	0	5	12.145	13.851	.579	.579	1...	H1-1b
92	M93	1.66" x 0.085"	.032	2.725	8	.001	2.725	5	12.096	13.851	.579	.579	1...	H1-1b
93	M94	1.66" x 0.085"	.042	0	8	.001	0	5	12.863	13.851	.579	.579	1...	H1-1b
94	M95	1.66" x 0.085"	.044	2.111	8	.003	2.111	8	12.77	13.851	.579	.579	2...	H1-1b
95	M96	1.66" x 0.085"	.050	0	8	.001	0	3	12.821	13.851	.579	.579	1...	H1-1b*
96	M97	1.66" x 0.085"	.059	2.085	8	.004	2.085	8	12.795	13.851	.579	.579	2...	H1-1b
97	M98	1.66" x 0.085"	.063	0	8	.004	0	8	12.82	13.851	.579	.579	2...	H1-1b*
98	M99	1.66" x 0.085"	.051	0	8	.001	2.071	3	12.809	13.851	.579	.579	1...	H1-1b
99	M100	1.66" x 0.085"	.079	0	8	.001	0	6	12.798	13.851	.579	.579	1...	H1-1b*
100	M101	1.66" x 0.085"	.068	2.081	3	.002	2.081	8	12.799	13.851	.579	.579	2...	H1-1b*
101	M102	1.66" x 0.085"	.090	0	8	.003	0	5	12.816	13.851	.579	.579	2...	H1-1b*
102	M103	1.66" x 0.085"	.088	2.069	3	.001	0	3	12.811	13.851	.579	.579	2...	H1-1b*
103	M104	1.66" x 0.085"	.158	0	8	.001	2.682	5	12.148	13.851	.579	.579	1...	H1-1b*
104	M105	1.66" x 0.085"	.125	0	8	.003	2.168	8	12.713	13.851	.579	.579	1...	H1-1b
105	M106	1.66" x 0.085"	.066	2.26	8	.001	0	3	12.618	13.851	.579	.579	1...	H1-1b*
106	M107	1.66" x 0.085"	.075	2.098	8	.000	2.098	8	12.782	13.851	.579	.579	1...	H1-1b
107	M108	1.66" x 0.085"	.048	0	8	.003	1.873	5	12.992	13.851	.579	.579	1...	H1-1b
108	M109	1.66" x 0.085"	.036	0	8	.001	2.094	9	12.787	13.851	.579	.579	1...	H1-1b
109	M110	1.66" x 0.085"	.065	1.937	3	.001	1.937	10	12.934	13.851	.579	.579	1...	H1-1b*
110	M111	1.66" x 0.085"	.093	1.757	8	.003	0	9	13.093	13.851	.579	.579	1...	H1-1b*
111	M112	1.66" x 0.085"	.085	2.091	8	.002	0	8	12.789	13.851	.579	.579	1...	H1-1b
112	M113	1.66" x 0.085"	.107	1.748	8	.001	1.748	9	13.1	13.851	.579	.579	1...	H1-1b*
113	M114	1.66" x 0.085"	.077	1.929	8	.002	0	8	12.942	13.851	.579	.579	1...	H1-1b
114	M115	1.66" x 0.085"	.163	2.269	8	.003	0	12	12.609	13.851	.579	.579	2...	H1-1b*
115	M120	1.66" x 0.085"	.050	1.343	8	.005	1.343	8	13.403	13.851	.579	.579	2...	H1-1b
116	M122	1.66" x 0.085"	.040	0	3	.003	0	3	13.386	13.851	.579	.579	2...	H1-1b*
117	M124	1.66" x 0.085"	.048	0	3	.004	0	3	13.444	13.851	.579	.579	2...	H1-1b*
118	M127	1.66" x 0.085"	.084	0	8	.005	1.344	8	13.402	13.851	.579	.579	2...	H1-1b
119	M129	1.66" x 0.085"	.047	1.344	8	.006	0	8	13.402	13.851	.579	.579	2...	H1-1b
120	M135	1.66" x 0.085"	.017	1.344	8	.000	0	8	13.402	13.851	.579	.579	1	H1-1b*
121	M112A	1.66" x 0.085"	.097	1.351	8	.017	1.351	8	13.397	13.851	.579	.579	2...	H1-1b
122	M113A	1.66" x 0.085"	.078	1.324	8	.012	1.324	8	13.416	13.851	.579	.579	2...	H1-1b
123	M115B	1.66" x 0.085"	.075	0	8	.007	1.296	8	13.434	13.851	.579	.579	2...	H1-1b
124	M118	1.66" x 0.085"	.071	1.402	8	.003	0	5	13.363	13.851	.579	.579	2.2	H1-1b
125	M119	1.66" x 0.085"	.067	0	8	.005	0	8	13.374	13.851	.579	.579	2...	H1-1b
126	M120A	1.66" x 0.085"	.051	1.426	3	.001	1.426	10	13.347	13.851	.579	.579	2...	H1-1b*
127	M121	1.66" x 0.085"	.074	1.353	3	.003	1.353	5	13.396	13.851	.579	.579	1...	H1-1b*
128	M129A	1.66" x 0.085"	.115	1.912	8	.007	0	8	12.957	13.851	.579	.579	2...	H1-1b
129	M130	1.66" x 0.085"	.145	1.912	8	.002	1.912	9	12.957	13.851	.579	.579	1...	H1-1b*
130	M131	1.66" x 0.085"	.064	1.911	3	.003	1.911	3	12.958	13.851	.579	.579	2...	H1-1b*
131	M132	1.66" x 0.085"	.040	1.911	3	.003	0	8	12.958	13.851	.579	.579	1...	H1-1b



Results for LC 13, DL
 Reaction and Moment Units are k and k-ft

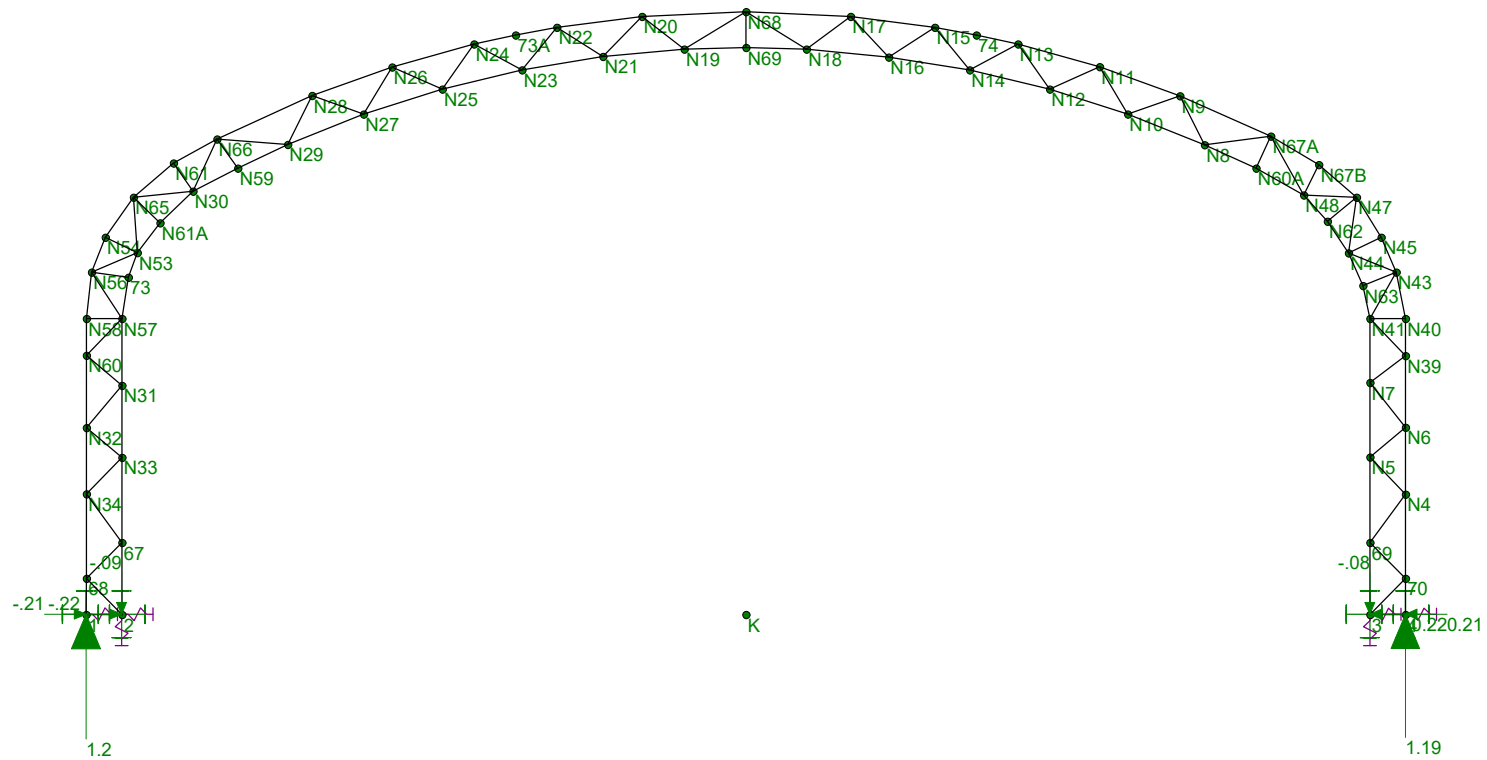
Big Top	50x72x23 DEM 18BB - Tallahassee, FL	SK - 8
Mo		May 27, 2021 at 11:32 AM
221-80		50x72x23 DEM 18BB - Tallahassee, FL.r3d



Joint Reactions (By Combination)

	LC	Joint Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]
1	13	1	0	.498	-.071	0	0	0
2	13	2	0	.058	-.073	0	0	0
3	13	3	0	.062	.073	0	0	0
4	13	4	0	.493	.071	0	0	0
5	13	Totals:	0	1.111	0			
6	13	COG (ft):	X: 0	Y: 15.238	Z: 24.95			

Reactions due to DL only



Results for LC 14, RLL
 Reaction and Moment Units are k and k-ft

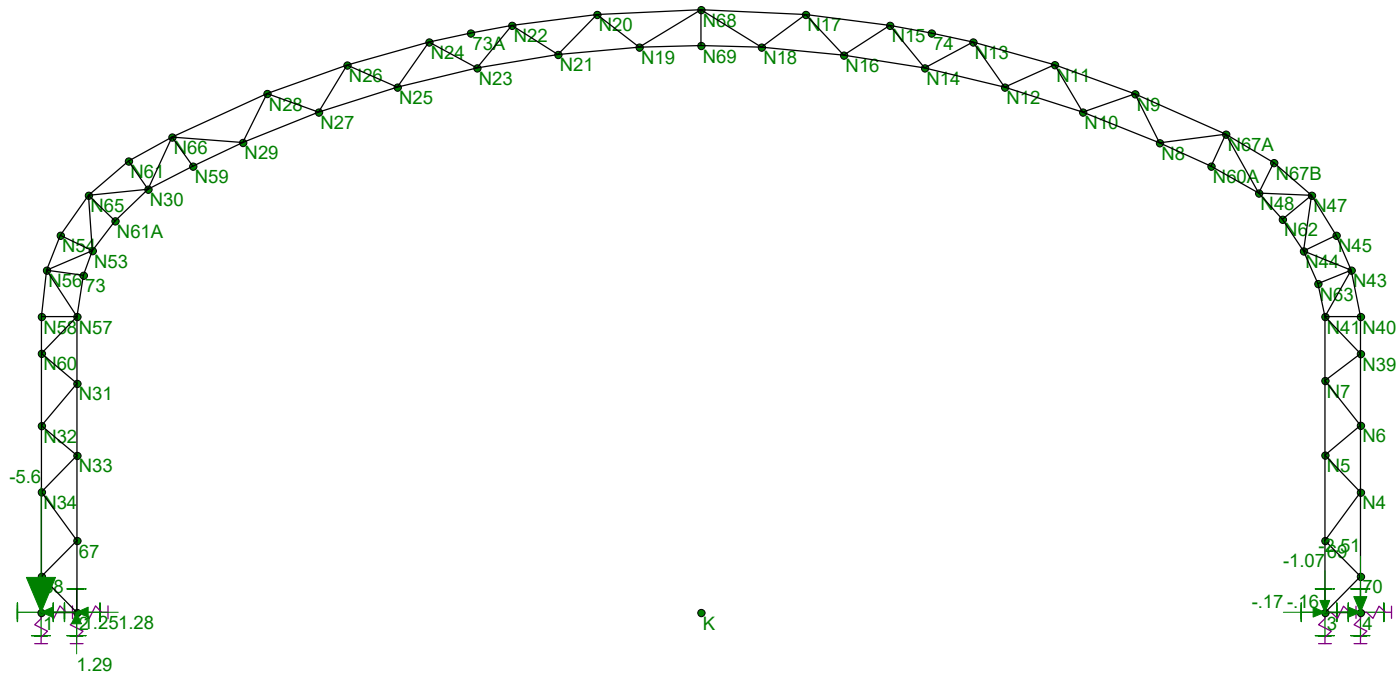
Big Top	50x72x23 DEM 18BB - Tallahassee, FL	SK - 9
Mo		May 27, 2021 at 11:32 AM
221-80		50x72x23 DEM 18BB - Tallahassee, FL.r3d



Joint Reactions (By Combination)

	LC	Joint Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]
1	14	1	0	1.204	-.215	0	0	0
2	14	2	0	-.089	-.221	0	0	0
3	14	3	0	-.079	.221	0	0	0
4	14	4	0	1.19	.215	0	0	0
5	14	Totals:	0	2.225	0			
6	14	COG (ft):	X: 0	Y: 19.77	Z: 24.977			

Reactions due to RLL only



Results for LC 15, WL+Z
 Reaction and Moment Units are k and k-ft

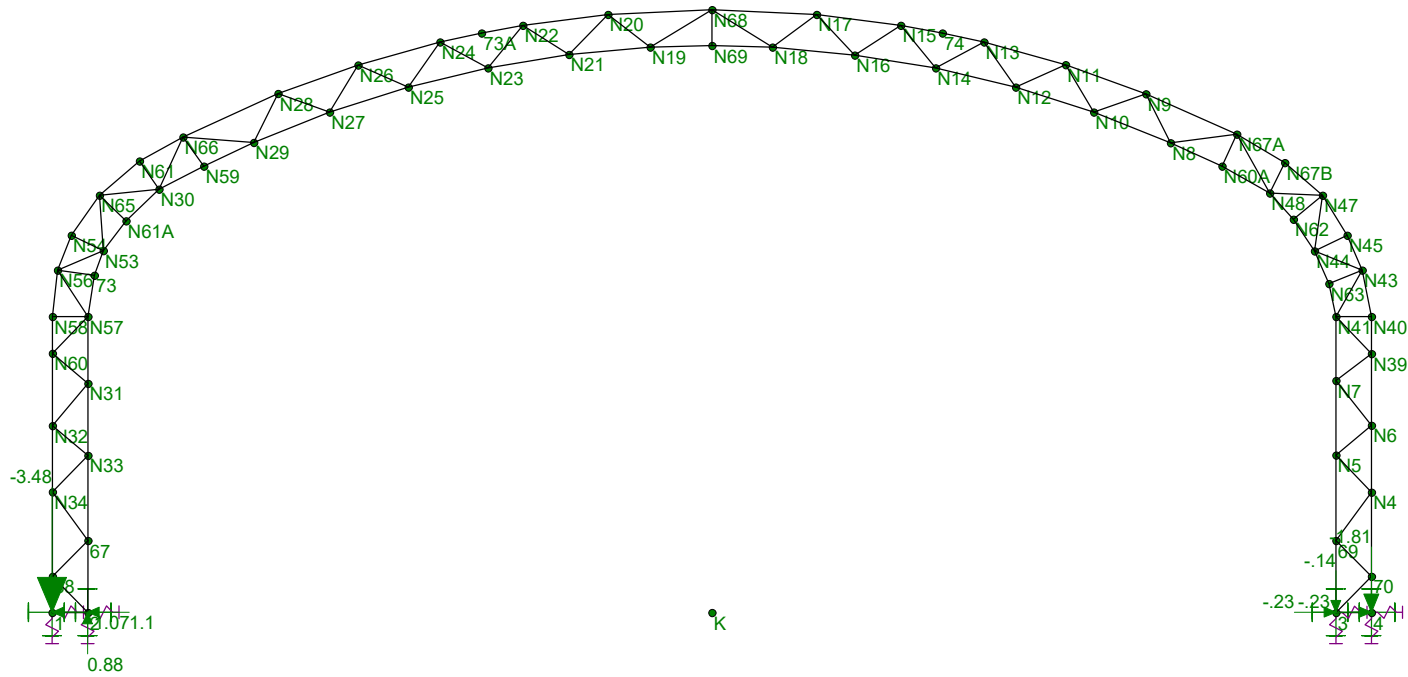
Big Top	50x72x23 DEM 18BB - Tallahassee, FL	SK - 10
Mo		May 27, 2021 at 11:32 AM
221-80		50x72x23 DEM 18BB - Tallahassee, FL.r3d



Joint Reactions (By Combination)

	LC	Joint Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]
1	15	1	0	-5.597	1.245	0	0	0
2	15	2	0	1.29	1.28	0	0	0
3	15	3	0	-1.073	-.17	0	0	0
4	15	4	0	-2.509	-.164	0	0	0
5	15	Totals:	0	-7.889	2.191			
6	15	COG (ft):	X: 0	Y: 20.363	Z: 26.556			

Reactions due to WL+Z only



Results for LC 16, WL-Z
 Reaction and Moment Units are k and k-ft

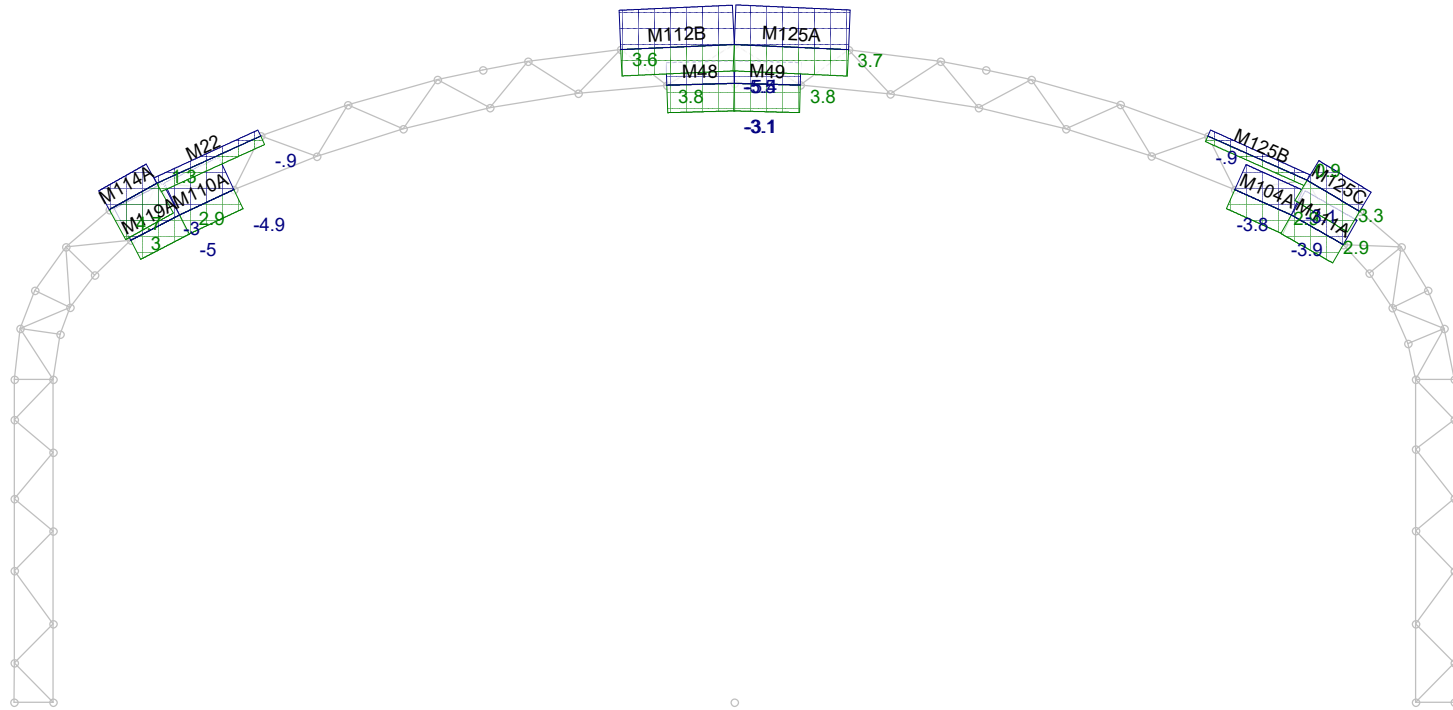
Big Top	50x72x23 DEM 18BB - Tallahassee, FL	SK - 11
Mo		May 27, 2021 at 11:32 AM
221-80		50x72x23 DEM 18BB - Tallahassee, FL.r3d



Joint Reactions (By Combination)

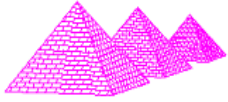
	LC	Joint Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]
1	16	1	0	-3.476	1.073	0	0	0
2	16	2	0	.879	1.104	0	0	0
3	16	3	0	-.143	-.234	0	0	0
4	16	4	0	-1.815	-.227	0	0	0
5	16	Totals:	0	-4.555	1.716			
6	16	COG (ft):	X: 0	Y: 20.425	Z: 28.032			

Reactions due to WL-Z only



Envelope Only Solution
 Member Axial Forces (k) (Enveloped)
 Reaction and Moment Units are k and k-ft (Enveloped)

Big Top	50x72x23 DEM 18BB - Tallahassee, FL	SK - 7
Mo		May 27, 2021 at 10:44 AM
221-80		50x72x23 DEM 18BB - Tallahassee, FL.r3d



Connection Check

PROJECT NUMBER 221-80

DESIGNER Mo

=Input
 =Calculation

Connection Check

Max Tension at Bolts = 5.5 kips

Bolted Connection

1 (# Bolts)
 1/2 inch (dia.)
 Material: A325 45 ksi
 8.8 kips
 (try 1/2" for trusses <= 40', otherwise use 5/8" min.)
 (F_{nt}/Ω, AISC Table 7-2)
 Number of bolts * Steel Strength * d² * pi/4

*USE only 90% of capacity because bolts are not centered in the connection.

Capacity = 0.9 * 8.8 kips = 8.0 > 5.5 kips

USE (1) 1/2" DIAM. BOLTS IN THE TOP AND BOTTOM CHORDS

Welded Connection

Max. Weld size allowed per AISC 360-10 (15th Edition), section J2.2b (a): 1/11 inch

Max Tension = $\frac{\text{span style="border: 1px solid black; padding: 2px;">5.5 \text{ kips}}{\text{span style="background-color: #d3d3d3; border: 1px solid black; padding: 2px;">1.34 \text{ kips/in}}$ = 4.1 Inch Weld Length

USE 5" MIN. LENGTH E70 WELD 0.09"

PRying ACTION ANALYSIS

For Structural Steel Connections
Per AISC 13th Edition Manual (ASD) - Pages 9-10 to 9-13

Project Name:	Client:	
Project No.: 221-80	Prep. By:	Date:

Input Data:

Total Tension Load, Tt =	5.50	kips
Total Shear Load, Vt =	0.20	kips
Tensile Strength, Fu =	65	ksi
Bolt Diameter, db =	1/2	in.
ASTM Bolt Desig. =	A325	
Bolt Type (N, X, or SC) =	N	
Faying Surface Class =	N.A.	
Bolt Hole Type =	Oversized	
Tributary Length/Bolt, p =	1.875	in.
Total No. of Bolts, Nb =	1	bolts
Width, bf =	4.0000	in.
Thickness, t =	0.3750	in.
Thickness, tw =	0.3750	in.
Bolt Gage, g =	2.000	in.
No. of Loading Cycles =	20000	

Results:

Check Bolt Tension and Shear:

Ab =	0.1963	in.^2	Ab = *db^2/4
vb =	0.20	kips/bolt	vb = Vt/Nb
fv =	1.02	ksi	fv = vb/Ab
T =	5.50	kips/bolt	T = Tt/Nb
ft =	28.01	ksi	ft = T/Ab
Tb =	N.A.	kips	Tb = not applicable for N or X bolts
Fnv =	48.00	ksi	Fnv = Nominal shear stress for A325-N from AISC Table J3.2, page 16.1-104
Fnv' =	48.00	ksi	Fnv' = Fnv (no reduction needed for comb. effects)
Fv =	24.00	ksi	Fv = Fnv' / 2
ks =	N.A.		ks = not applicable for N or X bolts
Vb =	4.71	kips/bolt	Vb = Ab*Fv
At =	0.1419	in.^2	At = /4*(db - 0.9743/n)^2
Fnt =	90.00	ksi	Fnt = Nominal tensile stress for A325 bolts from AISC Table J3.2, page 16.1-104
Fnt' =	90.00	ksi	Fnt' = Fnt (no reduction needed for comb. effects)
Ft =	45.00	ksi	Ft = Fnt' / 2, fatigue is not considered)
B =	8.84	kips/bolt	B = Ft*Ab

Nomenclature

Vb >= vb, O.K.

B >= T, O.K.

(continued)

Calculate Required Thickness:

b =	<input type="text" value="0.8125"/>	in.	b = (g-tw)/2
b' =	<input type="text" value="0.5625"/>	in.	b' = b-db/2
a =	<input type="text" value="1.0000"/>	in.	a = minimum of: (bf-g)/2 or 1.25*b
a' =	<input type="text" value="1.2500"/>	in.	a' = a+db/2
	<input type="text" value="0.4500"/>		= b'/a'
d' =	<input type="text" value="0.6250"/>	in.	d' = Nominal hole dimensions from Table J3.3
	<input type="text" value="0.6667"/>		= 1-d'/p
	<input type="text" value="1.348"/>		= (1/)*(B/T-1)
' =	<input type="text" value="1.0000"/>		If >= 1: ' = 1, If < 1: ' = lesser of 1 or (1/)*(/((1-)))
t(req'd) =	<input type="text" value="0.318"/>	in.	t(req'd) = SQRT(6.66*T*b'/(p*Fu*(1+ * '))) t >= t(req'd), O.K.

Calculate Prying Force, Q:

tc =	<input type="text" value="0.521"/>	in.	tc = SQRT(6.66*B*b'/(p*Fu)) (to develop 'B' in bolts/no prying)
	<input type="text" value="0.303"/>		= 1/ *((T/B)/(t/tc)^2-1) (Note: 0 <= a <= 1.0)
Q =	<input type="text" value="0.42"/>	kips	Q = B* * * (t/tc)^2 (prying force per bolt at design load)

Check Allowable Bolt Tension with Prying Action:

' =	<input type="text" value="0.9635"/>		' = 1/(*(1+))*((tc/t)^2-1)
Ta =	<input type="text" value="7.51"/>	kips	If ' > 1: Ta = B*(t/tc)^2*(1+), If ' < 0: Ta = B
			If 0 <= ' <= 1: Ta = B*(t/tc)^2*(1+ * ')
			Ta >= T, O.K.

Calculate Required Thickness to Eliminate Prying Action:

t(req'd) =	<input type="text" value="0.411"/>	in.	t(req'd) = SQRT(6.66*T*b'/(p*Fu))
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Comments:

PRying ACTION ANALYSIS For Structural Steel Connections Per AISC 13th Edition Manual (ASD) - Pages 9-10 to 9-13

Project Name:	Client:	
Project No.: 221-80	Prep. By:	Date:

Input Data: Anchor Angle at Base

Total Tension Load, Tt =	1.56	kips
Total Shear Load, Vt =	0.36	kips
Tensile Strength, Fu =	65	ksi
Bolt Diameter, db =	1/2	in.
ASTM Bolt Desig. =	A325	
Bolt Type (N, X, or SC) =	N	
Faying Surface Class =	N.A.	
Bolt Hole Type =	Oversized	
Tributary Length/Bolt, p =	4.000	in.
Total No. of Bolts, Nb =	1	bolts
Width, bf =	6.0000	in.
Thickness, t =	0.2500	in.
Thickness, tw =	0.2500	in.
Bolt Gage, g =	3.000	in.
No. of Loading Cycles =	20000	

Results:

Check Bolt Tension and Shear:

Ab =	0.1963	in.^2	Ab = *db^2/4
vb =	0.36	kips/bolt	vb = Vt/Nb
fv =	1.85	ksi	fv = vb/Ab
T =	1.56	kips/bolt	T = Tt/Nb
ft =	7.92	ksi	ft = T/Ab
Tb =	N.A.	kips	Tb = not applicable for N or X bolts
Fnv =	48.00	ksi	Fnv = Nominal shear stress for A325-N from AISC Table J3.2, page 16.1-104
Fnv' =	48.00	ksi	Fnv' = Fnv (no reduction needed for comb. effects)
Fv =	24.00	ksi	Fv = Fnv' / 2
ks =	N.A.		ks = not applicable for N or X bolts
Vb =	4.71	kips/bolt	Vb = Ab*Fv
At =	0.1419	in.^2	At = /4*(db - 0.9743/n)^2
Fnt =	90.00	ksi	Fnt = Nominal tensile stress for A325 bolts from AISC Table J3.2, page 16.1-104
Fnt' =	90.00	ksi	Fnt' = Fnt (no reduction needed for comb. effects)
Ft =	45.00	ksi	Ft = Fnt' / 2, fatigue is not considered)
B =	8.84	kips/bolt	B = Ft*Ab

Nomenclature

Vb >= vb, O.K.

B >= T, O.K.

(continued)

Calculate Required Thickness:

b =	<input type="text" value="1.3750"/>	in.	b = (g-tw)/2
b' =	<input type="text" value="1.1250"/>	in.	b' = b-db/2
a =	<input type="text" value="1.5000"/>	in.	a = minimum of: (bf-g)/2 or 1.25*b
a' =	<input type="text" value="1.7500"/>	in.	a' = a+db/2
	<input type="text" value="0.6429"/>		= b'/a'
d' =	<input type="text" value="0.6250"/>	in.	d' = Nominal hole dimensions from Table J3.3
	<input type="text" value="0.8438"/>		= 1-d'/p
	<input type="text" value="7.283"/>		= (1/)*(B/T-1)
' =	<input type="text" value="1.0000"/>		If >= 1: ' = 1, If < 1: ' = lesser of 1 or (1/)*(/((1-)))
t(req'd) =	<input type="text" value="0.156"/>	in.	t(req'd) = SQRT(6.66*T*b'/(p*Fu*(1+ * '))) t >= t(req'd), O.K.

Calculate Prying Force, Q:

tc =	<input type="text" value="0.505"/>	in.	tc = SQRT(6.66*B*b'/(p*Fu)) (to develop 'B' in bolts/no prying)
	<input type="text" value="0.000"/>		= 1/ *((T/B)/(t/tc)^2-1) (Note: 0 <= a <= 1.0)
Q =	<input type="text" value="0.00"/>	kips	Q = B* * * (t/tc)^2 (prying force per bolt at design load)

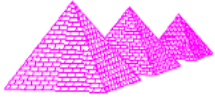
Check Allowable Bolt Tension with Prying Action:

' =	<input type="text" value="2.2176"/>		' = 1/(*(1+))*((tc/t)^2-1)
Ta =	<input type="text" value="4.00"/>	kips	If ' > 1: Ta = B*(t/tc)^2*(1+), If ' < 0: Ta = B
			If 0 <= ' <= 1: Ta = B*(t/tc)^2*(1+ * ')
			Ta >= T, O.K.

Calculate Required Thickness to Eliminate Prying Action:

t(req'd) =	<input type="text" value="0.212"/>	in.	t(req'd) = SQRT(6.66*T*b'/(p*Fu))
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Comments:



Soil Anchor Design - Tension

PROJECT NUMBER

DESIGNER

	=Input
	=Calculation

Connection Check

Max Uplift at Anchors = kips as per page: *Joint 1*

Anchored Connection

2500	lbs	Medium/Sandy Soil Gray	Ultimate Pullout Strength
		Type of Soil	
2		-----	Facto of Safety
1250	lbs	-----	Allowable Pullout Strength
250	lbs	-----	Alloawble Shear Strength

# of Vertical Anchors at Truss	1
# of sloped Anchors =	2
Angle of slope, ϕ =	15

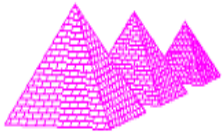
Pullout capacity = Pullout Strength * # of vertical Anchors + Pullout Strength * # of Sloped Anchors Cos (ϕ)

Allowable Pullout Capacity = kips

Shear capacity = Shear Strength * total # of Anchors + Pullout Strength * # of Sloped Anchors Sin (ϕ)

Allowable shear Capacity = kips

Pullout Capacity = kips 3.111 kips



Soil Anchor Design - Shear

PROJECT NUMBER

DESIGNER

	=Input
	=Calculation

Connection Check

Max Shear at Anchors = kips as per page: *Joint 2*

Anchored Connection

2000	lbs	Medium/Sandy Soil Gray	Ultimate Pullout Strength
		Type of Soil	
2		-----	Facto of Safety
1000	lbs	-----	Allowable Pullout Strength
250	lbs	-----	Alloawble Shear Strength

# of Vertical Anchors at Truss	1
# of sloped Anchors =	2
Angle of slope, ϕ =	15

Pullout capacity = Pullout Strength * # of vertical Anchors + Pullout Strength * # of Sloped Anchors Cos (ϕ)
 Allowable Pullout Capacity = kips

Shear capacity = Shear Strength * total # of Anchors + Pullout Strength * # of Sloped Anchors Sin (ϕ)
 Allowable shear Capacity = kips

Shear Capacity = kips 0.726 kips

Job: 221-80

Name: _____
Date: _____

Wind Pressure: **Ultimate**

Wind Pressure = **20.86** psf

Height to Use: **Average**

Tallest Height = **23** ft

Medium Height = **19.1145** ft

Lowest Height = **15.229** ft

Assumed Height = **0** ft

Height = **19.1** ft

Half Height = **9.6** ft

Wind Force = **199** plf of shelter width
=(Wind Pressure)(Half Height)*

Total Wind Force on Roof = **9968** lbs
=(Wind Force)(With)*

Total Wind Force on Single Wall = **4984** lbs
=(Total Wind Force on Roof)/2

Roof Cables

of Cables Along one Side = **4**

Length along X-Braces = **31.8** ft

Bay Spacing = **24** ft

Cable Angle = **53.0** degrees

Sum of Forces Equation

Force on 1 Side of Shelter = **8274**

Ultimate Capacity of Roof Cables

Capacity of Single Cable = **7000** lbs

Capacity of All Roof Cables = **28000** lbs

SAFE

Shelter Dimensions

Width: **50** ft

Length: **72** ft

Height: **23** ft

Cable Diameter Roof

1/4 in

Cable Diameter Wall

1/4 in

Wall Cables

of Cables Along one Wall = **8**

Length along X-Braces = **17.2** ft

Bay Spacing = **16** ft

Cable Angle = **47.1** degrees

Sum of Forces Equation

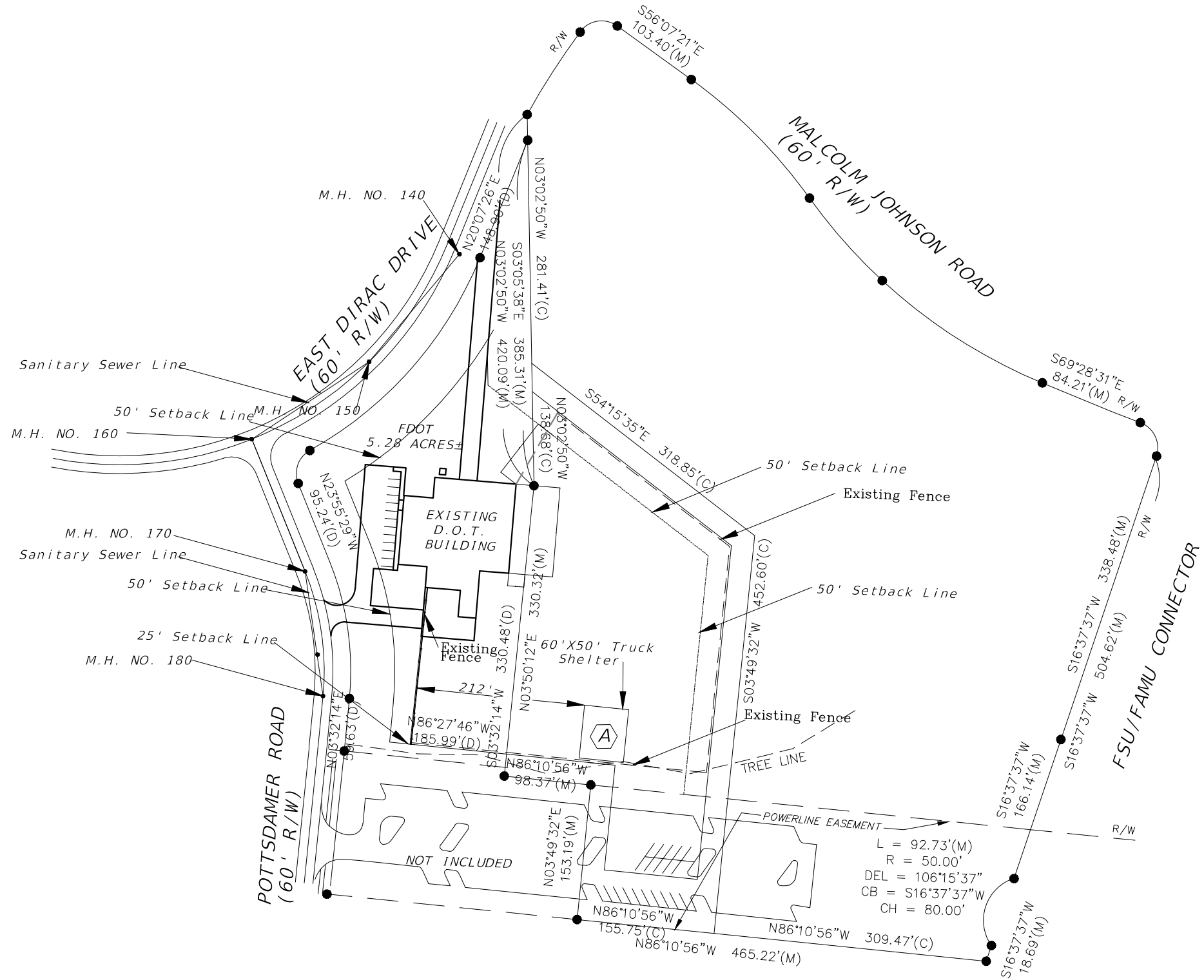
Force on 1 Side of Shelter = **3659**

Capacity of Side Wall Cables

Capacity of Single Cable = **7000** lbs

Capacity of Cables in Wall = **56000** lbs

SAFE



CONSTRUCTION NOTES:
 (A) Truck Parking Shelter



SITE PLAN

GENERAL NOTE:
 Contractor to verify all survey data and utilities locations

REVISIONS			REVISIONS			DRAWN BY: YY 08-23	STATE OF FLORIDA DEPARTMENT OF TRANSPORTATION			SHEET TITLE: Truck Parking Shelter	REF. DWG. NO.
DATE	BY	DESCRIPTION	DATE	BY	DESCRIPTION		ROAD NO.	COUNTY	FINANCIAL PROJECT ID.		
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